# Earlysville Road with Reas Ford Rd/Earlysville Forest Dr Intersection Traffic Study Earlysville, Albemarle County 

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## EXECUTIVE SUMMARY

This report summarizes evaluation of potential intersection improvement alternatives at the intersection of Earlysville Road with Reas Ford Road and Earlysville Forest Drive in Earlysville, Albemarle County. This study includes review of previous investigations, assessment of physical conditions, traffic volume collection, evaluation of crash data, discussion of alternatives, alternatives evaluation, signal warrant analysis, capacity analysis, queuing analysis, safety analysis, and investigative conclusions.

Albemarle County and The Virginia Department of Transportation (VDOT) previously identified safety concerns at the intersection of Earlysville Road with Reas Ford Road and Earlysville Forest Drive. As a result of a pattern of right angle crashes at the intersection, two traffic studies have been prepared evaluating the intersection.

## Previous Studies

An internal intersection traffic study was completed by VDOT Culpepper District in 2018. This study was prompted from a request from a state legislator based upon citizen concerns regarding intersection safety. This study included evaluation of crash data, sight distance, signal warrant analysis, auxiliary lane analysis, and signing and marking considerations. Recommendations from this report are separated by Short Term, Intermediate, and Long Term timeframes. Short term improvements consisted of low cost traffic control device installation, intermediate recommendations included a right turn lane on Reas Ford Road eastbound and driveway channelization, and the long term recommendation was to evaluate and construct a roundabout.

A subsequent intersection traffic study was completed by a consultant employed by VDOT in 2019. This study was again prompted by concerns from elected officials and local residents. This study included evaluation of existing conditions, traffic volume collection, crash analysis, intersection capacity analysis, alternative development, evaluation of alternatives, signal warrant analysis, conceptual cost estimates, alternative comparison, and recommendations. The recommendations of this report were separated as short term low cost improvements (traffic control device installation) and a long term recommendation to convert the intersection to a mini roundabout.

## Physical Conditions

The intersection of Earlysville Road with Reas Ford Road and Earlysville Forest Drive is a four legged crossroad intersection that is two way stop controlled with free flow on Earlysville Road. The Earlysville Business Park is located just over one mile west of the intersection along the south side of Reas Ford Road. This facility is a multi-tenant industrial park that generates truck traffic that utilizes the study intersection. The Charlottesville-Albemarle Airport is located two miles south of the intersection along the north side of Earlysville Road. The majority of airport traffic enters from US 29 and the roadway network south of the intersection.

## Traffic Volume

A 12-hour turning movement count was collected at the intersection of Earlysville Road with Reas Ford Road and Earlysville Forest Drive on Thursday September 23, 2021 between the hours of 7 AM to 7 PM. The overall peak hour was found to occur between the hours of 4 PM to 5 PM when 996 vehicles entered the intersection. This includes 543 vehicles on the Earlysville Road northbound approach, 307 vehicles on the Earlysville southbound approach, 95 vehicles on the Reas Ford Road eastbound approach, and 51
vehicles on the Earlysville Forest Drive westbound approach. Pedestrian volumes are low throughout all hours of the collected data, with less than five pedestrians in total traversing the intersection in all hours. Overall, trucks and heavy vehicles constitute $1.2 \%$ of all vehicles entering the intersection. Ten large trucks entered the intersection in the AM peak hour and 12 entered during the PM peak hour. The heaviest truck movement is the Reas Ford Road eastbound right turn movement, which is approximately $7 \%$ of all traffic on that approach.

## Crash Data

Crash data was obtained from VDOT sources for the most recent five year period available from July 1, 2016 to June 30, 2021. Crash data was utilized to quantify the recent safety performance of the intersection and to compare the potential benefit of potential alternatives understanding constrained funding for potential safety improvement projects. Over the five year period, 15 crashes were reported within the intersection and its influence area. Right angle crashes account for $53 \%$ of intersection crashes and is the most common crash type reported to occur. Angle crashes are the type of crash potentially prevented by the installation of a traffic signal or roundabout. Six of the intersection angle crashes involved a motorist from Reas Ford colliding with a northbound motorist on Earlysville Road. Right angle crashes are concerning since this is the type of intersection crash that tends to result in injuries. The right angle crashes at this intersection accounted for 12 of the 16 documented injuries. The data shows that the majority of the angle crashes occurred from 2016 to 2018, with only one angle crash each reported in 2019 and 2020, with zero in the first half of 2020.

## Alternative Evaluation

Preliminary intersection alternatives have been developed as the basis for evaluation within this study founded upon the results of previous studies and screening for appropriate countermeasures for similar locations. Preliminary design and cost estimation was performed for each alternative utilizing aerial survey data obtained from VDOT. Potential alternatives include No Build, widening Earlysville Road to construct left turn lanes in both directions and widening Reas Ford Road to construct an eastbound right turn lane (Alternative 1), installing a traffic signal along with the Alternative 1 improvements (Alternative 2), and converting the intersection to a single lane roundabout (Alternative 3). An additional short-term alternative is also briefly discussed, which is simple installation of All Way Stop Control (AWSC) as an interim measure (Alternative 4). One of the previous studies indicated that a mini roundabout should be considered for the intersection. Mini roundabouts are typically constructed in low speed residential areas and the study intersection is not appropriate for this type of design, especially considering the regular occurrence of large trucks arriving and departing the Earlysville Industrial Park via Reas Ford Road and prevailing speed of each roadway.

The No Build Alternative is detailed by existing traffic analysis and recent crash data. The No Build alternative is viable if existing intersection operation is acceptable in terms of level of service and crash history, or if the cost of improvement is excessive compared to the anticipated benefit. No major intersection modification or widening occurs in the No Build Alternative.

Alternative 1 includes construction of exclusive left turn lanes on both Earlysville Road approaches and construction of an exclusive right turn lane on the Reas Ford Road eastbound approach without any modification to intersection control (i.e. no need for signalization or a roundabout). Alternative $\mathbf{2}$ includes the installation of a traffic signal along with construction of exclusive left turn lanes on both Earlysville Road approaches and construction of an exclusive right turn lane on the Reas Ford Road eastbound
approach without any modification to intersection control. Alternative $\mathbf{3}$ includes construction of a single lane roundabout with an inscribed circle diameter of 170 feet. Due to the truck percentage and location of the Earlysville Business Park, the roundabout is a traditional design to accommodate a WB-62 design vehicle (tractor trailer).

Alternative 3B includes construction of a mini roundabout. This alternative was included based upon feedback from review of the preliminary report. This alternative is a modified version of Alternative 3 utilizing significantly smaller dimensions. The mini roundabout uses a total inscribed circle diameter of 80 feet to minimize right of way impact and cost. Alternative $\mathbf{3 B}$ is assumed to provide similar operational and safety impact compared to a traditional roundabout. Therefore; LOS, queuing, and safety analysis is assumed to be identical for the purpose of this study. The key difference with a mini roundabout is that the dimension do not accommodate large vehicles to traverse the circle the same as passenger cars. With a mini roundabout, large vehicles and trucks are able to travel through and over the center island, which can be mountable curb, painted, or a modular device. With the skewed angle of the Reas Ford approach to Earlysville Road, the mini roundabout would still necessitate modification of this approach to align near 90 degrees opposite Earlysville Forest Road.

Previous studies suggested construction of a mini roundabout at the intersection, which are typically utilized for intersections where all approaching roadways have prevailing speed of less than 30 mph and truck traffic is low. With the volume of truck traffic generated by the Earlysville Business Park west of the intersection on Reas Ford Road and the prevailing speed of traffic, a mini roundabout is likely not appropriate for this location.

Alternative 4 is simply the installation of All Way Stop Control (AWSC) as a short-term (interim only) potential option to address the occurrence of angle crashes at the intersection. This alternative includes installation of stop signs at the intersection with advance warning signs on Earlysville Road. The engineering construction estimate for the Alternative 4 improvements is of negligible cost. Costs to implement AWSC would be minimal if implemented by VDOT forces.

A summary table listing the potential alternatives and estimated construction cost is shown below:

| Alternative Number | Description | Construction Estimate |
| :---: | :---: | :---: |
| No Build | No Build | $\$ 0$ |
| Alt 1 | Turn Lanes Only | $\$ 1,903,495$ |
| Alt 2 | Traffic Signal and Turn Lanes | $\$ 2,330,995$ |
| Alt 3 | Traditional Roundabout | $\$ 4,267,066$ |
| Alt 3B | Mini Roundabout | $\$ 2,430,144$ |
| Alt 4 | All Way Stop | Less than $\$ 5,000$ |

## Traffic Signal Warrant Analysis

The Manual on Uniform Traffic Control Devices (MUTCD) contains nine warrants for investigating the need for a traffic signal at a particular intersection. The satisfaction of a signal warrant or warrants may indicate
the need for the installation of a traffic signal. Three of the warrants deal directly with traffic volumes; two warrants focus on pedestrian issues; one focuses on safety; one on grade crossings; one on traffic signal progression; and one on a Planning level (non-data-based) analysis. None of the nine MUTCD warrants are satisfied for the intersection of Earlysville Road with Reas Ford Road and Earlysville Forest Drive. The heaviest side street movement at the intersection is the right turn movement from Reas Ford Road, and right turning traffic is generally only impeded by the queue of left turning traffic. Based upon review of the actual intersection conditions, the MUTCD traffic signal warranting criteria is not satisfied for the study intersection.

## Turn Lane Analysis

Auxiliary turn lane analysis was performed for the intersection using the VDOT Access Management Design Standards for Entrances and Intersections, Revised January of 2021. These standards are based upon the AASHTO publication A Policy on Geometric Design of Highways and Streets. Based upon evaluation of actual intersection conditions, the Earlysville Road northbound approach meets the criteria for a left turn lane during the PM peak hour. In addition, the Reas Ford Road eastbound approach meets the criteria for a right turn lane during the AM peak hour.

## Capacity Analysis

The procedures outlined in the Highway Capacity Manual; $6^{\text {th }}$ Edition were used as guidelines for the analysis of the intersection alternatives. This manual provides procedures for the analysis of both signalized and unsignalized intersections. Level of Service (LOS) categories range from LOS "A" (best) to " F " (worst). LOS analysis was completed through the use of Synchro, version 10.3 and Sidra, version 9.0. These software packages categorize the LOS based on HCM methodology and criteria.

Evaluation of the collected data shows that the intersection currently (No Build Alternative) operates at an acceptable LOS, with LOS A on Earlysville Road with modest delay on the side streets. Reas Ford Road operates at LOS C and Earlysville Forest Drive operates at LOS D. Construction of auxiliary lanes including left turn lanes on Earlysville Road in both directions and a right turn lane on the Reas Ford Road eastbound approach (Alternative 1) provides minimal improvement only with LOS remaining unchanged. Installation of a traffic signal with auxiliary lanes (Alternative 2) improves all movements to LOS B or better. Installation of a roundabout (Alternative 3) improves all movements to LOS A or better. For the purpose of analysis, a traditional roundabout and a mini roundabout are assumed to provide the same LOS. The installation of All Way Stop Control (Alternative 4) as an interim measure improves LOS on the side roads to LOS B or better but deteriorates the Earlysville Road southbound approach to LOS D in the AM peak hour the northbound approach to LOS D in the PM peak hour. Alternative 4 is a considered a short term safety measure only.

## Queuing Analysis

Queuing refers to the back up of vehicles on a particular approach to an intersection. Analysis was performed at the study intersection during the weekday AM and PM peak hours using the SimTraffic micro-simulation model, which is a simulation complement to the Synchro traffic analysis models utilized for the capacity analysis.

Queuing analysis indicates that no existing (No Build Alternative) turning movements currently exceed the available storage length or impede other traffic movements during the peak periods analyzed. Queuing analysis indicates that all conditions described in the Existing Conditions are expected to continue
with similar queuing following construction of exclusive left turn lanes on Earlysville Road and a right turn lane on the Reas Ford (Alternative 1) northbound approach. Queue lengths are minimally reduced in comparison to Existing Conditions. With the installation of a traffic signal (Alternative 2), short queues are created on the Earlysville northbound and southbound approaches. The queues are not substantial and are not anticipated to inhibit access to proposed exclusive left turn lanes. Queuing on the side road approaches is similar to existing conditions. Queuing analysis indicates that queuing is anticipated to be minimal with the construction of a roundabout (Alternative 3). For the purpose of analysis, a traditional roundabout and a mini roundabout are assumed to provide the same queuing results. Queuing analysis indicates that queuing is anticipated to be a more significant issue with All Way Stop Control (Alternative 4). The most significant queue is the Earlysville Road southbound approach during AM peak hour and Earlysville northbound approach during PM peak hour.

## Safety Analysis

For purposes of comparing benefit vs cost for potential intersection improvement alternatives, evaluation of economic cost of safety performance resulting from motor vehicle crashes at the intersection was performed utilizing accepted Federal Highway Administration (FHWA) safety analysis procedures.

Applying approved Crash Modification Factors (CMF's), Alternative 3 (Roundabout) would be anticipated to result in the largest reduction in overall crashes at the intersection. Alternative 3, however, also is the most expensive and the most impactful to adjacent property owners and the community. Alternative 3B was is a mini roundabout option intended to be less costly. For the purpose of this study, crash reduction is assumed to be the same for the traditional roundabout and mini roundabout. Further evaluation of anticipated monetized annual safety performance over a 20 year service life was compared to the estimated cost of construction for each alternative. The 20 year performance assumes annual inflation of $4 \%$ for cost of each crash type. By comparison of the forecast crash reduction with estimated cost, Alternative 3B (mini roundabout) was found to achieve the highest benefit/cost ratio of all alternatives evaluated.

## Conclusions:

This report summarizes evaluation of potential intersection improvement alternatives at the intersection of Earlysville Road (Route 743) with Reas Ford Road (Route 660) and Earlysville Forest Drive (Route 660) in Earlysville, Albemarle County. Albemarle County and The Virginia Department of Transportation (VDOT) previously identified safety concerns at the intersection evidenced by crash data, and subsequently previously evaluated various options for modification of the intersection.

Based upon evaluation of the collected data and Alternatives evaluation, the following recommendations are made in regard to the intersection of Earlysville Road with Reas Ford Road and Earlysville Forest Drive:

- Based upon assessment of the entirety of the collected data, major intersection reconfiguration is not necessary at this time, and the No Build Alternative is appropriate. The intersection currently operates at adequate Level of Service (LOS) and the occurrence of crashes at the intersection has declined in the most recent 30 month period of the study.
- Due to the identified pattern of right angle crashes from 2016 to 2018, the intersection should continue to be monitored closely to determine if the recent reduction of intersection crashes following implementation of low cost safety improvements endures.
- If right angle crashes persist or increase where five or more occur in a 12 month period, a traffic signal can be installed in accordance with MUTCD Warrant Seven (Crash Safety). If safety performance or future traffic volume indicate that intersection control needs to be enhanced, a traffic signal or a roundabout both would provide adequate Level of Service.
- A mini roundabout appears to be inappropriate at this intersection due to volume, truck traffic, and prevailing speed. If a roundabout is considered in the future, a traditional roundabout is more appropriate for the conditions at this location.
- Ideally, construct auxiliary lanes including left turn lanes in both directions of Earlysville Road and a right turn lane on Reas Ford Road. VDOT warranting criteria based upon AASHTO is satisfied for these approaches. These auxiliary lanes, however, do not address the right angle crash pattern at the intersection or appreciably improve Level of Service.


## INTRODUCTION

This report summarizes evaluation of potential intersection improvement alternatives at the intersection of Earlysville Road (Route 743) with Reas Ford Road (Route 660) and Earlysville Forest Drive (Route 660) in Earlysville, Albemarle County. Albemarle County and The Virginia Department of Transportation (VDOT) previously identified safety concerns at the intersection of Earlysville Road and Reas Ford Road evidenced by crash data, and subsequently evaluated various options for modification of the intersection. This study includes review of previous investigations, assessment of physical conditions, traffic volume collection, evaluation of crash data, discussion of alternatives, alternatives evaluation, signal warrant analysis, capacity analysis, queuing analysis, safety analysis, and investigative conclusions.

The specific purpose of this study is to review and expand the effort from previous studies, determine if the roundabout alternative is appropriate, consider alternatives to a roundabout, evaluate the intersection operation to define any deficiency, provide cost and benefit analysis for improvements, evaluate and compare operation of alternatives, determine appropriate size of a potential roundabout, prepare cost estimates for recommended improvements, and identify the pros and cons associated with the proposed recommendation including impact of construction on neighboring businesses and the community of Earlysville.

Traffic analyses will consider No Build Conditions utilizing 2021 date along with evaluation of four separate alternatives. Forecast or Design Year analysis was not part of the scope of work for this investigation. Alternatives evaluated include widening to construct left turn lanes on Earlysville Road and right turn lane on Reas Ford Road without installation of a traffic signal (Alternative 1), Installation of a Traffic Signal with left turn lanes on Earlysville Road and a right turn lane on Reas Ford Road (Alternative 2), conversion to a roundabout (Alternative 3 and Alternative 3B), and installation of All-way Stop Control (Alternative 4). The No Build Alternative is evaluated for comparison as shown in the existing configuration. Crash data is reviewed in detail to document the extent of the existing safety issue and as related to performance of potential mitigation strategies.

The study area and project location is shown on Figure 1.


Earlysville and Reas Ford Road
Site Location Map

FIGURE 1

## PREVIOUS STUDIES

Albemarle County and The Virginia Department of Transportation (VDOT) previously identified safety concerns at the intersection of Earlysville Road with Reas Ford Road and Earlysville Forest Drive. The primary issues that resulted in the previous intersection studies were right angle crashes that occurred at the intersection. The principal conclusion of previous intersection studies was that the intersection should be reconfigured as a roundabout. Copies of previous traffic study documents are included in Appendix I.

An internal intersection traffic study was completed by VDOT Culpepper District in 2018. This study was prompted from a request from a state legislator based upon citizen concerns regarding intersection safety. This study included evaluation of crash data, sight distance, signal warrant analysis, auxiliary lane analysis, and signing and marking considerations. Recommendations from this report are separated by Short Term, Intermediate, and Long Term timeframes and are shown below:

- Short Term Recommendations:
- Refresh Stop Ahead pavement markings on Reas Ford Road
- Refresh Stop Bar on the Reas Ford Road approach
- Refresh and relocate Stop Bart forward on the Earlysville Forest Drive approach
- Intermediate Recommendations:
- Introduce driveway channelization for uncontrolled approaches in the northwest quadrant
- Construct an exclusive right-turn lane on the Reas Ford Road approach
- Long Term Recommendations:
- Evaluate and install a roundabout as the preferred intersection alternative

A subsequent intersection traffic study was completed by a consultant employed by VDOT in 2019. This study was again prompted by concerns from elected officials and local residents. This study included evaluation of existing conditions, traffic volume collection, crash analysis, intersection capacity analysis, alternative development, evaluation of alternatives, signal warrant analysis, conceptual cost estimates, alternative comparison, and recommendations. The recommendations of this report were separated as short term low cost improvements and a long term recommendation to convert the intersection to a mini roundabout. Recommendations are detailed below:

- Short Term (Low Cost) Recommendations:
- Dual installation of oversized W2-1 (Crossroad Warning) signs with street name plaques
- Enhanced pavement markings to delineate through lanes through the intersection
- Dual installation of W3-1 (Stop Ahead) signs on side streets
- Dual installation of R1-1 (STOP) signs on side streets
- Install retroreflective sign post inserts
- Removal of vegetation or obstructions to improve sight distance
- Long Term Recommendation:
- Construct a mini roundabout

Additional traffic control devices have been installed at the intersection following the most recent traffic study. The additional traffic control devices include:

- Radar feedback sign on Earlysville Road NB - Installed May 2020
- Flashing LED STOP sign on Reas Ford Road - installed June 2020


## ROADWAY CONDITIONS

Below is a detailed description of the existing study area roadway network. AADT (Annual Average Daily Traffic) volume information was estimated based on the collected turning movement counts (TMC) using a K factor of $10 \%$.

Earlysville Road (Route 743) is a two lane Urban Collector roadway with an exclusive right turn lane in the northbound direction. The roadway is undivided with shoulders of varying width from 0-10 feet wide. Earlysville Road is oriented north-south operating as free-flow traveling unimpeded through the intersection. The speed limit on Earlysville Road is 35 mph (miles per hour) and the AADT is $8,500 \mathrm{vpd}$ (vehicles per day).

Reas Ford Road (Route 660) is a two lane Rural Major Collector roadway. Reas Ford Road is oriented eastwest operating under stop control. The roadway is undivided without paved shoulders and has an open ditch on the east side of the road. The speed limit on Reas Ford Road is 35 mph and the AADT is 5,700 vpd.

Earlysville Forest Drive (Route 660) is a two lane undivided Urban Local Collector without paved shoulders. Earlysville Forest Drive is oriented east-west opposite Reas Ford Road operating under stop control. The speed limit on Earlysville Forest Drive is 35 mph and the AADT is $1,110 \mathrm{vpd}$.

The Rivanna Community Church is located in the northeast quadrant of the intersection. A new sanctuary was recently completed that relocated the building closer to the roadway. The parking area with access to Earlysville Forest Drive has also been expanded. The Earlysville Exchange Thrift Store is located in the northwest quadrant of the intersection with an uncontrolled driveway frontage along the west side of Earlysville Road. VIP Customs is located north of and adjacent to the Earlysville Exchange and utilizes the same uncontrolled connected roadway frontage. The Earlysville Auto Center is located 0.07 mile north of the intersection along the east side of Earlysville Road. The Earlysville Post Office is located in the southeast quadrant of the intersection with access to Earlysville Forest Drive via Bent Oaks Drive.

The Earlysville Business Park is located just over one mile west of the intersection along the south side of Reas Ford Road. This facility is a multi-tenant industrial park that generates truck traffic that utilizes the study intersection. The Charlottesville-Albemarle Airport is located two miles south of the intersection along the north side of Earlysville Road. The majority of airport traffic enters from US 29 and the roadway network south of the intersection.

Table 1 below provides a detailed description of the existing study area roadway network. The 2021 existing intersection lane configuration and intersection control are shown on Figure 2.

Table 1: Roadway Facility Summary

| Name | Code | State Functional <br> Classification | Area | Direction | Speed <br> Limit | AADT | Year | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Earlysville Road | 743 | Urban Collector | Earlysville | N-S | 35 | 8,500 | 2021 | N-S Urban Collector that connects with Route 606 to the southeast <br> and Route 629 to the northwest |
| Reas Ford Road | 660 | Rural Major <br> Collector | Earlysville | E-W | 35 | 5,700 | 2021 | E-W Rural Major Collector that connects to Route 676 to the south <br> and Route 743 to the north |
| Earlysville Forest <br> Drive | 660 | Urban Local <br> Collector | Earlysville | E-W | 35 | 1,110 | 2021 | E-W Urban Local Collector that intersects with Route 743 to the |
| north and south |  |  |  |  |  |  |  |  |



| LEGEND |  |  |
| :---: | :---: | :---: |
| ST0P Existing Traffic Control |  | Earlysville and Reas Ford Road |
| - Existing Roadway <br> $\rightarrow$ Existing Lane Configuration |  | 2021 Existing Lane Configuration |
| XXX Storage Bay Length | NOT | DATE: March 2022 |
|  | $\begin{gathered} \text { TO } \\ \text { SCALE } \end{gathered}$ | FIGURE 2 |

## TRAFFIC VOLUME

A 12-hour turning movement count was collected at the intersection of Earlysville Road with Reas Ford Road and Earlysville Forest Drive on Thursday September 23, 2021 between the hours of 7 AM to 7 PM. On this date, Albemarle County Schools were fully operational with in classroom instruction for all students.

The overall peak hour was found to occur between the hours of 4 PM to 5 PM when 996 vehicles entered the intersection. This includes 543 vehicles on the Earlysville Road northbound approach, 307 vehicles on the Earlysville southbound approach, 95 vehicles on the Reas Ford Road eastbound approach, and 51 vehicles on the Earlysville Forest Drive westbound approach.

Overall, trucks and heavy vehicles constitute $1.2 \%$ of all vehicles entering the intersection. Ten large trucks entered the intersection in the AM peak hour and 12 entered during the PM peak hour. The most significant truck movements occur on the Reas Ford Road approach right turn movement (7\% in the PM peak hour), the Earlysville Road northbound left turn movement ( $5 \%$ in the PM peak hour), and the Earlysville Road southbound right turn movement ( $6 \%$ in the PM peak hour).

Pedestrian and bicycle data was collected as part of the turning movement counts. Pedestrian volumes are low throughout all hours of the collected data, with less than five pedestrians traversing the intersection in all hours.

The turning movement count (including truck and pedestrian data) is located in Appendix B and the 2021 Existing Traffic Volumes for the weekday AM and PM peak hour volumes are shown in Figure 3.



## CRASH DATA

Crash data was obtained from VDOT sources for the most recent five year period available from July 1, 2016 to June 30, 2021. Crash data was utilized to quantify the recent safety performance of the intersection and to compare the potential benefit of potential alternatives understanding constrained funding for potential safety improvement projects.

Over the five year period, 15 crashes were reported within the intersection and its influence area. The influence area of the intersection was assumed to be within 300 feet on all approaches. Of the 15 crashes, one occurred during hours of darkness and two occurred on wet and/or snow covered pavement. The 15 total reported crashes include eight angle crashes, two rear end crashes, two sideswipe (opposite direction) crashes, one head-on crash, one roadway departure (right) crash, and one crash involving a bicycle rider being struck by a vehicle. Right angle crashes account for $53 \%$ of intersection crashes and is the most common crash type reported to occur. Angle crashes are the type of crash potentially prevented by the installation of a traffic signal or roundabout. Table $\mathbf{2}$ below provides a summary of the crash type along with the percentage of total crashes at the intersection during the five-year period.

Table 2: Crash Type Summary

| Crash Type | Number of Crashes | Percent of Total |
| :--- | ---: | ---: |
| Angle | 8 | $53 \%$ |
| Head On | 1 | $7 \%$ |
| Bicycle Hit by Vehicle | 1 | $7 \%$ |
| Ran Off Road (Right) | 1 | $7 \%$ |
| Rear End | 2 | $13 \%$ |
| Sideswipe, Opposite Direction | 2 | $13 \%$ |

No fatal crashes occurred at the intersection during the study period. The 15 total reported crashes resulted in 16 total reported injuries from eight injury crashes. Of the 16 total injuries, two were Type A injuries, 11 were Type B injuries, and three were Type C injuries. Type A injuries are severe incapacitating injuries, Type B injuries are non-incapacitating visible injuries, and Type C injuries are non-visible injuries where the occupant complains of pain. Twelve of the injuries resulted from the right angle crashes and two injuries occurred during the collision involving a bicycle. Table $\mathbf{3}$ provides a summary of number of injuries by crash severity.

Table 3: Injuries by Severity

| Injury Type | Number of Injuries | Percent of Total |
| :--- | ---: | ---: |
| Fatal Injuries | 0 | $0 \%$ |
| Class A Injuries | 2 | $13 \%$ |
| Class B Injuries | 11 | $69 \%$ |
| Class C Injuries | 3 | $19 \%$ |
| Total Non-Fatal Injuries | 16 | $100 \%$ |
| Total Injuries | 16 | $100 \%$ |

The intersection crash rate was determined to be 0.83 crashes per million entering vehicles. The intersection severity rate is 0.11 injuries per million entering vehicles, with serious injuries being correlated with Type A injuries. Table 4 provides a summary of the intersection crash rates.

Table 4: Intersection Crash Rate Summary

| Intersection | DHV | ADT | Crashes | Years | Crash Rate <br> (CPMEV) | Total <br> Injuries | Injury <br> Rate | Severe (Type <br> A + Fatal) | Severity <br> Rate |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Earlysville Road with Reas Ford Road | 996 | 9960 | 15 | 5 | 0.83 | 16 | 0.88 | 2 | 0.11 |

The most concerning crash pattern at the intersection is the occurrence of right angle crashes involving entering motorists from the Reas Ford approach. Six of the intersection right angle crashes involved a motorist from Reas Ford colliding with a northbound motorist on Earlysville Road. A single angle crash also occurred from the Thrift Store open frontage approach and another from the Ravenna Community Church approach. Right angle crashes are concerning since this is the type of intersection crash that tends to result in injuries. The right angle crashes at this intersection accounted for 12 of the 16 documented injuries. The data shows that the majority of the angle crashes occurred from 2016 to 2018, with only one reported in 2019 and none in 2020 or the first half of 2021.


## ALTERNATIVES DISCUSSION

Preliminary intersection alternatives have been developed as the basis for evaluation within this study founded upon the results of previous studies and screening for appropriate countermeasures for similar locations. Preliminary design was performed for each alternative utilizing aerial survey data obtained from VDOT. Initial cross sections were developed for each site specific improvement for the purpose of preparing accurate cost estimates.

Potential alternatives include widening Earlysville Road to construct left turn lanes in both directions and widening Reas Ford Road to provide an eastbound right turn lane (Alternative 1), Installing a traffic signal along with the Alternative 1 improvements (Alternative 2), and converting the intersection to a single lane roundabout (Alternative 3). A mini roundabout option (Alternative 3B) is also included as a variation of Alternative 3. An additional short-term alternative is also briefly discussed, which is simple installation of All Way Stop Control (AWSC) as an interim measure (Alternative 4).

## Intersection Alternatives

Intersection Alternative improvements Include:

* No Build Alternative
* Alternative 1: Left-Turn Lanes Earlysville Road NB and SB \& Right-Turn Lane Reas Ford Road EB
* Alternative 2: Installation of a Traffic Signal along with Left-Turn Lanes Earlysville Road \& Right-

Turn Lane Reas Ford Road

* Alternative 3: Single Lane Roundabout
* Alternative 3B: Mini Roundabout
- Alternative 4: Interim AWSC


## No Build Alternative

The Traffic Operations Study details analysis of Existing Condition, which equates as the No Build Condition for the intersection. The No Build Alternative is detailed by existing traffic analysis and current crash data. The No Build alternative is viable if existing intersection operation is acceptable in terms of level of service analysis and crash history, or if the cost of improvement is excessive compared to the anticipated benefit. Table 5 presents Pros and Cons for the No Build Alternative.

Table 5: No Build Pros \& Cons

| Pros | Cons |
| :--- | :--- |
| No Cost | No Substantial Safety Enhancement |
| No Property Impacts | Potential Stakeholder Dissatisfaction |
| Earlysville Road Remains Free Flow |  |
| Allows further Monitoring |  |
| Intersection Operation is Already Acceptable |  |

## Alternative 1 (Turn Lanes Only)

Alternative 1 include construction of exclusive left turn lanes on both Earlysville Road approaches and construction of an exclusive right turn lane on the eastbound Reas Ford Road approach without any modification to intersection control. The engineering construction estimate for the Alternative 1 improvements is $\$ \mathbf{1}, \mathbf{9 0 3}, \mathbf{4 9 5}$. A breakdown of costs for the estimate can be found Appendix $\mathbf{E}$.

Widening will require right of way acquisition but is not anticipated to adversely impact any adjacent property owners. Utility relocations are minimal or not necessary with this alternative. All driveway and property access is left intact as well. Table 6 presents Pros and Cons for Alternative 1.

Table 6: Alternative 1 Pros \& Cons

| Pros | Cons |
| :--- | :--- |
| Less Costly Compared with other Alternatives | Does Not Address Right Angle Crashes |
| Reduces Potential for Rear End Crashes | Potential Stakeholder Dissatisfaction |
| Earlysville Road Remains Free Flow | Property Impacts are Moderate |
| Improves Operation of Side Streets |  |

A detailed exhibit of Alternative 1 is illustrated in Figure 5.

## Alternative 2 (Traffic Signal Plus Turn Lanes)

Alternative 2 include the installation of a traffic signal along with construction of exclusive left-turn lanes on both Earlysville Road approaches and construction of an exclusive right-turn lane on the eastbound Reas Ford Road approach without any modification to intersection control. The engineering construction estimate for the Alternative $\mathbf{2}$ improvements is $\mathbf{\$ 2 , 3 3 0 , 9 9 5}$. A breakdown of costs for the estimate can be found Appendix E.

The same as Alternative 1, widening will require right of way acquisition but is not anticipated to adversely impact any adjacent property owners. Utility relocations are minimal or not necessary with this alternative. All driveway and property access is left intact as well. Installation of the signal improves ingress and egress from the Rivanna Church, Earlysville Business Park, and Earlysville Post Office. Due to proximity, the queuing from the traffic signal creates some interference with the open driveway to the Earlysville Exchange and VIP Customs. Table $\mathbf{7}$ presents Pros and Cons for Alternative 2.

Table 7: Alternative 2 Pros \& Cons

| Pros | Cons |
| :--- | :--- |
| Less Costly than Roundabout Alternative | Long Term Maintenance |
| Reduces Potential for Angle Crashes | Increases Delay on Earlysville Road |
| Improves Operation of Side Streets | Property Impacts are Moderate |
| Gateway to Business Park | Potential for Increased Rear End Crashes |
| Less Property Impacts than Roundabout | Marginal Need for Signal in terms of Volume |

A detailed exhibit of Alternative 2 is illustrated in Figure 6.

## Alternative 3 (Single Lane Roundabout)

Alternative 3 includes construction of a single lane roundabout with an inscribed circle diameter of 170 feet. Due to the truck percentage and location of the Earlysville Business Park, the roundabout is designed to accommodate a WB-62 design vehicle. The engineering construction estimate for the Alternative 3 improvements is $\mathbf{\$ 4 , 2 6 7 , 0 6 6}$. A breakdown of costs for the estimate can be found Appendix E.

Construction of the single lane roundabout will have major impacts on right of way acquisition. The roundabout creates significant takes from the Rivanna Community Church, Earlysville Post Office, and likely total takes for the Earlysville Exchange on the northwest corner. One utility pole will be relocated. This alternative will require a complex Temporary Traffic Control (TTC) plan that adds significant cost. Table 8 presents Pros and Cons for Alternative 3.

Table 8: Alternative 3 Pros \& Cons

| Pros | Cons |
| :--- | :--- |
| Greatest Reduction in Crashes Predicted | Most Costly Alternative |
| Traffic Calming Impact | Major Property Impacts |
| Better LOS Compared with Traffic Signal | Benefit vs Cost |
| Improves Operation of Side Streets | Constructability and MOT |
| Gateway to Business Park |  |

A detailed exhibit of Alternative $\mathbf{3}$ is illustrated in Figure 7.

## Alternative 3B (Mini Roundabout)

Alternative 3B includes construction of a single lane mini roundabout with an inscribed circle diameter of 80 feet. Trucks would traverse a mountable circular median built within existing right of way. Due to the skewed angle of approach, the Reas Ford approach necessitates realignment for proper operation. The engineering construction estimate for the Alternative 3B improvements is $\mathbf{\$ 2 , 4 3 0 , 1 4 4}$. A breakdown of costs for the estimate can be found Appendix E.

Previous studies suggested construction of a mini roundabout. Typically, mini roundabouts should only be considered in areas where all approaching roadways have prevailing speed of less than 30 mph . Mini roundabouts are not well suited for high volumes of trucks, as trucks will occupy most of the intersection when turning. Mini roundabouts are most often employed in residential areas with lower volumes of traffic. With the volume of truck traffic generated by the Earlysville Industrial Park west of the intersection on Reas Ford Road and the prevailing speed of traffic, a mini roundabout may not be appropriate for this location.

Construction of the mini roundabout will have modest impacts on right of way acquisition for the realignment of the Reas Ford Road approach. Table 9 presents Pros and Cons for Alternative 3B.

Table 9: Alternative 3B Pros \& Cons

| Pros | Cons |
| :--- | :--- |
| Greatest Reduction in Crashes Predicted | Impacts to Truck Traffic |
| Traffic Calming Impact | Not Appropriate with Industrial Park |
| Better LOS Compared with Traffic Signal | May be perceived as a Nuissance |
| Highest B/C safety Ratio | Constructability and MOT |
| Less Expensive than a Traditional Roundabout |  |

A detailed exhibit of Alternative 3B is illustrated in Figure 8.

## Alternative 4 (Interim AWSC)

Alternative 4 is simply the installation of All Way Stop Control (AWSC) as a short-term interim potential option to address the occurrence of angle crashes at the intersection. This alternative includes installation of stop signs at the intersection with advance warning signs on Earlysville Road. The engineering construction estimate for the Alternative 4 improvements is of negligible cost. Costs to implement AWSC would be under $\$ \mathbf{5}, 000$ if implemented by VDOT forces.

There are no impacts with the installation of the AWSC aside from traffic operations, which is detailed in the capacity section of this report. AWSC is not a long term intersection control strategy and should be considered an interim measure only if determined to be viable to address angle crashes. No design schematic is provided for this interim alternative. Table $\mathbf{1 0}$ presents Pros and Cons for Alternative 4.

Table 10: Alternative 4 Pros \& Cons

| Pros | Cons |
| :--- | :--- |
| Minimal Cost | Disruptive to Earlysville Road LOS |
| Easily Implemented | Potential for Rear End Crashes on Earlysville Road |
| Addresses Right Angle Crash Problem | Stakeholder Dissatisfaction |
| Improves Operation of Side Streets | Interim Solution Only |
|  | No Gateway Effect for Industrial Park |






## SIGNAL WARRANT ANALYSIS

The Manual on Uniform Traffic Control Devices (MUTCD) contains nine warrants for investigating the need for a traffic signal at a particular intersection. The satisfaction of a signal warrant or warrants may indicate the need for the installation of a traffic signal. Three of the warrants deal directly with traffic volumes; two warrants focus on pedestrian issues; one focuses on safety; one on grade crossings; one on traffic signal progression; and one on a Planning level (non-data-based) analysis.

In accordance with MUTCD procedures, the impact of right turning traffic from the side street approaches was assessed to determine appropriate consideration as a component of the signal warrant analysis. Left turning motorists or those crossing the intersection are those most benefiting from a traffic signal, as right turning maneuvers typically can be made easily without a signal. Therefore, Pagones Theorem was utilized to reduce the number of right turns included in the minor street approach volume. A detailed report containing the hourly volumes at the intersection is located in Appendix D.

## Warrant 1 - Eight-Hour Vehicular Volume

This warrant is intended for application at locations where there is a large volume of intersection traffic. To meet Warrant 1, the major street traffic (total of both approaches) must meet or exceed 350 vehicles per hour while the minor street traffic (one direction only) must meet or exceed 105 vehicles per hour for any eight hours of the day (Condition A - Minimum Vehicular Volume), or the major street traffic (total of both approaches) must meet or exceed 525 vehicles per hour while the minor street traffic (one direction only) must meet or exceed 53 vehicles per hour for any 8 hours of the day (Condition B - Interruption of Continuous Traffic). Warranting criteria have been reduced by $30 \%$ to utilize the $70 \%$ column to reflect the isolated location of the intersection. Adjustment of side street right turn volume was made using Pagones Theorem.

The minimum thresholds and conditions for this warrant as listed in the MUTCD are located on Table 11.
It is intended that warrant 1 be treated as a single warrant. If condition $A$ is satisfied, then the criteria for warrant 1 is satisfied and condition $B$ and the combination of condition $A$ and $B$ are not needed. Also, if condition $B$ is satisfied, then the criteria for warrant 1 is satisfied and the combination of conditions $A$ and $B$ is not needed. Warrant 1 is considered the primary warrant for the installation of a signal and is often considered as singular standalone criteria.

Table 11: MUTCD Table 4C-1, Warrant 1 Eight-Hour Vehicular Volume
Table 4C-1. Warrant 1, Eight-Hour Vehicular Volume
Condition A-Minimum Vehicular Volume

| Number of lanes for moving <br> traffic on each approach |  | Vehicles per hour on major street <br> (total of both approaches) |  |  | Vehicles per hour on higher-volume <br> minor-street approach (one direction only) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street | Minor Street | $100 \%^{\mathrm{a}}$ | $80 \%^{\mathrm{b}}$ | $70 \%^{\mathrm{e}}$ | $56 \%^{\mathrm{d}}$ | $100 \%^{\mathrm{a}}$ | $80 \%^{\mathrm{b}}$ | $70 \%^{\mathrm{e}}$ | $56 \%^{\mathrm{d}}$ |
| 1 | 1 | 500 | 400 | 350 | 280 | 150 | 120 | 105 | 84 |
| 2 or more | 1 | 600 | 480 | 420 | 336 | 150 | 120 | 105 | 84 |
| 2 or more | 2 or more | 600 | 480 | 420 | 336 | 200 | 160 | 140 | 112 |
| 1 | 2 or more | 500 | 400 | 350 | 280 | 200 | 160 | 140 | 112 |

Condition B-Interruption of Continuous Traffic

| Number of lanes for moving traffic on each approach |  | Vehicles per hour on major street (total of both approaches) |  |  |  | Vehicles per hour on higher-volume minor-street approach (one direction only) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street | Minor Street | 100\% ${ }^{\text {a }}$ | 80\% ${ }^{\text {b }}$ | 70\% | 56\% ${ }^{\text {d }}$ | 100\% ${ }^{\text {a }}$ | 80\% ${ }^{\text {b }}$ | 70\% | $56 \%{ }^{\text {d }}$ |
| 1 | 1 | 750 | 600 | 525 | 420 | 75 | 60 | 53 | 42 |
| 2 or more | 1 | 900 | 720 | 630 | 504 | 75 | 60 | 53 | 42 |
| 2 or more | 2 or more | 900 | 720 | 630 | 504 | 100 | 80 | 70 | 56 |
| 1 | 2 or more | 750 | 600 | 525 | 420 | 100 | 80 | 70 | 56 |

${ }^{\text {a }}$ Basic minimum hourly volume
${ }^{b}$ Used for combination of Conditions A and B after adequate trial of other remedial measures
${ }^{6}$ May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000
${ }^{d}$ May be used for combination of Conditions A and B after adequate trial of other remedial measures when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000

After applying the warrant criteria for Existing Conditions, zero of the twelve hours meet the criteria set for Warrant 1 A , five hours meet the criteria for Warrant 1 B , and zero hours meet the criteria for combination of Warrant $1 \mathrm{~A} \& 1 \mathrm{~B}$ of the Major and Minor street volumes set in the " $70 \%$ " conditions. Criteria 1 B is three hours short of meeting the warranting criteria.

## Warrant 1 is NOT MET.

## Warrant 2 - Four Hour Vehicular Volumes

The warrant is intended for locations where, for a brief period of the day, minor road traffic experiences excessive delays in attempting to enter or cross the major street. Warrant 2 requires that the combination of the major street traffic (total of both approaches) and minor street traffic (one direction only) reaches a designated minimum volume during any four hours of any average day.

Only two hours meet the guideline criteria, short of the four required in evaluation of Existing Conditions. Evaluation of Warrant 2 is illustrated in Figure 9.

Warrant 2 is NOT MET.

Figure 9: Warrant 2 - Four-Hour Vehicular Volume


## Warrant 3 - Peak Hour Vehicular Volumes

This warrant is intended to be used where large numbers of vehicles are attracted or discharged for brief periods and minor street traffic suffers excessive delay when entering or crossing the major street. Warrant 3 requires that the combination of the major street traffic (total of both approaches) and the minor street traffic (one approach only) reaches a designated minimum volume during any one hour of an average day.

For Existing Conditions, none of the twelve hours evaluated meet the criteria established for Warrant 3. Evaluation of Warrant 3 is illustrated in Figure 10.

Figure 10: Warrant 3 - Peak Hour Vehicular Volume


## Warrant 3 is NOT MET.

## Warrant 4 - Pedestrian Volume

The pedestrian volume signal warrant is intended for locations where traffic volumes on the major street are such that pedestrians experience excessive delay in crossing the major street. Warrant 4 requires a minimum of 75 pedestrians for each of any four hours or 93 pedestrians during the peak hour.

The volume of pedestrians at the intersection is far below the threshold required by the MUTCD.
Warrant 4 is NOT MET.

## Warrant 5 - School Crossing

This warrant is intended for application where school children must cross the major street is the principle reason to consider the installation of a traffic control signal.

A signal at the subject intersection does not serve to create a controlled school crossing.
Warrant 5 is NOT MET.

## Warrant 6 - Coordinated Signal System

This warrant is intended for intersections that fall within an existing coordinated signal system in order to maintain proper vehicle progression.

The subject intersection is isolated from any potential coordination with adjacent traffic signals.
Warrant 6 is NOT APPLICABLE.

## Warrant 7 - Crash Experience

This warrant is intended for application where the severity and frequency of crashes are the principle reasons to consider installing a traffic control signal. Warrant 7 is applicable where five or more crashes that are potentially preventable by the installation of a traffic signal have occurred a 12-month period and the intersection traffic volumes meet the 56\% column from MUTCD Table 4C-1.

Based upon an evaluation of the intersection crash data, there was not a period where five correctable right angle crashes occurred within a one year period. Four right angle crashes occurred between $10 / 14 / 17$ and $8 / 17 / 18$, one short of the initial threshold. An additional angle crash occurred on 5/27/17, constituting five crashes in a fifteen month period. Since August of 2018, there was one reported crash that occurred at the intersection that is potentially correctable by the installation of a traffic signal. Within the five year study period, eight potentially correctable right angle crashes have occurred at the intersection. If the initial correctable crash threshold were satisfied, the subsequent $56 \%$ volume criteria would be met and Warrant 7 would be met.

Warrant 7 is NOT MET.

## Warrant 8 - Roadway Network

A signal may be justified to encourage concentration and organization of traffic flow on a roadway network. According to the MUTCD, Warrant 8 can be considered when two or more major routes intersect and a minimum total entering volume of at least 1,000 vehicles during the peak hour of a typical weekday and has 5 -year projected traffic volumes that meet one or more of Warrants 1,2 , and 3.

The subject intersection does not involve the crossing of two major routes.
Warrant 8 is NOT APPLICABLE.

## Warrant 9 - Intersection Near a Grade Crossing

This warrant is intended for use at a location where the proximity to the intersection of a grade crossing on an intersection approach controlled by a stop or yield sign is the principal reason to consider installing a traffic control signal.

There is not a railroad crossing near the intersection that impacts traffic flow.

## Warrant 9 is NOT APPLICABLE.

None of the nine MUTCD warrants are satisfied for the intersection of Earlysville Road with Reas Ford Road and Earlysville Forest Drive. The heaviest side street movement at the intersection is the right turn from Reas Ford Road, and right turning traffic is generally only impeded by the queue of left turning traffic. Based upon review of the actual intersection conditions, the MUTCD traffic signal warranting criteria is not satisfied for the study intersection. As noted, If the initial correctable crash threshold were satisfied, Warrant 7 could be utilized to justify the installation of a traffic signal.

Copies of signal warrant analysis are included in Appendix D.

## AUXILIARY LANE ANALYSIS

Auxiliary turn lane analysis was performed for the intersection using the VDOT Access Management Design Standards for Entrances and Intersections, Revised January of 2021. These standards are based upon the AASHTO publication A Policy on Geometric Design of Highways and Streets.

Intersection traffic volume and design speed are the primary variables evaluated to determine the need for auxiliary lanes. Left turn lane warranting criteria is outlined in Figure 3-4 through Figure 3-9 from VDOT Access Management Manual and are shown in Appendix G.

Based upon evaluation of actual intersection conditions, the Earlysville Road northbound approach meets the criteria shown in Figure 3-5 during the PM peak hour with $10 \%$ left turns. The left turn warranting criteria is not met northbound in the AM peak hour and not for the southbound approach in either the AM or PM peak hour. In addition, a right turn taper is warranted on the Reas Ford Road eastbound approach during the AM peak hour. Table $\mathbf{1 2}$ provides a summary of the various potential turn lanes evaluated and whether VDOT warranting criteria is satisfied.

Table 12: Auxiliary Lane Analysis Summary

| Approach | Analysis Results |  |  |
| :---: | :---: | :---: | :---: |
|  |  | AM Peak Hour | PM Peak Hour |
| EB Approach (Reas Ford Road) | Right-Turn Lane | MET | NOT MET |
| WB Approach (Earlysville Forest Drive) | Right-Turn Lane | NOT MET | NOT MET |
| NB Approach (Earlysville Road) | Left-Turn Lane | NOT MET | MET |
|  | Right-Turn Lane | NOT MET | NOT MET |
| SB Approach (Earlysville Road) | Left-Turn Lane | NOT MET | NOT MET |
|  | Right-Turn Lane | NOT MET | NOT MET |

## CAPACITY ANALYSIS

The Highway Capacity Manual defines capacity as the maximum suitable flow rate at which vehicles reasonably can be expected to traverse a point during a specified time period. Capacity uses the measure of efficiency, Level-of-Service (LOS), to describe the traffic performance at intersections. LOS is defined for the overall intersection delay for signalized intersections. An acceptable LOS for a signalized intersection is considered to be LOS D or better (i.e. A, B, C or D).

At unsignalized intersections, the LOS is defined by the control delay for the movement that must yield right-of-way. It may be typical for stop-controlled minor streets to experience long delays during peak periods, while the majority of the traffic flows through the intersection on the major street travel unimpeded.

The procedures outlined in the Highway Capacity Manual; $6^{\text {th }}$ Edition were used as guidelines for the analysis of the study area intersections. This manual provides procedures for the analysis of both signalized and unsignalized intersections. LOS categories range from LOS " A " (best) to " F " (worst) as shown in Table 13.

Table 13: Level of Service Criteria

| Level of <br> Service | SIGNALIZED <br> Intersection <br> Control Delay <br> (sec/veh) | UNSIGNALIZED <br> Intersection <br> Control Delay <br> (sec/veh) | Intersection LOS Description |
| :--- | :--- | :--- | :--- |
| A | $\leq 10.0$ | $\leq 10.0$ | Free flow, insignificant delays. |
| B | $10.1-20.0$ | $10.1-15.0$ | Stable operation, minimal delays. |
| C | $20.1-35.0$ | $15.1-25.0$ | Stable operation, acceptable delays. |
| D | $35.1-55.0$ | $25.1-35.0$ | Restricted flow, common delays. |
| E | $55.1-80.0$ | $35.1-50.0$ | Maximum capacity, extended delays. Volumes at <br> or near capacity. Long queues form upstream <br> from intersection. |
| F | $>80.0$ | $>50.0$ | Forced flow, excessive delays. Represents <br> jammed conditions. Intersection operates below <br> capacity with low volumes. Queues may block <br> upstream intersections. |

LOS analysis was completed through the use of Synchro, version 10.3 and Sidra, version 9.0. These software packages categorize the LOS based on HCM methodology and criteria. According to industry standards, any signalized intersection or any approach of an unsignalized intersection is considered acceptable if the average delay is at LOS D or better with LOS A representing little or no delay. Any signalized intersection or approach with a LOS of E or F is considered substandard and may need solutions to improve the operational performance. Copies of the Synchro and Sidra reports are included in Appendix F .

## No Build Conditions (Existing Configuration)

Analysis was performed of the existing intersection configuration with two way stop control on the Reas Ford Road and Earlysville Forest Drive approaches. Analysis shows that the left turn movements on both Earlysville Road approaches operate at LOS A during both the AM and PM peak hours, which control operation on each mainline approach in the absence of exclusive turn lanes. The Reas Ford Road eastbound approach currently operates at LOS C during both the AM and PM peak hours while the Earlysville Forest Drive westbound approach currently operates at LOS D during the AM peak hour and LOS C during the PM peak hour under two way stop control.

## Alternative 1 - TWSC with Turn Lanes

Improvements included in Alternative $\mathbf{1}$ include construction of exclusive left turn lanes on both Earlysville Road approaches and construction of an exclusive right turn lane on the eastbound Reas Ford Road approach.

Following construction of the proposed exclusive auxiliary lanes, analysis indicates that the left turn movement on each Earlysville Road approach continues to operate at LOS A during both the AM and PM peak hours. The shared thru/right lane in each direction operates free flow traveling unimpeded through the intersection. The Reas Ford Road eastbound approach will continue to operate at LOS C during both the AM and PM peak hours with two way stop control. The Earlysville Forest Drive westbound approach will continue to operate at LOS D during the AM peak hour and LOS C during the PM peak hour with two way stop control.

## Alternative 2 - Traffic Signal Plus Turn Lanes

Improvements included in Alternative $\mathbf{2}$ include installation of a traffic signal and construction of exclusive left turn lanes on both Earlysville Road approaches as well as a right turn lane on the Reas Ford eastbound approach.

Following installation of a traffic signal and auxiliary lanes at the intersection, analysis indicates that the Earlysville Road southbound approach is expected to operate at LOS B during the AM peak hour and LOS A during the PM peak hour. The Earlysville Road northbound approach is expected to operate at LOS A during both the AM and PM peak hours. The Reas Ford Road eastbound approach to Earlysville Road is expected to improve to LOS B during both the AM and PM peak hours. The Earlysville Forest Drive westbound approach to improve to LOS B during both the AM and PM peak hours. The overall signalized intersection is expected to operate at LOS B during the AM peak hour and LOS A during the PM peak hour.

## Alternative 3 - Roundabout Conditions

Improvements included in Alternative $\mathbf{3}$ consist of conversion of the intersection to a single lane roundabout without any auxiliary or slip lanes. This analysis is assumed to be the same for a traditional roundabout or a mini roundabout.

Following construction of a single lane roundabout, analysis indicates that the Earlysville Road southbound approach is expected to operate at LOS A during both the AM and PM peak hours under
roundabout yield control. The Earlysville Road northbound approach is expected to operate at LOS A during both the AM and PM peak hours. The Reas Ford Road eastbound approach is expected to operate at LOS A during both the AM and PM peak hours. The Earlysville Forest Drive westbound approach is expected to operate at LOS A during both the AM and PM peak hours. The overall roundabout intersection is expected to operate at LOS A during both the AM and PM peak hours.

## Alternative 4 - Short-Term AWSC

Alternative 4 should be considered as a short-term interim option to address the angle crash pattern and is not evaluated as a long term intersection control option. Level of Service (LOS) analysis is shown as a measure of the anticipated operation of the intersection.

Following installation of All Way Stop Control (AWSC), analysis indicates that the Earlysville Road southbound approach would be expected to deteriorate to LOS D during the AM peak hour and LOS B during the PM peak hour. The Earlysville Road northbound approach would be expected to deteriorate to LOS B during the AM peak hour and LOS C during the PM peak hour. The Reas Ford Road eastbound approach is expected to improve to LOS B during both the AM and PM peak hours. The Earlysville Forest Drive westbound approach is expected to improve to LOS B during the AM peak hour and LOS A during the PM peak hour. The overall AWSC intersection is expected to operate at LOS C during both the AM and PM peak hours.

Table 14 provides a summary of the LOS results during the weekday AM and PM peak hours for Existing Conditions, Alternative 1 (Turn Lanes Only), Alternative 2 (Traffic Signal Plus Turn Lanes), and Alternative 3 (Single Lane Roundabout).

Figure 11 shows the LOS during the weekday AM and PM peak hours for the various alternatives evaluated study intersection.

| Intersection | Movement | No-Build Conditions |  |  |  | Alternative 1 (Turn Lanes Only) |  |  |  | Alternative 2 (Signal with TurnLanes) |  |  |  | Alternative 3/3B (Roundabouts) |  |  |  | Alternative 4 (AWSC) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak |  | PM Peak |  | AM Peak |  | PM Peak |  | AM Peak |  | PM Peak |  | AM Peak |  | PM Peak |  | AM Peak |  | PM Peak |  |
|  |  | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay |
| Intersection 1-Earlysville Road (Route 743) with Reas Ford Road /Earlysville Forest Drive (Route 660) | EB Left/Thru/Right | C | 18.4 | C | 17.7 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | A | 6.6 | A | 4.6 | B | 10.1 | B | 10.1 |
|  | EB Left/Thru | N/A | N/A | N/A | N/A | C | 21.6 | C | 23.9 | B | 15.3 | B | 12.7 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | EB Right-Turn | N/A | N/A | N/A | N/A | B | 13.5 | B | 10.3 | B | 14.6 | B | 11.3 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | EB Approach | C | 18.4 | C | 17.7 | C | 16.0 | C | 15.9 | B | 14.8 | B | 11.9 | A | 6.6 | A | 4.6 | B | 10.1 | B | 10.1 |
|  | WB Left/Thru/Right | D | 25.5 | C | 19.5 | D | 25.5 | C | 19.8 | B | 16.0 | B | 12.9 | A | 3.9 | A | 4.9 | B | 10.3 | A | 9.8 |
|  | WB Approach | D | 25.5 | C | 19.5 | D | 25.5 | C | 19.8 | B | 16.0 | B | 12.9 | A | 3.9 | A | 4.9 | B | 10.3 | A | 9.8 |
|  | NB Left-Turn | A | 8.9 | A | 8.0 | A | 8.9 | A | 8.0 | A | 6.8 | A | 6.3 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | NB Thru/Right | N/A | N/A | N/A | N/A | N/A | FREE | N/A | FREE | A | 6.1 | A | 9.4 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | NB Left/Thru | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | B | 11.3 | D | 25.2 |
|  | NB Right-Turn | N/A | FREE | N/A | FREE | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | A | 7.9 | A | 7.6 |
|  | NB Left/Thru/Right | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | A | 4.2 | A | 7.1 | N/A | N/A | N/A | N/A |
|  | NB Approach | N/A | 1.9 | N/A | 0.9 | N/A | 1.9 | N/A | 0.9 | A | 6.2 | A | 9.1 | A | 4.2 | A | 7.1 | B | 11.1 | C | 23.9 |
|  | SB Left-Turn | A | 7.5 | A | 8.5 | A | 7.5 | A | 8.5 | A | 5.7 | A | 7.2 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | SB Thru/Right | N/A | N/A | N/A | N/A | N/A | FREE | N/A | FREE | B | 10.3 | A | 8.9 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Existing Four legged unsignalized intersection with stop control on Reas Ford Road \& Earlysville Forest Drive | SB Left/Thru/Right | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | A | 8.5 | A | 5.2 | D | 29.0 | B | 12.9 |
|  | SB Approach | N/A | 0.2 | N/A | 0.4 | N/A | 0.2 | N/A | 0.4 | B | 10.2 | A | 8.8 | A | 8.5 | A | 5.2 | D | 29.0 | B | 12.9 |
|  | Overall | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | B | 10.4 | A | 9.5 | A | 7.1 | A | 6.2 | C | 22.0 | C | 18.5 |



## QUEUING ANALYSIS

Queuing analysis was performed at the study intersection during the weekday AM and PM peak hours using the SimTraffic micro-simulation model, which is a simulation complement to the Synchro traffic analysis models utilized for the capacity analysis. The queuing calculations produced by SimTraffic are acknowledged within the industry to be a realistic replication of actual conditions. Each simulation model was seeded for 10 minutes and recorded for 60 minutes. The simulation was run five times and then averaged to estimate the $95^{\text {th }}$ percentile queuing for all scenarios. Queuing analysis was performed for roundabout analysis during the weekday AM and PM peak hours using Sidra modeling. The queuing calculations produced by Sidra are acknowledged within the industry to be a realistic replication of actual conditions for roundabout intersections.

## No Build Conditions (Existing Configuration)

The queuing analysis indicates that no existing turning movements currently exceed the available storage length or impeded other traffic movements during the peak periods analyzed.

## Alternative 1 - TWSC with Turn Lanes

Queuing analysis indicates that all conditions described in the No Build Conditions are expected to continue with similar queuing following construction of exclusive left turn lanes on Earlysville Road and a right turn lane on the Reas Ford eastbound approach. Queue lengths are reduced in comparison to No Build Conditions.

## Alternative 2 - Traffic Signal Plus Turn Lanes

With the installation of a traffic signal, short queues are created on the Earlysville southbound and northbound approaches with the installation of a traffic signal. The queues are not substantial and are not anticipated to inhibit access to proposed exclusive left turn lanes. The projected queue is 129 feet northbound during the PM peak hour and 140 feet southbound during the AM peak hour. Queuing on the side road approaches is similar to No Build Conditions.

## Alternative 3 - Roundabout

Queuing analysis indicates that queuing is anticipated to be minimal with roundabout operation. This analysis is assumed to be the same for a traditional roundabout and a mini roundabout. The most significant queue is the Earlysville southbound approach during AM peak hour and Earlysville northbound approach during PM peak hour. The projected queue is 110 feet southbound during the AM peak hour and 91 feet northbound during the PM peak hour.

## Alternative 4 - Short-Term AWSC

Queuing analysis indicates that queuing is anticipated to be a more significant issue with AWSC. The most significant queue is the Earlysville southbound approach during AM peak hour and Earlysville northbound approach during PM peak hour. The projected queue is 129 feet northbound during the PM peak hour and 163 feet southbound during the AM peak hour.

Earlysville Road / Reas Ford Road Intersection Study

Table 15 presents the $95 \%$ queuing results and Figure 12 provides an illustration of anticipated queuing for the weekday AM and PM peak periods for the alternatives evaluated. Copies of the SimTraffic and Sidra analyses outputs are included in Appendix F.

Table 15: Queueing Analysis Summary

| Intersection | Movement | Existing <br> Storage <br> Length (ft) | No-Build |  | Proposed <br> Storage <br> Length (ft) | Alternative 1 |  | Proposed <br> Storage <br> Length (ft) | Alternative 2 |  | Proposed <br> Storage <br> Length (ft) | Alternative 3/3B |  | Existing <br> Storage <br> Length (ft) | Alternative 4 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM | PM |  | AM | PM |  | AM | PM |  | AM | PM |  | AM | PM |
| Intersection 1 - Earlysville Road (Route | EB Left/Thru/Right | -- | 64 | 66 | N/A | N/A | N/A | N/A | N/A | N/A | -- | 24 | 14 | -- | 50 | 49 |
| 743) with Reas Ford Road (Route | EB Left/Thru | N/A | N/A | N/A | -- | 38 | 39 | -- | 41 | 47 | N/A | N/A | N/A | N/A | N/A | N/A |
| 660)/Earlysville Forest Drive | EB Right-Turn | N/A | N/A | N/A | 125 | 45 | 44 | 125 | 49 | 39 | N/A | N/A | N/A | N/A | N/A | N/A |
|  | WB Left/Thru/Right | -- | 43 | 37 | -- | 45 | 37 | -- | 53 | 36 | -- | 9 | 9 | -- | 35 | 28 |
|  | NB Left/Thru | -- | 31 | 53 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | -- | 58 | 129 |
|  | NB Right-Turn | 100 | 0 | 0 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | 100 | 27 | 57 |
|  | NB Left-Turn | N/A | N/A | N/A | 125 | 36 | 38 | 125 | 40 | 46 | N/A | N/A | N/A | N/A | N/A | N/A |
|  | NB Thru/Right | N/A | N/A | N/A | -- | 4 | 20 | -- | 71 | 129 | N/A | N/A | N/A | N/A | N/A | N/A |
|  | NB Left/Thru/Right | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A | -- | 25 | 91 | N/A | N/A | N/A |
|  | SB Left/Thru/Right | -- | 17 | 31 | N/A | N/A | N/A | N/A | N/A | N/A | -- | 110 | 41 | -- | 163 | 77 |
|  | SB Left-Turn | N/A | N/A | N/A | 125 | 8 | 21 | 125 | 22 | 27 | N/A | N/A | N/A | N/A | N/A | N/A |
|  | SB Thru/Right | N/A | N/A | N/A | -- | 5 | 9 | -- | 140 | 98 | N/A | N/A | N/A | N/A | N/A | N/A |



## SAFETY ANALYSIS

For purposes of comparing benefit vs cost for potential intersection improvement alternatives, evaluation of economic cost of safety performance resulting from motor vehicle crashes at the intersection was performed utilizing accepted FHWA safety analysis procedures. Crash Modification Factors (CMF's) depicting the proposed alternatives were selected from the VDOT Preferred CMF List, which is provided in Appendix $\mathbf{H}$ for reference. A summary of the CMF's utilized is illustrated in Table 16.

Table 16: Utilized CMF Summary

| Countermeasure | CMF \# | Crash Type | K | A | BC | 0 | Service Life | Reference |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Add Left-Turn Lane to Major Approach of 3-Leg Stop Controlled Intersection | 1 | ALL | 0.56 | 0.56 | 0.56 | 0.56 | 20 YRS | HSM Table 11-22 |
| Convert Stop-Controlled Intersection to Signalized Intersection | 2 | ALL | 0.642 | 0.642 | 0.642 | 0.639 | 20 YRS | CMF ID: 7983, 7986 |
| Convert Stop-Controlled Intersection to Roundabout | 3 | ALL | 0.56 | 0.18 | 0.18 | 0.56 | 20 YRS | CMF ID: 227, 228 |
| Convert Minor Stop-Control to All-Way Stop Control | 4 | ALL | 0.23 | 0.23 | 0.23 | 0.319 | 20 YRS | CMF ID: 3127, 3128 |

The selected CMF's were utilized to forecast the safety performance of each alternative as a means to estimate the anticipated benefit in terms of reduction of injury crashes. The CMF's shown in Table $\mathbf{1 6}$ are applied to recent crash data to predict the expected crash reduction from each alternative by severity. Safety performance is a key factor of this study, as all alternatives including No Build operate at acceptable level of service (LOS). For that reason, Benefit/Cost ( $B / C$ ) is expressed simply in terms of safety performance based upon economic cost based upon injury severity over 20 years compared with cost of construction. Table 17 shows the annualized crash performance of the intersection based upon recent data and application of the CMF's. Each value reflects the number of crashes expected by severity annually following construction of each alternative.

Table 17: Annualized CMF Application

| Crash Severity | Number of Crashes | Annualized Crashes | CMF 1 - ALT 1 | CMF 2/CMF 1 ALT 2 | CMF 3 -ALT 3/3B | CMF 4 - ALWSC |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Fatal Crashes | 0 | 0 | 0.00 | 0.00 | 0.00 |  |
| Class A Crashes | 2 | 0.40 | 0.22 | 0.14 | 0.07 | 0.09 |
| Class B Crashes | 6 | 1.20 | 0.67 | 0.43 | 0.22 | 0.00 |
| Class C Crashes | 0 | 0.00 | 0.00 | 0.00 | 0.00 |  |
| Property Damage Only Crashes | 7 | 1.40 | 0.78 | 0.57 | 0.78 | 0.45 |
| Total | 15 | 3.00 | 1.68 | 1.15 | 0.07 | 0.8 |

Utilizing the forecast annual crashes by severity along with the monetized crash value by severity established by FHWA, total safety performance was calculated from a baseline of No Build based upon recent crash history. Safety performance is monetized as a way to measure the effectiveness of constrained financial resources to achieve the most benefit. Table 18 illustrates the total forecast 20 year cost of motor vehicle crashes for each alternative. Since Alternative 4 (All Way Stop Control) is shown as a potential interim or short-term solution only, it is not applicable to present a 20 year service life for this scenario.

Table 18: Forecast Monetized Safety Performance by Alternative

| Crash Severity | Monetized Crash <br> Value (2021) | NO BUILD | CMF 1-ALT1 | CMF 1/2 - ALT 2 | CMF 3-ALT3 | CMF 4-ALT4 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Fatal Crashes | $\$ 5,861,850.00$ | $\$ 0.00$ | $\$ 0.00$ | $\$ 0.00$ | $\$ 0.00$ |  |
| Class A Crashes | $\$ 315,837.00$ | $\$ 126,334.80$ | $\$ 70,747.49$ | $\$ 45,419.89$ | $\$ 22,740.26$ | $\$ 29,057.00$ |
| Class B Crashes | $\$ 115,515.00$ | $\$ 138,618.00$ | $\$ 77,626.08$ | $\$ 49,835.94$ | $\$ 24,951.24$ | $\$ 31,882.14$ |
| Class C Crashes | $\$ 65,653.00$ | $\$ 0.00$ | $\$ 0.00$ | $\$ 0.00$ | $\$ 0.00$ | $\$ 0.00$ |
| Property Damage Only Crashes | $\$ 10,820.00$ | $\$ 15,148.00$ | $\$ 8,482.88$ | $\$ 6,214.29$ | $\$ 8,482.88$ | $\$ 29,320.63$ |
| Total |  | $\$ 280,100.80$ | $\$ 156,856.45$ | $\$ 101,470.12$ | $\$ 56,174.38$ | $\$ 90,259.77$ |
| 20 Year Safety Cost |  | $\$ 8,340,869.63$ | $\$ 4,670,886.99$ | $\$ 3,021,587.26$ | $\$ 1,672,766.42$ | $n / a$ |

As shown through the application of the CMF's, Alternative 3 (Roundabout) would be anticipated to result in the largest reduction in overall crashes at the intersection. Alternative 3 , however, also is the most expensive and the most impactful to adjacent property owners and the community. Further evaluation of anticipated monetized annual safety performance over a 20 year service life was compared to the estimated cost of construction for each alternative. The 20 year performance assumes annual inflation of $4 \%$ for cost of each crash type. By comparison of the forecast crash reduction with estimated cost, Alternative 3B (Mini Roundabout) was found to achieve the highest benefit/cost ratio of 2.7. A summary of $\mathrm{B} / \mathrm{C}$ analysis is illustrated in Table 19.

## Table 19: Benefit/Cost Comparison

| Scenario | 20 YR safety cost | ALT Cost | Crash Savings | B/C |
| :--- | ---: | ---: | ---: | ---: |
| NO Build | $\$ 8,340,870$ | $\$ 0$ | $\$ 0$ | 0 |
| ALT 1 | $\$ 4,670,887$ | $\$ 1,903,345$ | $\$ 3,669,983$ | 1.9 |
| ALT 2 | $\$ 3,021,587$ | $\$ 2,330,995$ | $\$ 5,319,282$ | 2.3 |
| ALT 3 | $\$ 1,672,766$ | $\$ 4,267,066$ | $\$ 6,668,103$ | 1.6 |
| ALT 3B | $\$ 1,672,766$ | $\$ 2,430,144$ | $\$ 6,668,103$ | 2.7 |
| ALT 4 | n/a | n/a | n/a | n/a |

Safety analysis was performed on the total number of crashes reported to occur for the five year period available from July 1, 2016 to June 30,2021 . Of the 15 crashes reported to occur, 11 occurred from July of 2016 to through 2018. Four crashes were reported to occur from January of 2019 through June of 2021. The safety analysis assumes crashes are linear for the reported time period. The data shows that fewer crashes have occurred in the most recent 30 month portion of the study, including only one crash after additional traffic control devices were installed.

## CONCLUSIONS

This report summarizes evaluation of potential intersection improvement alternatives at the intersection of Earlysville Road (Route 743) with Reas Ford Road (Route 660) and Earlysville Forest Drive (Route 660) in Earlysville, Albemarle County. Albemarle County and The Virginia Department of Transportation (VDOT) previously identified safety concerns at the intersection of Earlysville Road and Reas Ford Road evidenced by crash data, and subsequently evaluated various options for modification of the intersection.

This study was initiated to evaluate the potential for intersection modification based upon previously identified safety concerns at the intersection. Evaluation of the collected data shows that the intersection currently operates at an acceptable Level of Service (LOS), with modest delay quantified on the side street approaches to the intersection. The intersection currently operates at acceptable LOS.

The most important operational issue at the intersection is the occurrence of right angle crashes at the intersection. Eight angle crashes were reported to occur at the intersection in the five year period evaluated, which resulted in 16 injuries including two serious injuries (Type A) and 11 significant injuries (Type B). All four alternatives evaluated are anticipated to reduce the occurrence of crashes, with the Roundabout and Traffic Signal options anticipated to address the angle crash pattern most significantly. The traditional roundabout, however, is the most expensive alternative and would have significant impacts in terms of right of way, utilities, and temporary traffic control. While the mini roundabout results in the highest benefit vs cost ratio in terms of safety impact, it is likely inappropriate for the intersection.

Based upon evaluation of the collected data and Alternatives evaluation, the following recommendations are made in regard to the intersection of Earlysville Road with Reas Ford Road and Earlysville Forest Drive:

- Based upon assessment of the entirety of the collected data, major intersection reconfiguration is not necessary at this time, and the No Build Alternative is appropriate. The intersection currently operates at adequate Level of Service (LOS) and the occurrence of crashes at the intersection has declined in the most recent 30 month period of the study.
- Due to the identified pattern of right angle crashes from 2016 to 2018, the intersection should continue to be monitored closely to determine if the recent reduction of intersection crashes following implementation of low cost safety improvements endures.
- If right angle crashes persist or increase where five or more occur in a 12 month period, a traffic signal can be installed in accordance with MUTCD Warrant Seven (Crash Safety). If safety performance or future traffic volume indicate that intersection control needs to be enhanced, a traffic signal or a roundabout both would provide adequate Level of Service.
- A mini roundabout appears to be inappropriate at this intersection due to volume, truck traffic, and prevailing speed. If a roundabout is considered in the future, a traditional roundabout is more appropriate for the conditions at this location.
- Ideally, construct auxiliary lanes including left turn lanes in both directions of Earlysville Road and a right turn lane on Reas Ford Road. VDOT warranting criteria based upon AASHTO is satisfied for these approaches. These auxiliary lanes, however, do not address the right angle crash pattern at the intersection or appreciably improve Level of Service.


## Appendix A

## Study Area Photos



Reas Ford Road Eastbound Approach to Earlysville Road



Earlysville Forest Drive Westbound Approach to Earlysville Road



Earlysville Road Northbound Approach to Reas Ford Road/Earlysville Forest Drive



Earlysville Road Southbound Approach to Reas Ford Road/Earlysville Forest Drive



Looking North from Reas Ford Road


Looking South from Reas Ford Road


Looking North from Earlysville Forest Drive


Looking South from Earlysville Forest Drive

## Appendix B

## Traffic Data

## Appendix B-1

## Turning Movement Counts

VEHICLE AND PEDESTRIAN VOLUME SUMMARY

| COUNT LOCATION |  |
| :--- | :--- |
| CITY | Earlysville |
| STATE | VA |
| DATE | 9/23/2021 |
| INTERSECTION | Int 1: Earlysville Road (CR 743) @ Reas <br> Ford Road (SR 660)/Earlysville Forest <br> Drive |
| COUNT BY | AMT |


| STREET | Earlysville Forest Dr <br> From North |  |  |  | SR 660 |  |  |  | CR 743 |  |  |  |  | CR 743 |  |  | Total |  |  | PEAK HR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TIME | L | T | R | TOT | L | T | R | TOT | L | T | R | TOT | L | T | R | TOT | N-S | E-W | ALL |  |
| 0700-0715 | 1 | 1 | 0 | 2 | 1 | 0 | 4 | 5 | 7 | 17 | 1 | 25 | 0 | 103 | 8 | 111 | 7 | 136 | 143 | 143 |
| 0715-0730 | 9 | 0 | 1 | 10 | 2 | 1 | 18 | 21 | 4 | 17 | 3 | 24 | 2 | 107 | 6 | 115 | 31 | 139 | 170 | 313 |
| 0730-0745 | 8 | 0 | 5 | 13 | 11 | 0 | 17 | 28 | 7 | 39 | 2 | 48 | 4 | 114 | 7 | 125 | 41 | 173 | 214 | 527 |
| 0745-0800 | 10 | 4 | 1 | 15 | 11 | 1 | 18 | 30 | 11 | 41 | 2 | 54 | 3 | 138 | 15 | 156 | 45 | 210 | 255 | 782 |
| 0800-0815 | 13 | 3 | 4 | 20 | 6 | 0 | 18 | 24 | 10 | 26 | 2 | 38 | 2 | 111 | 9 | 122 | 44 | 160 | 204 | 843 |
| 0815-0830 | 16 | 0 | 2 | 18 | 1 | 0 | 13 | 14 | 8 | 21 | 3 | 32 | 5 | 126 | 5 | 136 | 32 | 168 | 200 | 873 |
| 0830-0845 | 11 | 0 | 1 | 12 | 7 | 1 | 15 | 23 | 10 | 35 | 3 | 48 | 4 | 106 | 0 | 110 | 35 | 158 | 193 | 852 |
| 0845-0900 | 11 | 0 | 1 | 12 | 5 | 2 | 15 | 22 | 9 | 45 | 5 | 59 | 3 | 79 | 6 | 88 | 34 | 147 | 181 | 778 |
| 0900-0915 | 14 | 0 | 0 | 14 | 3 | 0 | 9 | 12 | 14 | 41 | 5 | 60 | 3 | 63 | 7 | 73 | 26 | 133 | 159 | 733 |
| 0915-0930 | 8 | 0 | 1 | 9 | 5 | 0 | 6 | 11 | 6 | 40 | 4 | 50 | 2 | 47 | 3 | 52 | 20 | 102 | 122 | 655 |
| 0930-0945 | 6 | 0 | 2 | 8 | 1 | 2 | 8 | 11 | 10 | 36 | 2 | 48 | 1 | 54 | 6 | 61 | 19 | 109 | 128 | 590 |
| 0945-1000 | 8 | 1 | 1 | 10 | 5 | 1 | 7 | 13 | 7 | 34 | 0 | 41 | 2 | 57 | 7 | 66 | 23 | 107 | 130 | 539 |
| 1000-1015 | 2 | 2 | 2 | 6 | 5 | 0 | 7 | 12 | 6 | 42 | 4 | 52 | 1 | 50 | 4 | 55 | 18 | 107 | 125 | 505 |
| 1015-1030 | 7 | 2 | 3 | 12 | 4 | 0 | 5 | 9 | 11 | 52 | 3 | 66 | 3 | 55 | 3 | 61 | 21 | 127 | 148 | 531 |
| 1030-1045 | 8 | 0 | 1 | 9 | 4 | 1 | 8 | 13 | 7 | 52 | 2 | 61 | 1 | 57 | 5 | 63 | 22 | 124 | 146 | 549 |
| 1045-1100 | 4 | 1 | 3 | 8 | 3 | 1 | 8 | 12 | 5 | 39 | 8 | 52 | 1 | 52 | 3 | 56 | 20 | 108 | 128 | 547 |
| 1100-1115 | 9 | 1 | 4 | 14 | 0 | 4 | 8 | 12 | 10 | 34 | 7 | 51 | 0 | 37 | 6 | 43 | 26 | 94 | 120 | 542 |
| 1115-1130 | 8 | 1 | 3 | 12 | 0 | 0 | 6 | 6 | 7 | 43 | 3 | 53 | 3 | 42 | 5 | 50 | 18 | 103 | 121 | 515 |
| 1130-1145 | 12 | 1 | 1 | 14 | 6 | 0 | 12 | 18 | 3 | 47 | 4 | 54 | 6 | 65 | 6 | 77 | 32 | 131 | 163 | 532 |
| 1145-1200 | 9 | 3 | 6 | 18 | 8 | 1 | 12 | 21 | 10 | 34 | 10 | 54 | 3 | 48 | 5 | 56 | 39 | 110 | 149 | 553 |
| 1200-1215 | 8 | 0 | 6 | 14 | 6 | 1 | 11 | 18 | 14 | 46 | 4 | 64 | 1 | 39 | 3 | 43 | 32 | 107 | 139 | 572 |
| 1215-1230 | 5 | 0 | 3 | 8 | 3 | 0 | 11 | 14 | 8 | 67 | 4 | 79 | 1 | 55 | 3 | 59 | 22 | 138 | 160 | 611 |
| 1230-1245 | 6 | 0 | 2 | 8 | 3 | 2 | 13 | 18 | 10 | 47 | 4 | 61 | 4 | 58 | 3 | 65 | 26 | 126 | 152 | 600 |
| 1245-1300 | 6 | 1 | 7 | 14 | 5 | 1 | 8 | 14 | 9 | 41 | 6 | 56 | 3 | 50 | 7 | 60 | 28 | 116 | 144 | 595 |
| 1300-1315 | 9 | 1 | 3 | 13 | 2 | 4 | 13 | 19 | 6 | 52 | 2 | 60 | 5 | 46 | 3 | 54 | 32 | 114 | 146 | 602 |
| 1315-1330 | 5 | 0 | 2 | 7 | 5 | 1 | 10 | 16 | 10 | 52 | 6 | 68 | 1 | 65 | 3 | 69 | 23 | 137 | 160 | 602 |
| 1330-1345 | 4 | 2 | 4 | 10 | 0 | 1 | 16 | 17 | 7 | 54 | 8 | 69 | 5 | 55 | 1 | 61 | 27 | 130 | 157 | 607 |
| 1345-1400 | 10 | 0 | 11 | 21 | 3 | 2 | 15 | 20 | 11 | 53 | 6 | 70 | 6 | 52 | 2 | 60 | 41 | 130 | 171 | 634 |
| 1400-1415 | 12 | 1 | 2 | 15 | 6 | 2 | 12 | 20 | 10 | 54 | 6 | 70 | 2 | 42 | 5 | 49 | 35 | 119 | 154 | 642 |
| 1415-1430 | 6 | 1 | 3 | 10 | 7 | 0 | 10 | 17 | 18 | 68 | 12 | 98 | 3 | 63 | 1 | 67 | 27 | 165 | 192 | 674 |
| 1430-1445 | 6 | 2 | 2 | 10 | 3 | 2 | 6 | 11 | 4 | 53 | 6 | 63 | 2 | 56 | 11 | 69 | 21 | 132 | 153 | 670 |
| 1445-1500 | 6 | 0 | 5 | 11 | 3 | 0 | 10 | 13 | 16 | 48 | 10 | 74 | 5 | 79 | 8 | 92 | 24 | 166 | 190 | 689 |
| 1500-1515 | 6 | 1 | 4 | 11 | 4 | 2 | 7 | 13 | 18 | 77 | 7 | 102 | 1 | 75 | 3 | 79 | 24 | 181 | 205 | 740 |
| 1515-1530 | 8 | 1 | 4 | 13 | 8 | 1 | 14 | 23 | 8 | 64 | 9 | 81 | 1 | 60 | 4 | 65 | 36 | 146 | 182 | 730 |
| 1530-1545 | 5 | 2 | 2 | 9 | 8 | 1 | 17 | 26 | 13 | 57 | 6 | 76 | 3 | 87 | 5 | 95 | 35 | 171 | 206 | 783 |
| 1545-1600 | 11 | 0 | 1 | 12 | 12 | 0 | 11 | 23 | 13 | 79 | 10 | 102 | 1 | 80 | 7 | 88 | 35 | 190 | 225 | 818 |
| 1600-1615 | 3 | 2 | 5 | 10 | 6 | 2 | 7 | 15 | 14 | 105 | 12 | 131 | 2 | 90 | 9 | 101 | 25 | 232 | 257 | 870 |
| 1615-1630 | 9 | 1 | 8 | 18 | 9 | 1 | 13 | 23 | 14 | 101 | 11 | 126 | 5 | 67 | 5 | 77 | 41 | 203 | 244 | 932 |
| 1630-1645 | 9 | 0 | 4 | 13 | 8 | 1 | 19 | 28 | 15 | 112 | 17 | 144 | 2 | 53 | 11 | 66 | 41 | 210 | 251 | 977 |
| 1645-1700 | 4 | 1 | 5 | 10 | 10 | 2 | 17 | 29 | 15 | 126 | 1 | 142 | 4 | 50 | 9 | 63 | 39 | 205 | 244 | 996 |
| 1700-1715 | 9 | 0 | 5 | 14 | 8 | 1 | 14 | 23 | 14 | 116 | 15 | 145 | 2 | 48 | 5 | 55 | 37 | 200 | 237 | 976 |
| 1715-1730 | 7 | 1 | 3 | 11 | 9 | 0 | 13 | 22 | 25 | 118 | 19 | 162 | 0 | 47 | 7 | 54 | 33 | 216 | 249 | 981 |
| 1730-1745 | 4 | 2 | 1 | 7 | 11 | 2 | 16 | 29 | 16 | 141 | 12 | 169 | 0 | 50 | 3 | 53 | 36 | 222 | 258 | 988 |
| 1745-1800 | 6 | 1 | 1 | 8 | 8 | 1 | 11 | 20 | 15 | 115 | 9 | 139 | 1 | 49 | 3 | 53 | 28 | 192 | 220 | 964 |
| 1800-1815 | 2 | 0 | 1 | 3 | 8 | 0 | 12 | 20 | 11 | 87 | 13 | 111 | 3 | 45 | 7 | 55 | 23 | 166 | 189 | 916 |
| 1815-1830 | 4 | 0 | 2 | 6 | 7 | 1 | 11 | 19 | 12 | 87 | 4 | 103 | 0 | 44 | 2 | 46 | 25 | 149 | 174 | 841 |
| 1830-1845 | 8 | 1 | 0 | 9 | 4 | 1 | 10 | 15 | 9 | 70 | 7 | 86 | 0 | 51 | 3 | 54 | 24 | 140 | 164 | 747 |
| 1845-1900 | 2 | 1 | 1 | 4 | 3 | 0 | 6 | 9 | 13 | 42 | 12 | 67 | 2 | 40 | 0 | 42 | 13 | 109 | 122 | 649 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak HR AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 0730-0830 | 47 | 7 | 12 | 66 | 29 | 1 | 66 | 96 | 36 | 127 | 9 | 172 | 14 | 489 | 36 | 539 | 162 | 711 | 873 |  |
| Peak HR PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1600-1700 | 25 | 4 | 22 | 51 | 33 | 6 | 56 | 95 | 58 | 444 | 41 | 543 | 13 | 260 | 34 | 307 | 146 | 850 | 996 |  |
| AM PHF | 0.825 |  |  |  | 0.800 |  |  |  | 0.796 |  |  |  | 0.864 |  |  |  | 0.856 |  |  |  |
| PM PHF | 0.708 |  |  |  | 0.819 |  |  |  | 0.943 |  |  |  | 0.760 |  |  |  | 0.969 |  |  |  |

VEHICLE AND PEDESTRIAN VOLUME SUMMARY

| COUNT LOCATION |  |
| :--- | :--- |
| CITY | Earlysville |
| STATE | VA |
| DATE | 9/23/2021 |
| INTERSECTION | Int 1: Earlysville Road (CR 743) @ Reas <br> Ford Road (SR 660)/Earlysville Forest <br> Drive |
| COUNT BY | AMT |



| COUNT LOCATION |  |
| :--- | :--- |
| CITY | Earlysville |
| STATE | VA |
| DATE | $9 / 23 / 2021$ |
| INTERSECTION | Int 1: Earlysville Road (CR 743) @ <br> Reas Ford Road (SR 660)/Earlysville <br> Forest Drive |
| COUNT BY | AMT |

Non-Vehicle Traffic
Thursday - 12 Hour Count

| STREET | Earlysville Forest Dr |  |  | SR 660 |  |  | CR 743 |  |  | CR 743 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | From North |  |  | From South |  |  | From East |  |  | From West |  |  |
| TIME | School Children | Pedestrians | Bicycles | School Children | Pedestrians | Bicycles | School Children | Pedestrians | Bicycles | School Children | Pedestrians | Bicycles |
| 0700-0715 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 |
| 0715-0730 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 1 | 0 |
| 0730-0745 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| 0745-0800 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 0800-0815 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 0 |
| 0815-0830 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0830-0845 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | , | 0 | 1 | 0 |
| 0845-0900 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 1 | 0 |
| 0900-0915 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 3 | 0 | 0 | 2 | 0 |
| 0915-0930 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 |
| 0930-0945 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| 0945-1000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| 1000-1015 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 0 | 0 | 0 | 0 |
| 1015-1030 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 3 | 0 |
| 1030-1045 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 1 |
| 1045-1100 | 0 | 0 | 0 | 0 | 0 | 3 | 1 |  | 0 | 0 | 0 | 1 |
| 1100-1115 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 1 | 0 | 0 | 2 | 0 |
| 1115-1130 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 3 | 1 |
| 1130-1145 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 2 | 0 |
| 1145-1200 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 2 | 0 |
| 1200-1215 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 1215-1230 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 |
| 1230-1245 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 2 | 0 | 0 | 1 | 0 |
| 1245-1300 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 1 | 1 |
| 1300-1315 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 1 | 0 | 0 | 3 | 0 |
| 1315-1330 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 0 | 0 | 2 | 0 |
| 1330-1345 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 |
| 1345-1400 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 1 |
| 1400-1415 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 0 |
| 1415-1430 | 0 | 0 | 0 | 0 | 0 | 2 | 5 | 2 | 0 | 0 | 3 | 0 |
| 1430-1445 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 1 | 0 | 0 | 0 | 0 |
| 1445-1500 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 4 | 0 |
| 1500-1515 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 2 | 0 |
| 1515-1530 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 |
| 1530-1545 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 0 |
| 1545-1600 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 1 | 0 |
| 1600-1615 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 |
| 1615-1630 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1630-1645 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 1 | 1 |
| 1645-1700 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 1 |
| 1700-1715 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |
| 1715-1730 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1730-1745 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| 1745-1800 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1800-1815 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1815-1830 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1830-1845 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 1 | 0 |
| 1845-1900 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Peak HR AM |  |  |  |  |  |  |  |  |  |  |  |  |
| 0730-0830 | 0 | 0 | 1 | 0 | 0 | 3 | 1 | 3 | 0 | 0 | 2 | 0 |
| Peak HR PM |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1600-1700 | 0 | 0 | 0 | 0 | 0 | 4 | 3 | 1 | 0 | 1 | 1 | 2 |



## Appendix C

## Crash Data



## Appendix D

## Signal Warrant Analysis

## Appendix D-1

## Warrant 1: Eight-Hour Warrant 2021 Existing Conditions

VEHICLE AND PEDESTRIAN VOLUME SUMMARY

| COUNT LOCATION |  |
| :--- | :--- |
| CITY | Earlysville |
| STATE | VA |
| DATE | $9 / 23 / 2021$ |
| INTERSECTION | Int 1: Earlysville Road (CR 743) @ Reas Ford Road <br> (SR 660)/Earlysville Forest Drive |
| COUNT BY | AMT |

All Vehicles
Thursday - 12 Hour Count

| STREET | Earlysville Forest Dr <br> From North |  |  |  |  | SR 660 |  |  |  |  | CR 743 |  |  |  | CR 743 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | From East | From West |  |  |  |
| TIME | L | T | R | R* | TOT |  |  |  |  |  | L | T | R | R* | TOT | L | T | R | TOT | L | T | R | TOT |
| 0700-0715 | 1 | 1 | 0 | 0 | 2 | 1 | 0 | 4 | 2 | 3 | 7 | 17 | 1 | 25 | 0 | 103 | 8 | 111 |
| 0715-0730 | 9 | 0 | 1 | 1 | 10 | 2 | 1 | 18 | 11 | 14 | 4 | 17 | 3 | 24 | 2 | 107 | 6 | 115 |
| 0730-0745 | 8 | 0 | 5 | 3 | 11 | 11 | 0 | 17 | 10 | 21 | 7 | 39 | 2 | 48 | 4 | 114 | 7 | 125 |
| 0745-0800 | 10 | 4 | 1 | 1 | 15 | 11 | 1 | 18 | 11 | 23 | 11 | 41 | 2 | 54 | 3 | 138 | 15 | 156 |
| 0800-0815 | 13 | 3 | 4 | 2 | 18 | 6 | 0 | 18 | 11 | 17 | 10 | 26 | 2 | 38 | 2 | 111 | 9 | 122 |
| 0815-0830 | 16 | 0 | 2 | 1 | 17 | 1 | 0 | 13 | 8 | 9 | 8 | 21 | 3 | 32 | 5 | 126 | 5 | 136 |
| 0830-0845 | 11 | 0 | 1 | 1 | 12 | 7 | 1 | 15 | 9 | 17 | 10 | 35 | 3 | 48 | 4 | 106 | 0 | 110 |
| 0845-0900 | 11 | 0 | 1 | 1 | 12 | 5 | 2 | 15 | 9 | 16 | 9 | 45 | 5 | 59 | 3 | 79 | 6 | 88 |
| 0900-0915 | 14 | 0 | 0 | 0 | 14 | 3 | 0 | 9 | 5 | 8 | 14 | 41 | 5 | 60 | 3 | 63 | 7 | 73 |
| 0915-0930 | 8 | 0 | 1 | 1 | 9 | 5 | 0 | 6 | 4 | 9 | 6 | 40 | 4 | 50 | 2 | 47 | 3 | 52 |
| 0930-0945 | 6 | 0 | 2 | 1 | 7 | 1 | 2 | 8 | 5 | 8 | 10 | 36 | 2 | 48 | 1 | 54 | 6 | 61 |
| 0945-1000 | 8 | 1 | 1 | 1 | 10 | 5 | 1 | 7 | 4 | 10 | 7 | 34 | 0 | 41 | 2 | 57 | 7 | 66 |
| 1000-1015 | 2 | 2 | 2 | 1 | 5 | 5 | 0 | 7 | 4 | 9 | 6 | 42 | 4 | 52 | 1 | 50 | 4 | 55 |
| 1015-1030 | 7 | 2 | 3 | 2 | 11 | 4 | 0 | 5 | 3 | 7 | 11 | 52 | 3 | 66 | 3 | 55 | 3 | 61 |
| 1030-1045 | 8 | 0 | 1 | 1 | 9 | 4 | 1 | 8 | 5 | 10 | 7 | 52 | 2 | 61 | 1 | 57 | 5 | 63 |
| 1045-1100 | 4 | 1 | 3 | 2 | 7 | 3 | 1 | 8 | 5 | 9 | 5 | 39 | 8 | 52 | 1 | 52 | 3 | 56 |
| 1100-1115 | 9 | 1 | 4 | 2 | 12 | 0 | 4 | 8 | 5 | 9 | 10 | 34 | 7 | 51 | 0 | 37 | 6 | 43 |
| 1115-1130 | 8 | 1 | 3 | 2 | 11 | 0 | 0 | 6 | 4 | 4 | 7 | 43 | 3 | 53 | 3 | 42 | 5 | 50 |
| 1130-1145 | 12 | 1 | 1 | 1 | 14 | 6 | 0 | 12 | 7 | 13 | 3 | 47 | 4 | 54 | 6 | 65 | 6 | 77 |
| 1145-1200 | 9 | 3 | 6 | 4 | 16 | 8 | 1 | 12 | 7 | 16 | 10 | 34 | 10 | 54 | 3 | 48 | 5 | 56 |
| 1200-1215 | 8 | 0 | 6 | 4 | 12 | 6 | 1 | 11 | 7 | 14 | 14 | 46 | 4 | 64 | 1 | 39 | 3 | 43 |
| 1215-1230 | 5 | 0 | 3 | 2 | 7 | 3 | 0 | 11 | 7 | 10 | 8 | 67 | 4 | 79 | 1 | 55 | 3 | 59 |
| 1230-1245 | 6 | 0 | 2 | 1 | 7 | 3 | 2 | 13 | 8 | 13 | 10 | 47 | 4 | 61 | 4 | 58 | 3 | 65 |
| 1245-1300 | 6 | 1 | 7 | 4 | 11 | 5 | 1 | 8 | 5 | 11 | 9 | 41 | 6 | 56 | 3 | 50 | 7 | 60 |
| 1300-1315 | 9 | 1 | 3 | 2 | 12 | 2 | 4 | 13 | 8 | 14 | 6 | 52 | 2 | 60 | 5 | 46 | 3 | 54 |
| 1315-1330 | 5 | 0 | 2 | 1 | 6 | 5 | 1 | 10 | 6 | 12 | 10 | 52 | 6 | 68 | 1 | 65 | 3 | 69 |
| 1330-1345 | 4 | 2 | 4 | 2 | 8 | 0 | 1 | 16 | 10 | 11 | 7 | 54 | 8 | 69 | 5 | 55 | 1 | 61 |
| 1345-1400 | 10 | 0 | 11 | 7 | 17 | 3 | 2 | 15 | 9 | 14 | 11 | 53 | 6 | 70 | 6 | 52 | 2 | 60 |
| 1400-1415 | 12 | 1 | 2 | 1 | 14 | 6 | 2 | 12 | 7 | 15 | 10 | 54 | 6 | 70 | 2 | 42 | 5 | 49 |
| 1415-1430 | 6 | 1 | 3 | 2 | 9 | 7 | 0 | 10 | 6 | 13 | 18 | 68 | 12 | 98 | 3 | 63 | 1 | 67 |
| 1430-1445 | 6 | 2 | 2 | 1 | 9 | 3 | 2 | 6 | 4 | 9 | 4 | 53 | 6 | 63 | 2 | 56 | 11 | 69 |
| 1445-1500 | 6 | 0 | 5 | 3 | 9 | 3 | 0 | 10 | 6 | 9 | 16 | 48 | 10 | 74 | 5 | 79 | 8 | 92 |
| 1500-1515 | 6 | 1 | 4 | 2 | 9 | 4 | 2 | 7 | 4 | 10 | 18 | 77 | 7 | 102 | 1 | 75 | 3 | 79 |
| 1515-1530 | 8 | 1 | 4 | 2 | 11 | 8 | 1 | 14 | 8 | 17 | 8 | 64 | 9 | 81 | 1 | 60 | 4 | 65 |
| 1530-1545 | 5 | 2 | 2 | 1 | 8 | 8 | 1 | 17 | 10 | 19 | 13 | 57 | 6 | 76 | 3 | 87 | 5 | 95 |
| 1545-1600 | 11 | 0 | 1 | 1 | 12 | 12 | 0 | 11 | 7 | 19 | 13 | 79 | 10 | 102 | 1 | 80 | 7 | 88 |
| 1600-1615 | 3 | 2 | 5 | 3 | 8 | 6 | 2 | 7 | 4 | 12 | 14 | 105 | 12 | 131 | 2 | 90 | 9 | 101 |
| 1615-1630 | 9 | 1 | 8 | 5 | 15 | 9 | 1 | 13 | 8 | 18 | 14 | 101 | 11 | 126 | 5 | 67 | 5 | 77 |
| 1630-1645 | 9 | 0 | 4 | 2 | 11 | 8 | 1 | 19 | 11 | 20 | 15 | 112 | 17 | 144 | 2 | 53 | 11 | 66 |
| 1645-1700 | 4 | 1 | 5 | 3 | 8 | 10 | 2 | 17 | 10 | 22 | 15 | 126 | 1 | 142 | 4 | 50 | 9 | 63 |
| 1700-1715 | 9 | 0 | 5 | 3 | 12 | 8 | 1 | 14 | 8 | 17 | 14 | 116 | 15 | 145 | 2 | 48 | 5 | 55 |
| 1715-1730 | 7 | 1 | 3 | 2 | 10 | 9 | 0 | 13 | 8 | 17 | 25 | 118 | 19 | 162 | 0 | 47 | 7 | 54 |
| 1730-1745 | 4 | 2 | 1 | 1 | 7 | 11 | 2 | 16 | 10 | 23 | 16 | 141 | 12 | 169 | 0 | 50 | 3 | 53 |
| 1745-1800 | 6 | 1 | 1 | 1 | 8 | 8 | 1 | 11 | 7 | 16 | 15 | 115 | 9 | 139 | 1 | 49 | 3 | 53 |
| 1800-1815 | 2 | 0 | 1 | 1 | 3 | 8 | 0 | 12 | 7 | 15 | 11 | 87 | 13 | 111 | 3 | 45 | 7 | 55 |
| 1815-1830 | 4 | 0 | 2 | 1 | 5 | 7 | 1 | 11 | 7 | 15 | 12 | 87 | 4 | 103 | 0 | 44 | 2 | 46 |
| 1830-1845 | 8 | 1 | 0 | 0 | 9 | 4 | 1 | 10 | 6 | 11 | 9 | 70 | 7 | 86 | 0 | 51 | 3 | 54 |
| 1845-1900 | 2 | 1 | 1 | 1 | 4 | 3 | 0 | 6 | 4 | 7 | 13 | 42 | 12 | 67 | 2 | 40 | 0 | 42 |

## WARRANT 1 -- EIGHT-HOUR VEHICULAR VOLUME

2021 Existing Year

| Major Street | Ealysville Road |
| :--- | :---: |
| Minor Street | Reas Ford Road |
| Jurisdiction | Earlysville |
| $85 \%$ Speed $>40 \mathrm{mph}$ | NO |
| Population < 10K | YES |
| \# of Lanes on Major Street | $\mathbf{1}$ |
| \# of Lanes on Minor Street | $\mathbf{1}$ |
| Minor St. Right Turns Discounted | YES |
| Have five (5) correctable crashes occurred in 1 year? | NO |



| WARRANT 1 -- EIGHT-HOUR VEHICULAR VOLUME CONDITION 'A' -- MINIMUM VEHICULAR VOLUME |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street |  |  | Ealysville Road |  |  |
| Minor Street |  |  | Reas Ford Road |  |  |
| Jurisdiction |  |  | Earlysville |  |  |
| 85\% Speed > 40 mph |  |  | NO |  |  |
| Population < 10K |  |  | YES |  |  |
| \# of Lanes on Major Street |  |  | 1 |  |  |
| \# of Lanes on Minor Street |  |  | 1 |  |  |
| Minor St. Right Turns Discounted |  |  | YES |  |  |
| Major St. Warranting Volume |  |  | 500 |  |  |
| Minor St. Warranting Volume |  |  | 150 |  |  |
| 30\% Warrant Volume Reduction |  |  | YES |  |  |
| HOUR | $\begin{gathered} \hline \text { MAJOR } \\ \text { STREET } \\ \text { VOLUME } \\ \hline \end{gathered}$ | MINOR STREET VOLUME | MAJOR ST WARRANT VOLUME | MINOR ST <br> WARRANT <br> VOLUME | $\begin{gathered} \text { HOUR } \\ \text { MET } \end{gathered}$ |
| 7-8 AM | 658 | 61 | 350 | 105 | NO |
| 8-9 AM | 633 | 59 | 350 | 105 | NO |
| 9-10 AM | 451 | 35 | 350 | 105 | NO |
| 10-11 AM | 466 | 35 | 350 | 105 | NO |
| 11-12 PM | 438 | 42 | 350 | 105 | NO |
| 12-1 PM | 487 | 47 | 350 | 105 | NO |
| 1-2 PM | 511 | 50 | 350 | 105 | NO |
| 2-3 PM | 582 | 46 | 350 | 105 | NO |
| 3-4 PM | 688 | 65 | 350 | 105 | NO |
| 4-5 PM | 850 | 73 | 350 | 105 | NO |
| 5-6 PM | 830 | 72 | 350 | 105 | NO |
| 6-7 PM | 564 | 47 | 350 | 105 | NO |
| FINDINGS: |  |  |  |  |  |
| Number of Hours Condition 'A' Met |  |  | 0 |  |  |
| Condition 'A' Satisfied? |  |  | NO |  |  |
| COMMENTS: |  |  |  |  |  |



| WARRANT 1 -- EIGHT-HOUR VEHICULAR VOLUME |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| COMBINATION OF CONDITION 'A' \& 'B' (80\% VOLUME) |  |  |  |  |  |
| Major Street |  |  | Ealysville Road |  |  |
| Minor Street |  |  | Reas Ford Road |  |  |
| Jurisdiction |  |  | Earlysville |  |  |
| CONDITION 'A' |  |  |  |  |  |
| HOUR | $\begin{gathered} \text { MAJOR } \\ \text { STREET } \\ \text { VOLUME } \end{gathered}$ | MINOR STREET VOLUME | MAJOR ST WARRANT VOLUME | MINOR ST WARRANT VOLUME | HOUR <br> MET |
| 7-8 AM | 658 | 61 | 280 | 84 | NO |
| 8-9 AM | 633 | 59 | 280 | 84 | NO |
| 9-10 AM | 451 | 35 | 280 | 84 | NO |
| 10-11 AM | 466 | 35 | 280 | 84 | NO |
| 11-12 PM | 438 | 42 | 280 | 84 | NO |
| 12-1 PM | 487 | 47 | 280 | 84 | NO |
| 1-2 PM | 511 | 50 | 280 | 84 | NO |
| 2-3 PM | 582 | 46 | 280 | 84 | NO |
| 3-4 PM | 688 | 65 | 280 | 84 | NO |
| 4-5 PM | 850 | 73 | 280 | 84 | NO |
| 5-6 PM | 830 | 72 | 280 | 84 | NO |
| 6-7 PM | 564 | 47 | 280 | 84 | NO |
| CONDITION 'B' |  |  |  |  |  |
| HOUR | MAJOR STREET VOLUME | MINOR STREET VOLUME | $\begin{gathered} \hline \text { MAJOR ST } \\ \text { WARRANT } \\ \text { VOLUME } \\ \hline \end{gathered}$ | MINOR ST WARRANT VOLUME | $\begin{gathered} \text { HOUR } \\ \text { MET } \end{gathered}$ |
| 7-8 AM | 658 | 61 | 420 | 42 | YES |
| 8-9 AM | 633 | 59 | 420 | 42 | YES |
| 9-10 AM | 451 | 35 | 420 | 42 | NO |
| 10-11 AM | 466 | 35 | 420 | 42 | NO |
| 11-12 PM | 438 | 42 | 420 | 42 | YES |
| 12-1 PM | 487 | 47 | 420 | 42 | YES |
| 1-2 PM | 511 | 50 | 420 | 42 | YES |
| 2-3 PM | 582 | 46 | 420 | 42 | YES |
| 3-4 PM | 688 | 65 | 420 | 42 | YES |
| 4-5 PM | 850 | 73 | 420 | 42 | YES |
| 5-6 PM | 830 | 72 | 420 | 42 | YES |
| 6-7 PM | 564 | 47 | 420 | 42 | YES |
| FINDINGS: |  |  |  |  |  |
| Number of Hours Combination A\&B Met |  |  | 0 |  |  |
| Combination of A\&B Satisfied? |  |  | NO |  |  |
| COMMENTS: |  |  |  |  |  |

## Appendix D-2

## Warrant 2: 4-Hour Signal Warrant 2021 Existing Conditions

## Warrant 2: Four-hour Vehicular Volume

## 1: Earlysville Rd @ Reas Ford Road/Earlysville Forest Drive

Intersection Information

|  | Major Street | Minor Street |
| :--- | :--- | :--- |
| Street Name | Earlysville Rd | Earlysville Forest Dr |
| Direction | EB/WB | $\mathrm{NB} / \mathrm{SB}$ |
| Number of Lane: | 1 | 1 |
| Approch Speed | 35 | 35 |

## Warrant 2 Met?

## Details:

| Notes | 2 Hours met (4 required) |
| :--- | :---: |
| Low populatior | Yes |

Four-Hour Vehicular Volume
Community Population Less Than 10,000 or Major Street Approach Speed Above 40 mph


- Warrant Curve
$\square$ Warranted
- Unwarranted
- 1 Major, 1 Minor

1 Major, 2+ Minor
$2+$ Major, 1 Minor
2+ Major, 2+ Minor

Warrant 2: Four-hour Vehicular Volume
1: Earlysville Rd @ Reas Ford Road/Earlysville Forest Drive

| Hourly Volumes |  |  |
| :---: | :---: | :---: |
| Hour | Major Street Total All Approaches (vph) | Minor Street Highest Volume Approach (vph) |
| 00:00:00-01:00:00 | 0 | 0 |
| 01:00:00-02:00:00 | 0 | 0 |
| 02:00:00-03:00:00 | 0 | 0 |
| 03:00:00-04:00:00 | 0 | 0 |
| 04:00:00-05:00:00 | 0 | 0 |
| 05:00:00-06:00:00 | 0 | 0 |
| 06:00:00-07:00:00 | 0 | 0 |
| 07:00:00-08:00:00 | 658 | 61 |
| 08:00:00-09:00:00 | 633 | 59 |
| 09:00:00-10:00:00 | 451 | 40 |
| 10:00:00-11:00:00 | 466 | 35 |
| 11:00:00-12:00:00 | 438 | 53 |
| 12:00:00-13:00:00 | 487 | 48 |
| 13:00:00-14:00:00 | 511 | 51 |
| 14:00:00-15:00:00 | 582 | 46 |
| 15:00:00-16:00:00 | 688 | 65 |
| 16:00:00-17:00:00 | 850 | 72 |
| 17:00:00-18:00:00 | 830 | 73 |
| 18:00:00-19:00:00 | 564 | 48 |
| 19:00:00-20:00:00 | 0 | 0 |
| 20:00:00-21:00:00 | 0 | 0 |
| 21:00:00-22:00:00 | 0 | 0 |
| 22:00:00-23:00:00 | 0 | 0 |

Warrant 2: Four-hour Vehicular Volume
1: Earlysville Rd @ Reas Ford Road/Earlysville Forest Drive

| $23: 00: 00-00: 00: 00$ | 0 | 0 |
| :---: | :---: | :---: |


| Warranted Hours |  |  |
| :---: | :---: | :---: |
| Hour | Major Street <br> Total All <br> Approaches (vph) | Minor Street <br> Highest Volume <br> Approach (vph) |
| $15: 30: 00-16: 30: 00$ | 796.00 | 68.00 |
| $16: 30: 00-17: 30: 00$ | 831.00 | 76.00 |

Note: Only data of hours warranted is represented in the above table.

## Appendix D-3

## Warrant 3: Peak Hour Signal Warrant 2021 Existing Conditions

Warrant 3: Peak Hour

## 1: Earlysville Rd @ Reas Ford Road/Earlysville Forest Drive

Intersection Information

|  | Major Street | Minor Street |
| :--- | :--- | :--- |
| Street Name | Earlysville Rd | Earlysville Forest Dr |
| Direction | EB/WB | NB/SB |
| Number of Lane: | 1 | 1 |
| Approch Speed | 35 | 35 |

## Warrant 3 Met? No

Details

| Low Population: | Yes |  |  |
| :--- | :--- | :--- | :--- |
| Condition A Met‘ | No |  |  |
| Notes | 0 Hours met (1 required) | Condition B Met | No |
| Minor Approach Time Delay Condition Met? | Notes | 0 Hours met (1 required) |  |
| Minor Approach Volume Condition Met? | Not Met |  |  |
| Total Entering Intersection Volume Condition Met? | Not Met |  |  |

Peak Hour Vehicular Volume Community Population Less Than 10,000 or Major Street Approach Speed Above 40 mph


Warrant 3: Peak Hour
1: Earlysville Rd @ Reas Ford Road/Earlysville Forest Drive

| Hour | Major Street <br> Total All <br> Approaches (vph) | Minor Street <br> Highest Volume <br> Approach (vph) |
| :---: | :---: | :---: |
| $7: 00$ | 658 | 61 |
| $8: 00$ | 633 | 59 |
| $9: 00$ | 451 | 40 |
| $10: 00$ | 466 | 35 |
| $11: 00$ | 438 | 53 |
| $12: 00$ | 487 | 48 |
| $13: 00$ | 511 | 51 |
| $14: 00$ | 582 | 46 |
| $15: 00$ | 688 | 65 |
| $16: 00$ | 850 | 72 |
| $17: 00$ | 830 | 73 |

## Appendix D-4

## Warrant 7: Crash Experience 2021 Existing Conditions

## WARRANT 7 -- CRASH EXPERIENCE



FINDINGS:

| Condition A Satisfied? | 0 |
| :--- | ---: |
| Condition B Satisfied? | 5 |
| WARRANT 7 Satisfied? | NO |

## Warrant 7: Crash Experience

## 1: Earlysville Rd @ Reas Ford Road/Earlysville Forest Drive

## Intersection Information

| Major Street Name | Earlysville Rd |
| :--- | :--- |
| Major Street Direction | EB/WB |
| Minor Street Direction | NB/SB |

Details:

| Low Population? | Yes Tr | Traffic Volume Condition Met? | Yes |
| :---: | :---: | :---: | :---: |
| Major Street Speed Limit | 35 |  | 10 Hours Met (8 Required) |
| Major Street 85th-\% tile Speed | 0.00 P | Ped Volume Condition Met? | No |
|  |  |  | 0 Hours Met (8 Required) |
|  | Qualifying Crashes | 7 |  |
|  | Adequate Alternative Trials? | ? No |  |


| Hour | Traffic Volumes |  |  |  | Pedestrian Volumes |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Major Street Vehicles | Minor Street Vehicles | 80\% Standard Met? <br> A or B |  | Northbound Ped Volumes |  | Southbound Ped Volumes |  |
|  |  |  | Conditio n A | Condition B | Peds | > 80? | Peds | > 80 ? |
| 07:00 to 08:00 | 658 | 0 | No | No | 0 | No | 0 | No |
| 07:15 to 08:15 | 682 | 0 | No | No | 0 | No | 0 | No |
| 07:30 to 08:30 | 711 | 0 | No | No | 0 | No | 0 | No |
| 07:45 to 08:45 | 696 | 0 | No | No | 0 | No | 0 | No |
| 08:00 to 09:00 | 633 | 0 | No | No | 0 | No | 0 | No |
| 08:15 to 09:15 | 606 | 0 | No | No | 0 | No | 0 | No |

## Warrant 7: Crash Experience

1: Earlysville Rd @ Reas Ford Road/Earlysville Forest Drive

| 08:30 to 09:30 | 540 | 0 | No | No | 0 | No | 0 | No |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 08:45 to 09:45 | 491 | 0 | No | No | 0 | No | 0 | No |
| 09:00 to 10:00 | 451 | 0 | No | No | 0 | No | 0 | No |
| 09:15 to 10:15 | 425 | 0 | No | No | 0 | No | 0 | No |
| 09:30 to 10:30 | 450 | 0 | No | No | 0 | No | 0 | No |
| 09:45 to 10:45 | 465 | 0 | No | No | 0 | No | 0 | No |
| 10:00 to 11:00 | 466 | 0 | No | No | 0 | No | 0 | No |
| 10:15 to 11:15 | 453 | 0 | No | No | 0 | No | 0 | No |
| 10:30 to 11:30 | 429 | 0 | No | No | 0 | No | 0 | No |
| 10:45 to 11:45 | 436 | 0 | No | No | 0 | No | 0 | No |
| 11:00 to 12:00 | 438 | 0 | No | No | 0 | No | 0 | No |
| 11:15 to 12:15 | 451 | 0 | No | No | 0 | No | 0 | No |
| 11:30 to 12:30 | 486 | 0 | No | No | 0 | No | 0 | No |
| 11:45 to 12:45 | 481 | 0 | No | No | 0 | No | 0 | No |
| 12:00 to 13:00 | 487 | 0 | No | No | 0 | No | 0 | No |
| 12:15 to 13:15 | 494 | 0 | No | No | 0 | No | 0 | No |

## Warrant 7: Crash Experience

1: Earlysville Rd @ Reas Ford Road/Earlysville Forest Drive

| 12:30 to 13:30 | 493 | 0 | No | No | 0 | No | 0 | No |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12:45 to 13:45 | 497 | 0 | No | No | 0 | No | 0 | No |
| 13:00 to 14:00 | 511 | 0 | No | No | 0 | No | 0 | No |
| 13:15 to 14:15 | 516 | 0 | No | No | 0 | No | 0 | No |
| 13:30 to 14:30 | 544 | 0 | No | No | 0 | No | 0 | No |
| 13:45 to 14:45 | 546 | 0 | No | No | 0 | No | 0 | No |
| 14:00 to 15:00 | 582 | 0 | No | No | 0 | No | 0 | No |
| 14:15 to 15:15 | 644 | 0 | No | No | 0 | No | 0 | No |
| 14:30 to 15:30 | 625 | 0 | No | No | 0 | No | 0 | No |
| 14:45 to 15:45 | 664 | 0 | No | No | 0 | No | 0 | No |
| 15:00 to 16:00 | 688 | 0 | No | No | 0 | No | 0 | No |
| 15:15 to 16:15 | 739 | 0 | No | No | 0 | No | 0 | No |
| 15:30 to 16:30 | 796 | 0 | No | No | 0 | No | 0 | No |
| 15:45 to 16:45 | 835 | 0 | No | No | 0 | No | 0 | No |
| 16:00 to 17:00 | 850 | 0 | No | No | 0 | No | 0 | No |
| 16:15 to 17:15 | 818 | 0 | No | No | 0 | No | 0 | No |

Warrant 7: Crash Experience
1: Earlysville Rd @ Reas Ford Road/Earlysville Forest Drive

| 16:30 to 17:30 | 831 | 0 | No | No | 0 | No | 0 | No |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16:45 to 17:45 | 843 | 0 | No | No | 0 | No | 0 | No |
| 17:00 to 18:00 | 830 | 0 | No | No | 0 | No | 0 | No |
| 17:15 to 18:15 | 796 | 0 | No | No | 0 | No | 0 | No |
| 17:30 to 18:30 | 729 | 0 | No | No | 0 | No | 0 | No |
| 17:45 to 18:45 | 647 | 0 | No | No | 0 | No | 0 | No |
| 18:00 to 19:00 | 564 | 0 | No | No | 0 | No | 0 | No |
| 18:15 to 19:15 | 398 | 0 | No | No | 0 | No | 0 | No |
| 18:30 to 19:30 | 249 | 0 | No | No | 0 | No | 0 | No |
| 18:45 to 19:45 | 109 | 0 | No | No | 0 | No | 0 | No |

## Appendix E

## Alternative Cost Analysis

## Appendix E-1

## Alternative 1: Cost Analysis

| Albemarle County <br> Earlysville Road / Reas Ford Road Turn Lanes <br> November 16, 2021 <br> Preliminary Cost Estimate |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \hline \text { ITEM } \\ & \text { CODE } \end{aligned}$ | SPEC | ITEM DESCRIPTION | UNITS | QUANTITY |  | T PRICE |  | AL PRICE |
|  |  |  |  |  |  |  |  |  |
| 00100 | 513 | MOBILIZATION | LS | 1 | \$ | 59,000 | \$ | 59,000 |
| 00101 | 105 | CONSTRUCTION SURVEYING (CONSTRUCTION) | LS | 1 | \$ | 7,000 | \$ | 7,000 |
| 00110 | 301 | CLEARING AND GRUBBING | ACRE | 1.0 | \$ | 15,000 | \$ | 15,000 |
| EARTHWORK |  |  |  |  |  |  |  |  |
| 00120 | 303 | REGULAR EXCAVATION | CY | 1,000 | \$ | 18 | \$ | 18,000 |
| 00140 | 303, 305 | BORROW EXCAVATION | CY | 500 | \$ | 23 | \$ | 11,500 |
| INCIDENTALS |  |  |  |  |  |  |  |  |
| 68576 | 315, 412 | SAW CUT | LF | 2,976 | \$ | 10 | \$ | 29,760 |
| PAVEMENT |  |  |  |  |  |  |  |  |
| 16350 | 315 | ASPHALT CONC. TYPE SM-12.5A (NEW SECTION) | TON | 180 | \$ | 115 | \$ | 20,700 |
| 10610 | 315 | ASPHALT CONC. TYPE IM-19.0A (NEW SECTION) | TON | 224 | \$ | 115 | \$ | 25,760 |
| 16390 | 315 | ASPH. CONC. BASE COURSE TY. BM-25.0A (NEW SECTION) | TON | 359 | \$ | 105 | \$ | 37,695 |
| 10128 | 308, 309 | AGGR. BASE MATL. TY. I NO. 21B (NEW SECTION) | TON | 725 | \$ | 40 | \$ | 29,000 |
| 10628 | 515 | FLEXIBLE PAVEMENT PLANNING 0" - 2" | SY | 4,828 | \$ | 6 | \$ | 28,968 |
| 16350 | 315 | ASPHALT CONC. TYPE SM-12.5A (OVERLAY) | TON | 531 | \$ | 100 | \$ | 53,100 |
| 24430 | 508 | DEMOLITION OF PAVEMENT (FLEXIBLE) | SY | 50 | \$ | 20 | \$ | 1,000 |
| DRAINAGE \& BASINS |  |  |  |  |  |  |  |  |
| NS |  | DRAINAGE ITEMS | LS | 1 | \$ | 150,000 | \$ | 150,000 |
| EROSION AND SEDIMENT CONTROL |  |  |  |  |  |  |  |  |
| NS |  | E\&S ITEMS | LS | 1 | \$ | 30,000 | \$ | 30,000 |
| TRAFFIC |  |  |  |  |  |  |  |  |
| NS |  | SIGNING \& PAVEMENT MARKING | LS | 1 | \$ | 30,000 | \$ | 30,000 |
| ROADSIDE DEVELOPMENT |  |  |  |  |  |  |  |  |
| NS |  | ROADSIDE DEVELOPMENT ITEMS | LS | 1 | \$ | 25,000 | \$ | 25,000 |
| MAINTENANCE OF TRAFFIC |  |  |  |  |  |  |  |  |
| NS | - | MOT | LS | 1 | \$ | 200,000 | \$ | 200,000 |
|  |  |  |  |  |  |  |  |  |
| Estimated Construction Cost |  |  |  |  |  |  | \$ | 771,483 |
| CONTINGENCY CEI |  |  |  |  |  | 50\% | \$ | 385,742 |
|  |  |  |  |  |  | 18\% | \$ | 190,964 |
| TOTAL CONSTRUCTION |  |  |  |  |  |  | \$ | 1,348,189 |
| PE \& Permitting (25\% of Construction Cost excluding CEI) |  |  |  |  |  |  | \$ | 289,306 |
| Preliminary Right of Way and Easements |  |  |  |  |  |  | \$ | 266,000 |
| Utility Easements and Relocation Cost |  |  |  |  |  |  | \$ | - |
| R/W \& UTILITIES (2020) |  |  |  |  |  |  | \$ | 266,000 |
| Environmental Mitigation (2020) |  |  |  |  |  |  | \$ | - |
| PROJECT GRAND TOTAL (FY 2020) |  |  |  |  |  |  | \$ | 1,903,495 |

## Appendix E-2

## Alternative 2: Cost Analysis

| Albemarle County <br> Earlysville Road / Reas Ford Road Turn Lanes <br> November 16, 2021 <br> Preliminary Cost Estimate |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \hline \text { ITEM } \\ & \text { CODE } \end{aligned}$ | SPEC | ITEM DESCRIPTION | UNITS | QUANTITY |  | T PRICE |  | TAL PRICE |
|  |  |  |  |  |  |  |  |  |
| 00100 | 513 | MOBILIZATION | LS | 1 | \$ | 59,000 | \$ | 59,000 |
| 00101 | 105 | CONSTRUCTION SURVEYING (CONSTRUCTION) | LS | 1 | \$ | 7,000 | \$ | 7,000 |
| 00110 | 301 | CLEARING AND GRUBBING | ACRE | 1.0 | \$ | 15,000 | \$ | 15,000 |
| EARTHWORK |  |  |  |  |  |  |  |  |
| 00120 | 303 | REGULAR EXCAVATION | CY | 1,000 | \$ | 18 | \$ | 18,000 |
| 00140 | 303, 305 | BORROW EXCAVATION | CY | 500 | \$ | 23 | \$ | 11,500 |
| INCIDENTALS |  |  |  |  |  |  |  |  |
| 68576 | 315, 412 | SAW CUT | LF | 2,976 | \$ | 10 | \$ | 29,760 |
| PAVEMENT |  |  |  |  |  |  |  |  |
| 16350 | 315 | ASPHALT CONC. TYPE SM-12.5A (NEW SECTION) | TON | 180 | \$ | 115 | \$ | 20,700 |
| 10610 | 315 | ASPHALT CONC. TYPE IM-19.0A (NEW SECTION) | TON | 224 | \$ | 115 | \$ | 25,760 |
| 16390 | 315 | ASPH. CONC. BASE COURSE TY. BM-25.0A (NEW SECTION) | TON | 359 | \$ | 105 | \$ | 37,695 |
| 10128 | 308, 309 | AGGR. BASE MATL. TY. I NO. 21B (NEW SECTION) | TON | 725 | \$ | 40 | \$ | 29,000 |
| 10628 | 515 | FLEXIBLE PAVEMENT PLANNING 0" - 2" | SY | 4,828 | \$ | 6 | \$ | 28,968 |
| 16350 | 315 | ASPHALT CONC. TYPE SM-12.5A (OVERLAY) | TON | 531 | \$ | 100 | \$ | 53,100 |
| 24430 | 508 | DEMOLITION OF PAVEMENT (FLEXIBLE) | SY | 50 | \$ | 20 | \$ | 1,000 |
| DRAINAGE \& BASINS |  |  |  |  |  |  |  |  |
| NS |  | DRAINAGE ITEMS | LS | 1 | \$ | 150,000 | \$ | 150,000 |
| EROSION AND SEDIMENT CONTROL |  |  |  |  |  |  |  |  |
| NS |  | E\&S ITEMS | LS | 1 | \$ | 30,000 | \$ | 30,000 |
| TRAFFIC |  |  |  |  |  |  |  |  |
| NS |  | SIGNING \& PAVEMENT MARKING | LS | 1 | \$ | 30,000 | \$ | 30,000 |
| ROADSIDE DEVELOPMENT |  |  |  |  |  |  |  |  |
| NS |  | ROADSIDE DEVELOPMENT ITEMS | LS | 1 | \$ | 25,000 | \$ | 25,000 |
| MAINTENANCE OF TRAFFIC |  |  |  |  |  |  |  |  |
| NS | - | MOT | LS | 1 | \$ | 200,000 | \$ | 200,000 |
| SIGNALIZATION |  |  |  |  |  |  |  |  |
| NS | - | TRAFFIC SIGNAL | LS | 1 | \$ | 200,000 | \$ | 200,000 |
|  |  |  |  |  |  |  |  |  |
| Estimated Construction Cost |  |  |  |  |  |  | \$ | 971,483 |
| CONTINGENCY |  |  |  |  |  | 50\% | \$ | 485,742 |
| CEI ${ }^{\text {TOTAL CONSTRUCTION }}$ |  |  |  |  |  | 18\% | \$ | 243,464 |
|  |  |  |  |  |  |  | \$ | 1,700,689 |
| PE \& Permitting (25\% of Construction Cost excluding CEI) |  |  |  |  |  |  | \$ | 364,306 |
| Preliminary Right of Way and Easements |  |  |  |  |  |  | \$ | 266,000 |
| Utility Easements and Relocation Cost |  |  |  |  |  |  | \$ | - |
| R/W \& UTILITIES (2020) |  |  |  |  |  |  | \$ | 266,000 |
| Environmental Mitigation (2020) |  |  |  |  |  |  | \$ | - |
| PROJECT GRAND TOTAL (FY 2020) |  |  |  |  |  |  | \$ | 2,330,995 |

## Appendix E-3

## Alternative 3: Cost Analysis

|  |  | Albemarle County Earlysville Road / Reas Ford Road November 16, 2021 Preliminary Cost Estim | dabou |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { ITEM } \\ & \text { CODE } \end{aligned}$ | SPEC | ITEM DESCRIPTION | UNITS | QUANTITY |  | T PRICE |  | TAL PRICE |
|  |  |  |  |  |  |  |  |  |
| 00100 | 513 | MOBILIZATION | LS | 1 | \$ | 93,368 | \$ | 93,368 |
| 00101 | 105 | CONSTRUCTION SURVEYING (CONSTRUCTION) | LS | 1 | \$ | 12,674 | \$ | 12,674 |
| 00110 | 301 | CLEARING AND GRUBBING | ACRE | 1.6 | \$ | 15,000 | \$ | 24,000 |
|  |  | EARTHWORK |  |  |  |  |  |  |
| 00120 | 303 | REGULAR EXCAVATION | CY | 2,891 | \$ | 18 | \$ | 52,038 |
| 00140 | 303, 305 | BORROW EXCAVATION | CY | 1,789 | \$ | 23 | \$ | 41,147 |
| 00128 | ATTD | UNSUITABLE EXCAVATION | CY | 320 | \$ | 20 | \$ | 6,400 |
|  |  | INCIDENTALS |  |  |  |  |  |  |
| 12600 | 502 | STD. COMB. CURB \& GUTTER CG-6 | LF | 210 | \$ | 34 | \$ | 7,140 |
| 12610 | 502 | RADIAL COMB. CURB \& GUTTER CG-6 | LF | 310 | \$ | 35 | \$ | 10,850 |
| 12032 | 502 | RADIAL CURB CG-3 | LF | 420 | \$ | 32 | \$ | 13,440 |
| 21020 | 502 | MEDIAN STRIP MS-1 | SY | 299 | \$ | 115 | \$ | 34,385 |
| 68576 | 315, 412 | SAW CUT | LF | 6,000 | \$ | 10 | \$ | 60,000 |
|  |  | PAVEMENT |  |  |  |  |  |  |
| 16350 | 315 | ASPHALT CONC. TYPE SM-12.5A (NEW SECTION) | TON | 219 | \$ | 115 | \$ | 25,185 |
| 10610 | 315 | ASPHALT CONC. TYPE IM-19.0A (NEW SECTION) | TON | 273 | \$ | 115 | \$ | 31,395 |
| 16390 | 315 | ASPH. CONC. BASE COURSE TY. BM-25.0A (NEW SECTION) | TON | 437 | \$ | 105 | \$ | 45,885 |
| 10128 | 308, 309 | AGGR. BASE MATL. TY. I NO. 21B (NEW SECTION) | TON | 884 | \$ | 40 | \$ | 35,360 |
| 10628 | 515 | FLEXIBLE PAVEMENT PLANNING 0" - 2" | SY | 1,290 | \$ | 6 | \$ | 7,740 |
| 16350 | 315 | ASPHALT CONC. TYPE SM-12.5A (OVERLAY) | TON | 142 | \$ | 100 | \$ | 14,200 |
| 24430 | 508 | DEMOLITION OF PAVEMENT (FLEXIBLE) | SY | 52 | \$ | 20 | \$ | 1,040 |
| 10011 | 504 | 7" HYDRAULIC CEMENT STAMPED CONCRETE (TRUCK APRON) | SY | 659 | \$ | 155 | \$ | 102,145 |
|  |  | DRAINAGE \& BAS |  |  |  |  |  |  |
| NS |  | DRAINAGE ITEMS | LS | 1 | \$ | 300,000 | \$ | 300,000 |
|  |  | EROSION AND SEDIMENT | ROL |  |  |  |  |  |
| NS |  | E\&S ITEMS | LS | 1 | \$ | 30,000 | \$ | 30,000 |
|  |  | TRAFFIC |  |  |  |  |  |  |
| NS |  | SIGNING \& PAVEMENT MARKING | LS | 1 | \$ | 30,000 | \$ | 30,000 |
| NS |  | ROUNDABOUT LIGHTING | LS | 1 | \$ | 60,000 | \$ | 60,000 |
|  |  | ROADSIDE DEVELOP |  |  |  |  |  |  |
| NS |  | ROADSIDE DEVELOPMENT ITEMS | LS | 1 | \$ | 25,000 | \$ | 25,000 |
| NS |  | LANDSCAPING | LS | 1 | \$ | 60,000 | \$ | 60,000 |
|  |  | MAINTENANCE OF TR |  |  |  |  |  |  |
| NS | - | MOT | LS | 1 | \$ | 250,000 | \$ | 250,000 |
|  |  |  |  |  |  |  |  |  |
|  | nated C | nstruction Cost |  |  |  |  | \$ | 1,373,391 |
|  | CONTING | NCY |  |  |  | 50\% | \$ | 686,696 |
|  | EI |  |  |  |  | 18\% | \$ | 341,958 |
|  | TOTAL | CONSTRUCTION |  |  |  |  | \$ | 2,402,044 |
| PE \& Permitting (25\% of Construction Cost excluding CEI) |  |  |  |  |  |  | \$ | 515,022 |
| Preliminary Right of Way and Easements |  |  |  |  |  |  | \$ | 1,250,000 |
| Utility Easements and Relocation Cost |  |  |  |  |  |  | \$ | 100,000 |
| R/W \& UTILITIES (2022) |  |  |  |  |  |  | \$ | 1,350,000 |
| Environmental Mitigation (2022) |  |  |  |  |  |  | \$ | - |
| PROJECT GRAND TOTAL (FY 2022) |  |  |  |  |  |  | \$ | 4,267,066 |

## Appendix E-3B

## Alternative 3B: Cost Analysis

|  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { ITEM } \\ & \text { CODE } \end{aligned}$ | SPEC | ITEM DESCRIPTION | UNITS | QUANTITY |  | T PRICE |  | TAL PRICE |
|  |  |  |  |  |  |  |  |  |
| 00100 | 513 | MOBILIZATION | LS | 1 | \$ | 66,160 | \$ | 66,160 |
| 00101 | 105 | CONSTRUCTION SURVEYING (CONSTRUCTION) | LS | 1 | \$ | 7,232 | \$ | 7,232 |
| 00110 | 301 | CLEARING AND GRUBBING | ACRE | 0.8 | \$ | 15,000 | \$ | 12,000 |
| EARTHWORK |  |  |  |  |  |  |  |  |
| 00120 | 303 | REGULAR EXCAVATION | CY | 1,051 | \$ | 18 | \$ | 18,918 |
| 00140 | 303, 305 | BORROW EXCAVATION | CY | 597 | \$ | 23 | \$ | 13,731 |
| 00128 | ATTD | UNSUITABLE EXCAVATION | CY | 105 | \$ | 20 | \$ | 2,100 |
| INCIDENTALS |  |  |  |  |  |  |  |  |
| 12600 | 502 | STD. COMB. CURB \& GUTTER CG-6 | LF | 0 | \$ | 34 | \$ | - |
| 12610 | 502 | RADIAL COMB. CURB \& GUTTER CG-6 | LF | 189 | \$ | 35 | \$ | 6,615 |
| 12032 | 502 | RADIAL CURB CG-3 | LF | 12 | \$ | 32 | \$ | 384 |
| 21020 | 502 | MEDIAN STRIP MS-1 | SY | 32 | \$ | 115 | \$ | 3,680 |
| 68576 | 315, 412 | SAW CUT | LF | 3,000 | \$ | 10 | \$ | 30,000 |
| PAVEMENT |  |  |  |  |  |  |  |  |
| 16350 | 315 | ASPHALT CONC. TYPE SM-12.5A (NEW SECTION) | TON | 139 | \$ | 115 | \$ | 15,985 |
| 10610 | 315 | ASPHALT CONC. TYPE IM-19.0A (NEW SECTION) | TON | 173 | \$ | 115 | \$ | 19,895 |
| 16390 | 315 | ASPH. CONC. BASE COURSE TY. BM-25.0A (NEW SECTION) | TON | 278 | \$ | 105 | \$ | 29,190 |
| 10128 | 308, 309 | AGGR. BASE MATL. TY. I NO. 21B (NEW SECTION) | TON | 561 | \$ | 40 | \$ | 22,440 |
| 10628 | 515 | FLEXIBLE PAVEMENT PLANNING 0" - 2" | SY | 927 | \$ | 6 | \$ | 5,562 |
| 16350 | 315 | ASPHALT CONC. TYPE SM-12.5A (OVERLAY) | TON | 102 | \$ | 100 | \$ | 10,200 |
| 24430 | 508 | DEMOLITION OF PAVEMENT (FLEXIBLE) | SY | 0 | \$ | 20 | \$ | - |
| 10011 | 504 | 7" HYDRAULIC CEMENT STAMPED CONCRETE (TRUCK APRON) | SY | 0 | \$ | 155 | \$ | - |
| DRAINAGE \& BASINS |  |  |  |  |  |  |  |  |
| NS |  | DRAINAGE ITEMS | LS | 1 | \$ | 150,000 | \$ | 150,000 |
| EROSION AND SEDIMENT CONTROL |  |  |  |  |  |  |  |  |
| NS |  | E\&S ITEMS | LS | 1 | \$ | 15,000 | \$ | 15,000 |
| TRAFFIC |  |  |  |  |  |  |  |  |
| NS |  | SIGNING \& PAVEMENT MARKING | LS | 1 | \$ | 45,000 | \$ | 45,000 |
| NS |  | ROUNDABOUT LIGHTING | LS | 1 | \$ | 60,000 | \$ | 60,000 |
| ROADSIDE DEVELOPMENT |  |  |  |  |  |  |  |  |
| NS |  | ROADSIDE DEVELOPMENT ITEMS | LS | 1 | \$ | 12,500 | \$ | 12,500 |
| MAINTENANCE OF TRAFFIC |  |  |  |  |  |  |  |  |
| NS | - | MOT | LS | 1 | \$ | 250,000 | \$ | 250,000 |
|  |  |  |  |  |  |  |  |  |
| Estimated Construction Cost |  |  |  |  |  |  | \$ | 796,592 |
| CONTINGENCY |  |  |  |  |  | 50\% | \$ | 398,296 |
| CEI |  |  |  |  |  | 18\% | \$ | 196,262 |
| TOTAL CONSTRUCTION |  |  |  |  |  |  | \$ | 1,391,150 |
| PE \& Permitting (25\% of Construction Cost excluding CEI) |  |  |  |  |  |  | \$ | 298,722 |
| Preliminary Right of Way and Easements |  |  |  |  |  |  | \$ | 640,272 |
| Utility Easements and Relocation Cost |  |  |  |  |  |  | \$ | 100,000 |
| R/W \& UTILITIES (2022) |  |  |  |  |  |  | \$ | 740,272 |
| Environmental Mitigation (2022) |  |  |  |  |  |  | \$ | - |
| PROJECT GRAND TOTAL (FY 2022) |  |  |  |  |  |  | \$ | 2,430,144 |

## Appendix F

Traffic Analysis

## Appendix F-1

## 2021 Existing Conditions AM Peak

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 4.4 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | * | 「 |  | \$ |  |  | $\ddagger$ |  |
| Traffic Vol, veh/h | 14 | 489 | 36 | 36 | 127 | 9 | 29 | 1 | 66 | 47 | 7 | 12 |
| Future Vol, veh/h | 14 | 489 | 36 | 36 | 127 | 9 | 29 | 1 | 66 | 47 | 7 | 12 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 3 | 3 | 0 | 2 |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | 100 | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 |
| Heavy Vehicles, \% | 0 | 1 | 0 | 3 | 3 | 0 | 0 | 0 | 5 | 0 | 0 | 8 |
| Mvmt Flow | 16 | 569 | 42 | 42 | 148 | 10 | 34 | 1 | 77 | 55 | 8 | 14 |



Queuing and Blocking Report

Intersection: 1: Reas Ford Rd/Earlysville Forest Drive \& Earlysville Road

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LT | LTR | LTR |
| Maximum Queue (ft) | 39 | 47 | 83 | 62 |
| Average Queue (ft) | 3 | 10 | 33 | 21 |
| 95th Queue (ft) | 17 | 31 | 64 | 43 |
| Link Distance (ft) | 906 | 1105 | 1198 | 748 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

## Network Summary

Network wide Queuing Penalty: 0

## Appendix F-2

## 2021 Existing Conditions PM Peak

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 3.3 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | * | 「 |  | \$ |  |  | $\ddagger$ |  |
| Traffic Vol, veh/h | 13 | 260 | 34 | 58 | 444 | 41 | 33 | 6 | 56 | 25 | 4 | 22 |
| Future Vol, veh/h | 13 | 260 | 34 | 58 | 444 | 41 | 33 | 6 | 56 | 25 | 4 | 22 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 4 | 2 | 0 | 4 |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | 100 | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 |
| Heavy Vehicles, \% | 8 | 1 | 6 | 5 | 1 | 0 | 0 | 0 | 7 | 0 | 0 | 0 |
| Mvmt Flow | 13 | 268 | 35 | 60 | 458 | 42 | 34 | 6 | 58 | 26 | 4 | 23 |



Queuing and Blocking Report

Intersection: 1: Reas Ford Rd/Earlysville Forest Drive \& Earlysville Road

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LT | LTR | LTR |
| Maximum Queue (ft) | 57 | 83 | 88 | 42 |
| Average Queue (ft) | 5 | 15 | 32 | 18 |
| 95th Queue (ft) | 31 | 53 | 66 | 37 |
| Link Distance (ft) | 906 | 1105 | 1198 | 748 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  | 0 |  |  |
| Storage Blk Time (\%) |  | 0 |  |  |
| Queuing Penalty (veh) |  | 0 |  |  |

## Network Summary

Network wide Queuing Penalty: 0

## Appendix F-3

## Alternative 1: TWSC w/ Turn Lanes Conditions AM Peak

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 4.2 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | F |  | ${ }^{1}$ | $\uparrow$ |  |  | $\uparrow$ | F |  | $\$$ |  |
| Traffic Vol, veh/h | 14 | 489 | 36 | 36 | 127 | 9 | 29 | 1 | 66 | 47 | 7 | 12 |
| Future Vol, veh/h | 14 | 489 | 36 | 36 | 127 | 9 | 29 | 1 | 66 | 47 | 7 | 12 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 3 | 3 | 0 | 2 |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 125 | - | - | 125 | - | - | - | - | 125 | - | - | - |
| Veh in Median Storage, \# | \# - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 |
| Heavy Vehicles, \% | 0 | 1 | 0 | 3 | 3 | 0 | 0 | 0 | 5 | 0 | 0 | 8 |
| Mvmt Flow | 16 | 569 | 42 | 42 | 148 | 10 | 34 | 1 | 77 | 55 | 8 | 14 |



Queuing and Blocking Report

Intersection: 1: Reas Ford Rd/Earlysville Forest Drive \& Earlysville Road

| Movement | EB | EB | WB | WB | NB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LT | R | LTR |
| Maximum Queue (ft) | 18 | 9 | 39 | 6 | 54 | 66 | 49 |
| Average Queue (ft) | 1 | 0 | 13 | 0 | 16 | 20 | 23 |
| 95th Queue (ft) | 8 | 5 | 36 | 4 | 38 | 45 | 45 |
| Link Distance (ft) |  | 905 |  | 1109 | 1192 |  | 755 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 125 |  |  | 125 |  |
| Storage Bay Dist (ft) | 125 |  | 125 |  |  |  |  |

## Network Summary

Network wide Queuing Penalty: 0

## Appendix F-4

## Alternative 1: TWSC w/ Turn Lanes Conditions PM Peak

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 3.1 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | F |  | ${ }^{7}$ | $\dagger$ |  |  | $\uparrow$ | 7 |  | $\$$ |  |
| Traffic Vol, veh/h | 13 | 260 | 34 | 58 | 444 | 41 | 33 | 6 | 56 | 25 | 4 | 22 |
| Future Vol, veh/h | 13 | 260 | 34 | 58 | 444 | 41 | 33 | 6 | 56 | 25 | 4 | 22 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 4 | 2 | 0 | 4 |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 125 | - | - | 125 | - | - | - | - | 125 | - | - | - |
| Veh in Median Storage, \# | \# - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 |
| Heavy Vehicles, \% | 8 | 1 | 6 | 5 | 1 | 0 | 0 | 0 | 7 | 0 | 0 | 0 |
| Mvmt Flow | 13 | 268 | 35 | 60 | 458 | 42 | 34 | 6 | 58 | 26 | 4 | 23 |



Queuing and Blocking Report

Intersection: 1: Reas Ford Rd/Earlysville Forest Drive \& Earlysville Road

| Movement | EB | EB | WB | WB | NB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LT | R | LTR |
| Maximum Queue (ft) | 32 | 17 | 44 | 43 | 42 | 53 | 42 |
| Average Queue (ft) | 5 | 1 | 13 | 3 | 19 | 19 | 20 |
| 95th Queue (ft) | 21 | 9 | 38 | 20 | 39 | 44 | 37 |
| Link Distance (ft) |  | 905 |  | 1109 | 1192 |  | 755 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  | 125 |  |
| Storage Bay Dist (ft) | 125 |  | 125 |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |

## Network Summary

Network wide Queuing Penalty: 0

## Appendix F-5

## Alternative 2: Traffic Signal Conditions AM Peak

HCM 6th Signalized Intersection Summary Earlysville Rd with Reas Ford Rd Intersection Study 1: Reas Ford Rd/Earlysville Forest Drive \& Earlysville Road

|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 | $\dagger$ | $p$ | $V$ | $\frac{1}{1}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |  | $\uparrow$ | 「 |  | \& |  |
| Traffic Volume (veh/h) | 14 | 489 | 36 | 36 | 127 | 9 | 29 | 1 | 66 | 47 | 7 | 12 |
| Future Volume (veh/h) | 14 | 489 | 36 | 36 | 127 | 9 | 29 | 1 | 66 | 47 | 7 | 12 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 0.98 | 1.00 |  | 0.98 | 0.99 |  | 0.99 | 0.99 |  | 0.99 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1900 | 1885 | 1900 | 1856 | 1856 | 1900 | 1900 | 1900 | 1826 | 1900 | 1900 | 1781 |
| Adj Flow Rate, veh/h | 16 | 569 | 42 | 42 | 148 | 10 | 34 | 1 | 77 | 55 | 8 | 14 |
| Peak Hour Factor | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Percent Heavy Veh, \% | 0 | 1 | 0 | 3 | 3 | 0 | 0 | 0 | 5 | 0 | 0 | 8 |
| Cap, veh/h | 745 | 765 | 56 | 405 | 804 | 54 | 368 | 8 | 262 | 267 | 38 | 32 |
| Arrive On Green | 0.02 | 0.44 | 0.44 | 0.05 | 0.47 | 0.47 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| Sat Flow, veh/h | 1810 | 1731 | 128 | 1767 | 1716 | 116 | 1494 | 67 | 1529 | 869 | 308 | 262 |
| Grp Volume(v), veh/h | 16 | 0 | 611 | 42 | 0 | 158 | 35 | 0 | 77 | 77 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1810 | 0 | 1859 | 1767 | 0 | 1832 | 1561 | 0 | 1529 | 1439 | 0 | 0 |
| Q Serve(g_s), s | 0.2 | 0.0 | 10.6 | 0.5 | 0.0 | 1.9 | 0.0 | 0.0 | 1.7 | 1.2 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 0.2 | 0.0 | 10.6 | 0.5 | 0.0 | 1.9 | 0.7 | 0.0 | 1.7 | 1.9 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.07 | 1.00 |  | 0.06 | 0.97 |  | 1.00 | 0.71 |  | 0.18 |
| Lane Grp Cap(c), veh/h | 745 | 0 | 822 | 405 | 0 | 858 | 376 | 0 | 262 | 337 | 0 | 0 |
| V/C Ratio(X) | 0.02 | 0.00 | 0.74 | 0.10 | 0.00 | 0.18 | 0.09 | 0.00 | 0.29 | 0.23 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 942 | 0 | 2400 | 550 | 0 | 2366 | 930 | 0 | 863 | 893 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 5.7 | 0.0 | 9.0 | 6.7 | 0.0 | 6.0 | 15.2 | 0.0 | 14.0 | 15.6 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 1.4 | 0.1 | 0.0 | 0.1 | 0.1 | 0.0 | 0.6 | 0.3 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/In | 0.0 | 0.0 | 3.0 | 0.1 | 0.0 | 0.5 | 0.2 | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 5.7 | 0.0 | 10.3 | 6.8 | 0.0 | 6.1 | 15.3 | 0.0 | 14.6 | 16.0 | 0.0 | 0.0 |
| LnGrp LOS | A | A | B | A | A | A | B | A | B | B | A | A |
| Approach Vol, veh/h |  | 627 |  |  | 200 |  |  | 112 |  |  | 77 |  |
| Approach Delay, s/veh |  | 10.2 |  |  | 6.2 |  |  | 14.8 |  |  | 16.0 |  |
| Approach LOS |  | B |  |  | A |  |  | B |  |  | B |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration (G+Y+Rc), s | 6.8 | 22.1 |  | 9.8 | 5.8 | 23.1 |  | 9.8 |  |  |  |  |
| Change Period (Y+Rc), s | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |  | 5.0 |  |  |  |  |
| Max Green Setting (Gmax), s | 5.0 | 50.0 |  | 20.0 | 5.0 | 50.0 |  | 20.0 |  |  |  |  |
| Max Q Clear Time (g_c+l1), s | 2.5 | 12.6 |  | 3.7 | 2.2 | 3.9 |  | 3.9 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 4.5 |  | 0.3 | 0.0 | 0.9 |  | 0.3 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 10.4 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | B |  |  |  |  |  |  |  |  |  |

Queuing and Blocking Report

Intersection: 1: Reas Ford Rd/Earlysville Forest Drive \& Earlysville Road

| Movement | EB | EB | WB | WB | NB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LT | R | LTR |
| Maximum Queue (ft) | 25 | 179 | 54 | 106 | 54 | 68 | 64 |
| Average Queue (ft) | 5 | 73 | 16 | 25 | 15 | 20 | 25 |
| 95th Queue (ft) | 22 | 140 | 40 | 71 | 41 | 49 | 53 |
| Link Distance (ft) |  | 905 |  | 1109 | 1192 |  | 755 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  | 125 |  |
| Storage Bay Dist (ft) | 125 |  | 125 |  |  |  |  |
| Storage Blk Time (\%) |  | 1 |  | 0 |  |  |  |

## Network Summary

Network wide Queuing Penalty: 0

## Appendix F-6

## Alternative 2: Traffic Signal <br> Conditions <br> PM Peak

HCM 6th Signalized Intersection Summary Earlysville Rd with Reas Ford Rd Intersection Study 1: Reas Ford Rd/Earlysville Forest Drive \& Earlysville Road

|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 | $\dagger$ | $p$ | $V$ | $\frac{1}{1}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1 /}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |  | $\uparrow$ | 「 |  | \& |  |
| Traffic Volume (veh/h) | 13 | 260 | 34 | 58 | 444 | 41 | 33 | 6 | 56 | 25 | 4 | 22 |
| Future Volume (veh/h) | 13 | 260 | 34 | 58 | 444 | 41 | 33 | 6 | 56 | 25 | 4 | 22 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 0.98 | 0.99 |  | 0.99 | 0.99 |  | 0.96 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1781 | 1885 | 1811 | 1826 | 1885 | 1900 | 1900 | 1900 | 1796 | 1900 | 1900 | 1900 |
| Adj Flow Rate, veh/h | 13 | 268 | 35 | 60 | 458 | 42 | 34 | 6 | 58 | 26 | 4 | 23 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, \% | 8 | 1 | 6 | 5 | 1 | 0 | 0 | 0 | 7 | 0 | 0 | 0 |
| Cap, veh/h | 394 | 564 | 74 | 560 | 666 | 61 | 356 | 47 | 293 | 236 | 41 | 86 |
| Arrive On Green | 0.02 | 0.35 | 0.35 | 0.06 | 0.39 | 0.39 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| Sat Flow, veh/h | 1697 | 1633 | 213 | 1739 | 1697 | 156 | 1167 | 361 | 1502 | 547 | 315 | 661 |
| Grp Volume(v), veh/h | 13 | 0 | 303 | 60 | 0 | 500 | 40 | 0 | 58 | 53 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1697 | 0 | 1847 | 1739 | 0 | 1853 | 1529 | 0 | 1502 | 1523 | 0 | 0 |
| Q Serve(g_s), s | 0.2 | 0.0 | 4.2 | 0.7 | 0.0 | 7.3 | 0.0 | 0.0 | 1.1 | 0.0 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 0.2 | 0.0 | 4.2 | 0.7 | 0.0 | 7.3 | 0.6 | 0.0 | 1.1 | 0.9 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.12 | 1.00 |  | 0.08 | 0.85 |  | 1.00 | 0.49 |  | 0.43 |
| Lane Grp Cap(c), veh/h | 394 | 0 | 638 | 560 | 0 | 727 | 403 | 0 | 293 | 363 | 0 | 0 |
| V/C Ratio(X) | 0.03 | 0.00 | 0.48 | 0.11 | 0.00 | 0.69 | 0.10 | 0.00 | 0.20 | 0.15 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 677 | 0 | 2663 | 822 | 0 | 2729 | 1146 | 0 | 1066 | 1113 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 7.2 | 0.0 | 8.4 | 6.2 | 0.0 | 8.2 | 12.6 | 0.0 | 11.0 | 12.7 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 0.6 | 0.1 | 0.0 | 1.2 | 0.1 | 0.0 | 0.3 | 0.2 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/In | 0.0 | 0.0 | 1.1 | 0.1 | 0.0 | 1.9 | 0.2 | 0.0 | 0.3 | 0.3 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 7.2 | 0.0 | 8.9 | 6.3 | 0.0 | 9.4 | 12.7 | 0.0 | 11.3 | 12.9 | 0.0 | 0.0 |
| LnGrp LOS | A | A | A | A | A | A | B | A | B | B | A | A |
| Approach Vol, veh/h |  | 316 |  |  | 560 |  |  | 98 |  |  | 53 |  |
| Approach Delay, s/veh |  | 8.8 |  |  | 9.1 |  |  | 11.9 |  |  | 12.9 |  |
| Approach LOS |  | A |  |  | A |  |  | B |  |  | B |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration (G+Y+Rc), s | 7.1 | 16.3 |  | 9.2 | 5.6 | 17.8 |  | 9.2 |  |  |  |  |
| Change Period (Y+Rc), s | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |  | 5.0 |  |  |  |  |
| Max Green Setting (Gmax), s | 7.0 | 47.0 |  | 21.0 | 6.0 | 48.0 |  | 21.0 |  |  |  |  |
| Max Q Clear Time (g_c+l1), s | 2.7 | 6.2 |  | 3.1 | 2.2 | 9.3 |  | 2.9 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 1.9 |  | 0.3 | 0.0 | 3.5 |  | 0.2 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 9.5 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | A |  |  |  |  |  |  |  |  |  |

Queuing and Blocking Report

Intersection: 1: Reas Ford Rd/Earlysville Forest Drive \& Earlysville Road

| Movement | EB | EB | WB | WB | NB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LT | R | LTR |
| Maximum Queue (ft) | 37 | 126 | 55 | 162 | 59 | 52 | 39 |
| Average Queue (ft) | 7 | 51 | 21 | 64 | 20 | 17 | 17 |
| 95th Queue (ft) | 27 | 98 | 46 | 129 | 47 | 39 | 36 |
| Link Distance (ft) |  | 905 |  | 1109 | 1192 |  | 755 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  | 125 |  |
| Storage Bay Dist (ft) | 125 |  | 125 |  |  |  |  |
| Storage Blk Time (\%) |  | 0 |  | 1 |  |  |  |

## Network Summary

Network wide Queuing Penalty: 0

## Appendix F-7

## Alternative 3: Roundabout Conditions AM Peak

## LANE SUMMARY

## © Site: 1 [2021 AM Peak (Site Folder: Earlysville Rd with Reas

Ford Rd)]
Proposed Single-Lane Roundabout
Site Category: Proposed Design 1
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Cap. <br> veh/h | Deg. Satn v/c | Lane Util. \% | Aver. Delay sec | Level of Service |  | K OF E Dist ] ft | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. <br> \% |
| South: Reas Ford Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 112 | 3.4 | 729 | 0.153 | 100 | 6.6 | LOS A | 0.9 | 24.1 | Full | 1600 | 0.0 | 0.0 |
| Approach | 112 | 3.4 |  | 0.153 |  | 6.6 | LOS A | 0.9 | 24.1 |  |  |  |  |
| East: Earlysville Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 200 | 2.8 | 1267 | 0.158 | 100 | 4.2 | LOS A | 1.0 | 25.0 | Full | 1000 | 0.0 | 0.0 |
| Approach | 200 | 2.8 |  | 0.158 |  | 4.2 | LOS A | 1.0 | 25.0 |  |  |  |  |
| North: Earlysville Forest Drive |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 77 | 1.5 | 1098 | 0.070 | 100 | 3.9 | LOS A | 0.4 | 9.3 | Full | 1600 | 0.0 | 0.0 |
| Approach | 77 | 1.5 |  | 0.070 |  | 3.9 | LOS A | 0.4 | 9.3 |  |  |  |  |
| West: Earlysville Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 627 | 0.9 | 1230 | 0.509 | 100 | 8.5 | LOS A | 4.4 | 109.7 | Full | 1600 | 0.0 | 0.0 |
| Approach | 627 | 0.9 |  | 0.509 |  | 8.5 | LOS A | 4.4 | 109.7 |  |  |  |  |
| Intersection | 1015 | 1.6 |  | 0.509 |  | 7.1 | LOS A | 4.4 | 109.7 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS $F$ will result if $v / c>1$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).
Roundabout Capacity Model: SIDRA Standard.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

## Approach Lane Flows (veh/h)

| South: Reas Ford Road |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov. <br> From S To Exit: | L2 W | T1 N | R2 E | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob SL Ov. \% | $\begin{array}{r} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{array}$ |
| Lane 1 | 34 | 1 | 77 | 112 | 3.4 | 729 | 0.153 | 100 | NA | NA |
| Approach | 34 | 1 | 77 | 112 | 3.4 |  | 0.153 |  |  |  |
| East: Earlysville Road |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From E <br> To Exit: | L2 S | T1 W | R2 N | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{array}{r} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{array}$ |
| Lane 1 | 42 | 148 | 10 | 200 | 2.8 | 1267 | 0.158 | 100 | NA | NA |


| Approach | 42 | 148 | 10 | 200 | 2.8 | 0.158 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North: Earlysville Forest Drive |  |  |  |  |  |  |  |  |  |
| Mov. <br> From N To Exit: | L2 E | T1 | R2 W | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | Ov. Lane No. |
| Lane 1 | 55 | 8 | 14 | 77 | 1.5 | 1098 | 0.070 | 100 NA | NA |
| Approach | 55 | 8 | 14 | 77 | 1.5 |  | 0.070 |  |  |
| West: Earlysville Road |  |  |  |  |  |  |  |  |  |
| Mov. <br> From W <br> To Exit | L2 N | T1 E | R2 S | Total | \%HV | Cap. veh/h | Deg. Satn v/c | $\begin{array}{cr} \text { Lane } & \text { Prob. } \\ \text { Util. SL Ov. } \\ \% & \% \end{array}$ | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 16 | 569 | 42 | 627 | 0.9 | 1230 | 0.509 | 100 NA | NA |
| Approach | 16 | 569 | 42 | 627 | 0.9 |  | 0.509 |  |  |
| Total \%HV Deg.Satn (v/c) |  |  |  |  |  |  |  |  |  |
| Intersection | 1015 | 1.6 |  | 0.509 |  |  |  |  |  |

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.

| Merge Analysis |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} \text { Exit } \\ \text { Lane } \\ \text { Number } \end{array}$ | Short Percent Opposing Lane Opng in Flow Rate Length Lane <br> \% veh/h pcu/h | Critical Gap | Follow-up Lane Headway Flow Rate sec veh/h | Capacity <br> veh/h | Deg. Min. Satn Delay v/c sec | Merge Delay |
| South Exit: Reas Ford Road Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |
| East Exit: Earlysville Road Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |
| North Exit: Earlysville Forest Drive Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |
| West Exit: Earlysville Road Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |

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## Appendix F-8

## Alternative 3: Roundabout Conditions PM Peak

## LANE SUMMARY

## © Site: 1 [2021 PM Peak (Site Folder: Earlysville Rd with Reas

Ford Rd)]
Proposed Single-Lane Roundabout
Site Category: Proposed Design 1
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Cap. <br> veh/h | Deg. Satn v/c | Lane Util. \% | Aver. Delay sec | Level of Service | 95\% <br> [ Veh | $\begin{gathered} \mathrm{K} \text { OF } \\ \mathrm{JE} \\ \text { Dist ] } \\ \mathrm{ft} \end{gathered}$ | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. <br> \% |
| South: Reas Ford Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 98 | 4.1 | 987 | 0.099 | 100 | 4.6 | LOS A | 0.5 | 14.1 | Full | 1600 | 0.0 | 0.0 |
| Approach | 98 | 4.1 |  | 0.099 |  | 4.6 | LOS A | 0.5 | 14.1 |  |  |  |  |
| East: Earlysville Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 560 | 1.4 | 1285 | 0.436 | 100 | 7.1 | LOS A | 3.6 | 91.1 | Full | 1000 | 0.0 | 0.0 |
| Approach | 560 | 1.4 |  | 0.436 |  | 7.1 | LOS A | 3.6 | 91.1 |  |  |  |  |
| North: Earlysville Forest Drive |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 53 | 0.0 | 848 | 0.062 | 100 | 4.9 | LOS A | 0.4 | 8.8 | Full | 1600 | 0.0 | 0.0 |
| Approach | 53 | 0.0 |  | 0.062 |  | 4.9 | LOS A | 0.4 | 8.8 |  |  |  |  |
| West: Earlysville Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 316 | 1.9 | 1235 | 0.256 | 100 | 5.2 | LOS A | 1.6 | 40.9 | Full | 1600 | 0.0 | 0.0 |
| Approach | 316 | 1.9 |  | 0.256 |  | 5.2 | LOS A | 1.6 | 40.9 |  |  |  |  |
| Intersection | 1027 | 1.7 |  | 0.436 |  | 6.2 | LOS A | 3.6 | 91.1 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS $F$ will result if $v / c>1$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).
Roundabout Capacity Model: SIDRA Standard.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

## Approach Lane Flows (veh/h)

| South: Reas Ford Road |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov. <br> From S To Exit: | L2 W | T1 N | R2 E | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob SL Ov. \% | $\begin{array}{r} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{array}$ |
| Lane 1 | 34 | 6 | 58 | 98 | 4.1 | 987 | 0.099 | 100 | NA | NA |
| Approach | 34 | 6 | 58 | 98 | 4.1 |  | 0.099 |  |  |  |
| East: Earlysville Road |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From E <br> To Exit: | L2 S | T1 W | R2 N | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{array}{r} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{array}$ |
| Lane 1 | 60 | 458 | 42 | 560 | 1.4 | 1285 | 0.436 | 100 | NA | NA |


| Approach | 60 | 458 | 42 | 560 | 1.4 | 0.436 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North: Earlysville Forest Drive |  |  |  |  |  |  |  |  |  |
| Mov. <br> From N To Exit: | L2 E | T1 | R2 W | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Prob. Util. SL Ov. \% \% | Ov. Lane No. |
| Lane 1 | 26 | 4 | 23 | 53 | 0.0 | 848 | 0.062 | 100 NA | NA |
| Approach | 26 | 4 | 23 | 53 | 0.0 |  | 0.062 |  |  |
| West: Earlysville Road |  |  |  |  |  |  |  |  |  |
| Mov. <br> From W <br> To Exit | L2 N | T1 E | R2 S | Total | \%HV | Cap. veh/h | Deg. Satn v/c | $\begin{array}{cr} \text { Lane } & \text { Prob. } \\ \text { Util. SL Ov. } \\ \% & \% \end{array}$ | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 13 | 268 | 35 | 316 | 1.9 | 1235 | 0.256 | 100 NA | NA |
| Approach | 13 | 268 | 35 | 316 | 1.9 |  | 0.256 |  |  |
| Total \%HV Deg.Satn (v/c) |  |  |  |  |  |  |  |  |  |
| Intersection | 1027 | 1.7 |  | 0.436 |  |  |  |  |  |

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.

| Merge Analysis |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} \text { Exit } \\ \text { Lane } \\ \text { Number } \end{array}$ | Short Percent Opposing Lane Opng in Flow Rate Length Lane <br> \% veh/h pcu/h | Critical Gap | Follow-up Lane Headway Flow Rate sec veh/h | Capacity <br> veh/h | Deg. Min. Satn Delay v/c sec | Merge Delay |
| South Exit: Reas Ford Road Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |
| East Exit: Earlysville Road Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |
| North Exit: Earlysville Forest Drive Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |
| West Exit: Earlysville Road Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |

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## Appendix F-9

## Alternative 4: AWSC Conditions AM Peak

| Intersection |  |
| :--- | :---: |
| Intersection Delay, s/veh | 22 |
| Intersection LOS | C |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ | 「 |  | ¢ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 14 | 489 | 36 | 36 | 127 | 9 | 29 | 1 | 66 | 47 | 7 | 12 |
| Future Vol, veh/h | 14 | 489 | 36 | 36 | 127 | 9 | 29 | 1 | 66 | 47 | 7 | 12 |
| Peak Hour Factor | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Heavy Vehicles, \% | 0 | 1 | 0 | 3 | 3 | 0 | 0 | 0 | 5 | 0 | 0 | 8 |
| Mvmt Flow | 16 | 569 | 42 | 42 | 148 | 10 | 34 | 1 | 77 | 55 | 8 | 14 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 2 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 2 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 2 |  |  | 1 |  |  |
| HCM Control Delay | 29 |  |  | 11.1 |  |  | 10.1 |  |  | 10.3 |  |  |
| HCM LOS | D |  |  | B |  |  | B |  |  | B |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | WBLn2 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $30 \%$ | $3 \%$ | $22 \%$ | $0 \%$ | $71 \%$ |
| Vol Thru, \% | $1 \%$ | $91 \%$ | $78 \%$ | $0 \%$ | $11 \%$ |
| Vol Right, \% | $69 \%$ | $7 \%$ | $0 \%$ | $100 \%$ | $18 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 96 | 539 | 163 | 9 | 66 |
| LT Vol | 29 | 14 | 36 | 0 | 47 |
| Through Vol | 1 | 489 | 127 | 0 | 7 |
| RT Vol | 66 | 36 | 0 | 9 | 12 |
| Lane Flow Rate | 112 | 627 | 190 | 10 | 77 |
| Geometry Grp | 2 | 5 | 7 | 7 | 2 |
| Degree of Util (X) | 0.18 | 0.85 | 0.31 | 0.015 | 0.133 |
| Departure Headway (Hd) | 5.793 | 4.882 | 5.886 | 5.064 | 6.258 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 617 | 746 | 610 | 706 | 571 |
| Service Time | 3.846 | 2.882 | 3.621 | 2.799 | 4.316 |
| HCM Lane V/C Ratio | 0.182 | 0.84 | 0.311 | 0.014 | 0.135 |
| HCM Control Delay | 10.1 | 29 | 11.3 | 7.9 | 10.3 |
| HCM Lane LOS | B | D | B | A | B |
| HCM 95th-tile Q | 0.7 | 9.9 | 1.3 | 0 | 0.5 |

Queuing and Blocking Report

Intersection: 1: Reas Ford Rd/Earlysville Forest Drive \& Earlysville Road

| Movement | EB | WB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LT | R | LTR | LTR |
| Maximum Queue (ft) | 190 | 74 | 28 | 60 | 46 |
| Average Queue (ft) | 94 | 33 | 8 | 28 | 18 |
| 95th Queue (ft) | 163 | 58 | 27 | 50 | 35 |
| Link Distance (ft) | 906 | 1105 |  | 1198 | 748 |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |
| Storage Bay Dist (ft) |  | 0 | 100 |  |  |
| Storage Blk Time (\%) |  | 0 |  |  |  |
| Queuing Penalty (veh) |  | 0 |  |  |  |

## Network Summary

Network wide Queuing Penalty: 0

## Appendix F-10

## Alternative 4: AWSC Conditions PM Peak

| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 18.5 |
| Intersection LOS | C |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | $\uparrow$ | 「 |  | * |  |  | \& |  |
| Traffic Vol, veh/h | 13 | 260 | 34 | 58 | 444 | 41 | 33 | 6 | 56 | 25 | 4 | 22 |
| Future Vol, veh/h | 13 | 260 | 34 | 58 | 444 | 41 | 33 | 6 | 56 | 25 | 4 | 22 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles, \% | 8 | 1 | 6 | 5 | 1 | 0 | 0 | 0 | 7 | 0 | 0 | 0 |
| Mvmt Flow | 13 | 268 | 35 | 60 | 458 | 42 | 34 | 6 | 58 | 26 | 4 | 23 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 2 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 2 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 2 |  |  | 1 |  |  |
| HCM Control Delay | 12.9 |  |  | 23.9 |  |  | 10.1 |  |  | 9.8 |  |  |
| HCM LOS | B |  |  | C |  |  | B |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | WBLn2 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $35 \%$ | $4 \%$ | $12 \%$ | $0 \%$ | $49 \%$ |
| Vol Thru, \% | $6 \%$ | $85 \%$ | $88 \%$ | $0 \%$ | $8 \%$ |
| Vol Right, \% | $59 \%$ | $11 \%$ | $0 \%$ | $100 \%$ | $43 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 95 | 307 | 502 | 41 | 51 |
| LT Vol | 33 | 13 | 58 | 0 | 25 |
| Through Vol | 6 | 260 | 444 | 0 | 4 |
| RT Vol | 56 | 34 | 0 | 41 | 22 |
| Lane Flow Rate | 98 | 316 | 518 | 42 | 53 |
| Geometry Grp | 2 | 5 | 7 | 7 | 2 |
| Degree of Util (X) | 0.161 | 0.465 | 0.786 | 0.054 | 0.09 |
| Departure Headway (Hd) | 5.929 | 5.292 | 5.466 | 4.633 | 6.174 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 604 | 680 | 668 | 778 | 579 |
| Service Time | 3.973 | 3.32 | 3.166 | 2.333 | 4.223 |
| HCM Lane VIC Ratio | 0.162 | 0.465 | 0.775 | 0.054 | 0.092 |
| HCM Control Delay | 10.1 | 12.9 | 25.2 | 7.6 | 9.8 |
| HCM Lane LOS | B | B | D | A | A |
| HCM 95th-tile Q | 0.6 | 2.5 | 7.7 | 0.2 | 0.3 |

Queuing and Blocking Report

Intersection: 1: Reas Ford Rd/Earlysville Forest Drive \& Earlysville Road

| Movement | EB | WB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LT | R | LTR | LTR |
| Maximum Queue (ft) | 92 | 172 | 77 | 60 | 33 |
| Average Queue (ft) | 53 | 72 | 22 | 27 | 15 |
| 95th Queue (ft) | 77 | 129 | 57 | 49 | 28 |
| Link Distance (ft) | 906 | 1105 |  | 1198 | 748 |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |
| Storage Bay Dist (ft) |  | 3 | 100 |  |  |
| Storage Blk Time (\%) |  | 1 |  |  |  |
| Queuing Penalty (veh) |  | 1 |  |  |  |

## Network Summary

Network wide Queuing Penalty: 1

## Appendix G

## Auxiliary Lane Analysis

## Appendix G-1

## Earlysville Road Northbound 2021 Existing Conditions

## Earlysville Road Northbound - 2021 AM Peak



FIGURE 3-6 WARRANT FOR LEFT TURN STORAGE LANES ON TWO LANE HIGHWAY


FIGURE 3-7 WARRANT FOR LEFT TURN STORAGE LANES ON TWO LANE HIGHWAY

Earlysville Road Northbound - 2021 AM Peak


FIGURE 3-26 WARRANTS FOR RIGHT TURN TREATMENT (2-LANE HIGHWAY)

Appropriate Radius required at all Intersections and Entrances (Commercial or Private).

## LEGEND

PHV - Peak Hour Volume (also Design Hourly Volume equivalent)

## Adjustment for Right Turns

For posted speeds at or under $45 \mathrm{mph}, \mathrm{PHV}$ right turns $>40$, and PHV total < 300.
Adjusted right turns = PHV Right Turns - 20
If PHV is not known use formula: $\mathrm{PHV}=\mathrm{ADT} \times \mathrm{K} \times \mathrm{D}$
$\mathrm{K}=$ the percent of AADT occurring in the peak hour
$D=$ the percent of traffic in the peak direction of flow
Note: An average of $11 \%$ for K x D will suffice.
When right turn facilities are warranted, see Figure 3-1 for design criteria.*

[^0]Earlysville Road Northbound - 2021 PM Peak
WARRANT FOR LEFT-TURN STORAGE LANES ON TWO-LANE HIGHWAY


FIGURE 3-4 WARRANT FOR LEFT TURN STORAGE LANES ON TWO LANE HIGHWAY


FIGURE 3-5 WARRANT FOR LEFT TURN STORAGE LANES ON TWO LANE HIGHWAY

Earlysville Road Northbound - 2021 PM Peak


FIGURE 3-26 WARRANTS FOR RIGHT TURN TREATMENT (2-LANE HIGHWAY)

Appropriate Radius required at all Intersections and Entrances (Commercial or Private).

## LEGEND

PHV - Peak Hour Volume (also Design Hourly Volume equivalent)

## Adjustment for Right Turns

For posted speeds at or under $45 \mathrm{mph}, \mathrm{PHV}$ right turns $>40$, and PHV total < 300.
Adjusted right turns = PHV Right Turns - 20
If PHV is not known use formula: $\mathrm{PHV}=\mathrm{ADT} \times \mathrm{K} \times \mathrm{D}$
$\mathrm{K}=$ the percent of AADT occurring in the peak hour
$D=$ the percent of traffic in the peak direction of flow
Note: An average of $11 \%$ for K x D will suffice.
When right turn facilities are warranted, see Figure 3-1 for design criteria.*

[^1]
## Appendix G-2

## Earlysville Road Southbound 2021 Existing Conditions

Earlysville Road Southbound - 2021 AM Peak
WARRANT FOR LEFT-TURN STORAGE LANES ON TWO-LANE HIGHWAY


FIGURE 3-4 WARRANT FOR LEFT TURN STORAGE LANES ON TWO LANE HIGHWAY


FIGURE 3-5 WARRANT FOR LEFT TURN STORAGE LANES ON TWO LANE HIGHWAY

Earlysville Road Southbound - 2021 AM Peak


FIGURE 3-26 WARRANTS FOR RIGHT TURN TREATMENT (2-LANE HIGHWAY)

Appropriate Radius required at all Intersections and Entrances (Commercial or Private).

## LEGEND

PHV - Peak Hour Volume (also Design Hourly Volume equivalent)

## Adjustment for Right Turns

For posted speeds at or under $45 \mathrm{mph}, \mathrm{PHV}$ right turns $>40$, and PHV total < 300.
Adjusted right turns = PHV Right Turns - 20
If PHV is not known use formula: $\mathrm{PHV}=\mathrm{ADT} \times \mathrm{K} \times \mathrm{D}$
$\mathrm{K}=$ the percent of AADT occurring in the peak hour
$D=$ the percent of traffic in the peak direction of flow
Note: An average of $11 \%$ for K x D will suffice.
When right turn facilities are warranted, see Figure 3-1 for design criteria.*

[^2]Earlysville Road Southbound - 2021 PM Peak
WARRANT FOR LEFT-TURN STORAGE LANES ON TWO-LANE HIGHWAY


FIGURE 3-4 WARRANT FOR LEFT TURN STORAGE LANES ON TWO LANE HIGHWAY


FIGURE 3-5 WARRANT FOR LEFT TURN STORAGE LANES ON TWO LANE HIGHWAY

Earlysville Road Southbound - 2021 PM Peak


FIGURE 3-26 WARRANTS FOR RIGHT TURN TREATMENT (2-LANE HIGHWAY)

Appropriate Radius required at all Intersections and Entrances (Commercial or Private).

## LEGEND

PHV - Peak Hour Volume (also Design Hourly Volume equivalent)

## Adjustment for Right Turns

For posted speeds at or under $45 \mathrm{mph}, \mathrm{PHV}$ right turns $>40$, and PHV total < 300.
Adjusted right turns = PHV Right Turns - 20
If PHV is not known use formula: $\mathrm{PHV}=\mathrm{ADT} \times \mathrm{K} \times \mathrm{D}$
$\mathrm{K}=$ the percent of AADT occurring in the peak hour
$D=$ the percent of traffic in the peak direction of flow
Note: An average of $11 \%$ for K x D will suffice.
When right turn facilities are warranted, see Figure 3-1 for design criteria.*

[^3]
## Appendix G-3

## Reas Ford Road Eastbound 2021 Existing Conditions

Reas Ford Road Eastbound - 2021 AM Peak


FIGURE 3-26 WARRANTS FOR RIGHT TURN TREATMENT (2-LANE HIGHWAY)

Appropriate Radius required at all Intersections and Entrances (Commercial or Private).

## LEGEND

PHV - Peak Hour Volume (also Design Hourly Volume equivalent)

## Adjustment for Right Turns

For posted speeds at or under $45 \mathrm{mph}, \mathrm{PHV}$ right turns $>40$, and PHV total < 300.
Adjusted right turns = PHV Right Turns - 20
If PHV is not known use formula: $\mathrm{PHV}=\mathrm{ADT} \times \mathrm{K} \times \mathrm{D}$
$K=$ the percent of AADT occurring in the peak hour
$D=$ the percent of traffic in the peak direction of flow
Note: An average of $11 \%$ for K x D will suffice.
When right turn facilities are warranted, see Figure 3-1 for design criteria.*

[^4]

FIGURE 3-26 WARRANTS FOR RIGHT TURN TREATMENT (2-LANE HIGHWAY)

Appropriate Radius required at all Intersections and Entrances (Commercial or Private).

## LEGEND

PHV - Peak Hour Volume (also Design Hourly Volume equivalent)

## Adjustment for Right Turns

For posted speeds at or under $45 \mathrm{mph}, \mathrm{PHV}$ right turns $>40$, and PHV total < 300.
Adjusted right turns = PHV Right Turns - 20
If PHV is not known use formula: $\mathrm{PHV}=\mathrm{ADT} \times \mathrm{K} \times \mathrm{D}$
$\mathrm{K}=$ the percent of AADT occurring in the peak hour
$D=$ the percent of traffic in the peak direction of flow
Note: An average of $11 \%$ for K x D will suffice.
When right turn facilities are warranted, see Figure 3-1 for design criteria.*

[^5]
## Appendix G-4

## Earlysville Forest Drive Westbound 2021 Existing Conditions

Earlysville Forest Drive Westbound - 2021 AM Peak


FIGURE 3-26 WARRANTS FOR RIGHT TURN TREATMENT (2-LANE HIGHWAY)

Appropriate Radius required at all Intersections and Entrances (Commercial or Private).

## LEGEND

PHV - Peak Hour Volume (also Design Hourly Volume equivalent)

## Adjustment for Right Turns

For posted speeds at or under $45 \mathrm{mph}, \mathrm{PHV}$ right turns $>40$, and PHV total < 300.
Adjusted right turns = PHV Right Turns - 20
If PHV is not known use formula: $\mathrm{PHV}=\mathrm{ADT} \times \mathrm{K} \times \mathrm{D}$
$K=$ the percent of AADT occurring in the peak hour
$D=$ the percent of traffic in the peak direction of flow
Note: An average of $11 \%$ for K x D will suffice.
When right turn facilities are warranted, see Figure 3-1 for design criteria.*

[^6]Earlysville Forest Drive Westbound - 2021 PM Peak


FIGURE 3-26 WARRANTS FOR RIGHT TURN TREATMENT (2-LANE HIGHWAY)

Appropriate Radius required at all Intersections and Entrances (Commercial or Private).

## LEGEND

PHV - Peak Hour Volume (also Design Hourly Volume equivalent)

## Adjustment for Right Turns

For posted speeds at or under $45 \mathrm{mph}, \mathrm{PHV}$ right turns $>40$, and PHV total < 300.
Adjusted right turns = PHV Right Turns - 20
If PHV is not known use formula: $\mathrm{PHV}=\mathrm{ADT} \times \mathrm{K} \times \mathrm{D}$
$\mathrm{K}=$ the percent of AADT occurring in the peak hour
$D=$ the percent of traffic in the peak direction of flow
Note: An average of $11 \%$ for K x D will suffice.
When right turn facilities are warranted, see Figure 3-1 for design criteria.*

[^7]
## Appendix H

## CMF Data

## VDOT

## VIRGINIA STATE PREFERRED CMF LIST

VIRGINIA STATE PREFERRED CMF LIST

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## Introduction

A crash modification factor (CMF) is a useful tool for estimating changes in safety performance that can be expected when implementing a countermeasure. Developed using various forms of statistical analyses, they provide average changes in crash frequency, and sometimes severity, which are commonly observed when a treatment is installed.

Almost all CMFs can be found in the Crash Modification Factors Clearinghouse, a web-based repository of more than 6,000 CMFs covering hundreds of treatments. Often, a search for a countermeasure on the website will return many CMFs for a single treatment. As a result, this document was developed.

The Virginia State Preferred CMF List is a condensed directory with common CMFs relative to Virginia. The State preferred list contains CMFs with high quality ratings and includes the applicable crash type, area type, severity, service life, functional class, and site description. These CMFs will be used to support Virginia's HSIP program as well as other, broader applications.

## CMF Example - Convert At-Grade Intersection to Interchange

The study intersection has experienced the following 15 crashes in one year:

| Severity | K | A | BC | O |
| :--- | :---: | :---: | :---: | :---: |
| Crashes | 1 | 2 | 5 | 7 |

Engineers want to convert this intersection to an interchange. Find CMFs in document
(as shown in Figure A-1) and calculate how many crashes of each severity can be reduced.
In the HSIP application, use all applicable CMFs as shown below:

- $K_{\text {reauced }}=1$ crash per year * $(1-0.58)=0.42$ crashes per year
- $A_{\text {reduced }}=2$ crashes per year * $(1-0.43)=1.14$ crashes per year
- $B C_{\text {reduced }}=5$ crashes per year * $(1-0.43)=2.85$ crashes per year
- $O_{\text {reduced }}=7$ crashes per year * $(1-0.64)=2.52$ crashes per year


## WHAT IS A CMF?

Mathematically, a CMF is a multiplicative factor used to compute the expected number of crashes after implementing a given countermeasure at a specific site. For example, a countermeasure expected to reduce the number of injury crashes by 23 percent will have a CMF of 0.77 ( $1-[23 / 100]=0.77)$. On the other hand, if the treatment is expected to increase the number of property damage crashes by 23 percent, the CMF will be $=1-(-23 / 100)=1.23$.

To estimate future expected crash frequency with the treatment, the CMFs are applied to expected crash frequency assuming no changes. For example, a stop-controlled intersection is expected to experience five crashes per year. A treatment is installed with a CMF of 0.77 , so the expected crash frequency with the installation would be $5 * 0.77=3.85$, a reduction of 1.15 crashes per year.

## HOW TO USE THIS DOCUMENT

This document consists of three tables spread over multiple pages which describe and provide supporting documentation for the CMFs. Descriptions of each table are provided later in this section. CMFs should be selected based on applicability, where the characteristics associated with the CMF closely match the characteristics of the scenario at hand. For example, CMFs often vary by crash type and crash severity. CMFs may also be specific to urban or rural areas and should be applied to situations that match.

As an example, consider the CMF "Convert At-Grade Intersection to Interchange" shown in Figure A-1. The location of interest is 4-leg at-grade intersection, and a new interchange was suggested by a safety assessment team to help mitigate crashes at this intersection. Use the CMF by crash severity to determine the expected number of crashes for the applicable severity.

Figure A-1 Convert Intersection to Interchange CMF Information

| COUNTERMEASURE | CRASH TYPE | AREA TYPE | K | A | BC | 0 | SERVICE LIFE | FUNCTIONAL CLASS | SITE DESCRIPTION | PRIOR CONDITION | REFERENCE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Convert At-Grade Intersection to Interchange | ALL | - | 0.58 | 0.43 | 0.43 | 0.64 | 20 | - | 4-Leg Intersection | At-Grade Intersection | $\begin{aligned} & \text { CMF ID: } 459, \\ & 460,461 \end{aligned}$ |

## Table 1: Virginia State Preferred CMF List

Table 1 provides CMFs by crash type and severity for the identified countermeasures. The countermeasures are separated into four categories: bike/ped, interchanges, intersections, and segments. For each countermeasure, the following information is provided:

- Countermeasure name;
- Applicable crash type, using codes defined within the key;
- Applicable area type, using codes defined within the key;
- CMFs for four severity categories;
- Fatal Crash (K);
- Suspected Serious Injury Crash (A)
- Suspected Minor Injury and Possible Injury Crashes (BC); and
- Property Damage Only (PDO) Crash (O).
- The anticipated service life for the treatment;
- The applicable functional class;
- A general site description;
- The designated prior condition for the countermeasure; and
- References for the CMF(s).

When applying these CMFs, analysts should be careful to apply the CMF only to the designated crash types and severities. However, these crash types should not limit consideration of the countermeasure's usage. Just because a CMF is not available for the specific conditions does not mean the countermeasure is not useful in that context, it just might not have been researched yet.

Countermeasures with ** listed for a CMF indicate this CMF is defined using an equation, which can be found in Table 2.

## Table 2: CMFunction Equations

Some CMFs may require the use of an equation, which can be called Crash Modification Functions (CMFunctions), and the equations are provided in Table 2. For some of the more complex CMFunctions, an online calculator has been provided to assist users in determining the expected number of crashes. This calculator can be found on VDOT's HSIP website.

The equations are functions of existing and proposed conditions, with the units varying based on the CMF; the units can be verified in the Units column. In all cases, the existing condition is represented as the variable $X$ and the proposed condition is represented as the variable Y. For equations that are not on the website, simply enter the existing and proposed conditions into the appropriate equation using the designated units. The resulting value from the equation is the CMF.

The countermeasures in Table 2 are divided into three categories: interchanges, intersections, and segments. Data provided for the countermeasures in Table 2 include:

- Countermeasure name.
- CMFunctions for four severity categories:
- Fatal Crash (K);
- Suspected Serious Injury Crash (A);
- Suspected Minor Injury and Possible Injury Crashes (BC); and
- Property Damage Only (PDO) Crash (O).
- Units for the existing and proposed conditions.

The resulting CMFs from the equation should be cross-referenced with Table 1 to ensure the CMF is being applied to the appropriate crash types.

## Table 3: References

Specific references for the selected CMFs are provided in Table 3. The countermeasures in Table 3 are divided into four categories: bike/ped, interchanges, intersections, and segments. For each countermeasure, four pieces of data are provided:

- Countermeasure name;
- The shorthand reference from Table 1;
- The hyperlink for the first reference; and
- The hyperlink for the second reference, when applicable.

If there are questions about the study design, applicability, and/or prior conditions of a CMF, the analyst can refer to the linked documents, which can offer some clarification from the authors of the CMF study.

## CAN'T FIND YOUR COUNTERMEASURE?

The list below contains an exhaustive list of countermeasures used in Virginia. If the user is proposing a countermeasure that cannot be located on this list, they are to identify relevant research supporting an estimated CMF value and submit this documentation to VDOT HSIP staff for review and approval.

## PREFERRED CMF LIST KEY

## Crash Type

VP Vehicle-Pedestrian
VT Vehicle-Train
SV Single Vehicle
CM Cross-Median
F Frontal
0 Opposing Direction Sideswipe

- Refer to the CMF Calculator on the HSIP website
$\Delta$ Refer to specific treatment.
** Refer to Equations Sheet on page 16.


## Key <br> Area Type

U+S Urban and Suburban
Sub Suburban

VIRGINIA STATE PREFERRED CMF LIST

Table 1 Virginia State Preferred CMF List


VIRGINIA STATE PREFERRED CMF LIST

## Table 1 Virginia State Preferred CMF List (cont)

|  | COUNTERMEASURE | CRASH <br> TYPE | AREA <br> TYPE | K | A | BC | 0 | SERVICE <br> LIFE | FUNCTIONAL CLASS | SITE DESCRIPTION | PRIOR CONDITION | REFERENCE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Install Raised Pedestrian Crossing | ALL | - | 0.64 | 0.64 | 0.64 | 0.7 | 20 | - | Pedestrian Crossing | At-Grade Pedestrian Crossing | PED CMF <br> Toolbox |
|  | Prohibit Left Turns | VP | - | 0.9 | 0.9 | 0.9 | 0.9 | 6 | - | Intersection with Left Turns into Pedestrian Crossings | Left Turns Allowed | Ped CMF <br> Toolbox |
|  | Remove Parking Near Intersection | VP | - | 0.7 | 0.7 | 0.7 | 0.7 | $\Delta$ | - | Intersection with Parking on Approaches | Parking Present Near Intersection Approaches | PED CMF <br> Toolbox |
|  | Upgrade Crosswalk to High-Visibility | VP | - | 0.52 | 0.52 | 0.52 | 0.52 | 2 | - | Pedestrian Crosswalk | Standard Crosswalk Markings | CMF ID: 4658 |
|  | Widen Sidewalk at Intersection | ALL | - | 1 | 1.12 | 1.12 | 1 | 20 | - | Intersection with Sidewalks | Existing Sidewalk Width | CMF ID: 413 |
|  | Add Auxiliary Lane Between Entrance and Exit Ramps | ALL | - | 0.77 | 0.77 | 0.77 | 0.79 | 20 | Principal <br> Arterial- Other <br> Freeways and <br> Expressways | Freeway Interchange Weaving Area | No Auxiliary Lane Present | $\begin{aligned} & \text { CMF ID: 7440, } \\ & 7441 \end{aligned}$ |
|  | Add Collector-Distributor Road | ALL | - | 0.9 | 0.9 | 0.9 | 0.9 | 20 | - | Freeway Interchange Area | No Collector-Distributor Road Present | ISATe, HSM <br> Chapters 18 and 19 |
|  | Add Entrance Ramp to One Side of Freeway | ALL | - | - | - | - | - | 20 | - | Directional Freeway Segment | Freeway Segment with No Entrance Ramp | ISATe, HSM Chapters 18 and 19 |
|  | Add Exit Ramp to One Side of Freeway | ALL | - | - | A | A | - | 20 | - | Directional Freeway Segment | Freeway Segment with No Exit Ramp | ISATe, HSM Chapters 18 and 19 |
|  | Convert Diamond Interchange to Diverging Diamond Interchange | ALL | Sub | 0.59 | 0.59 | 0.59 | 0.67 | 20 | Principal Arterial Interstate | Diamond Interchange | Traditional Diamond Interchange | $\begin{aligned} & \text { CMF ID: 8258, } \\ & 8278 \end{aligned}$ |
|  | Convert Diamond Interchange to SPUI | ALL | - | 0.62 | 0.62 | 0.62 | 0.62 | 20 | - | Diamond Interchange | Traditional Diamond Interchange | VDOT Planning Level CMFs |
|  | Extend Deceleration Lane Length by 100 Feet | ALL | - | 0.93 | 0.93 | 0.93 | 0.93 | 20 | - | Freeway Segment with Deceleration Lane | Existing Deceleration Lane Length | CMD ID: 475 |
|  | Interchange Lighting | Night <br> Time | - | 0.5 | 0.5 | 0.5 | 0.5 | 15 | Principal Arterial Interstate | Freeway Interchange | No Highway Lighting Present | CMF ID: 1283 |
|  | Lengthen Acceleration Lane from X Miles to Y Miles | ALL | - | ** | ** | ** | ** | 20 | Principal <br> Arterial - <br> Interstate | Freeway Segment with Acceleration Lane | Existing Acceleration Lane of Length X Miles | $\begin{aligned} & \text { CMF ID: 5215, } \\ & 5216 \end{aligned}$ |
|  | Replace Loop Ramp with Short Direct Ramp | ALL | - | 0.7 | 0.7 | 0.7 | 0.7 | 20 | - | Interchange Ramp | Existing Loop Ramp | CMF ID: 480 |

VIRGINIA STATE PREFERRED CMF LIST

Table 1 Virginia State Preferred CMF List (cont)

|  | COUNTERMEASURE | $\begin{aligned} & \text { CRASH } \\ & \text { TYPE } \end{aligned}$ | AREA <br> TYPE | K | A | BC | 0 | SERVICE <br> LIFE | FUNCTIONAL CLASS | SITE DESCRIPTION | PRIOR CONDITION | REFERENCE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Widen Ramp Lane Width from X to Y in Feet | ALL | - | ** | ** | ** | 1 | 20 | Freeway Ramp | Freeway Ramp | Existing Ramp Lane Width of X Feet | $\begin{aligned} & \text { HSM Eqn } \\ & \text { 19-34 } \end{aligned}$ |
|  | Widen Ramp Left Shoulder | ALL | - | ** | ** | ** | ** | 20 | Freeway <br> Ramp | Freeway Ramp | Existing Left-Shoulder Width of $X$ Feet | HSM Eqn 19-36 |
|  | Widen Ramp Right Shoulder | ALL | - | ** | ** | ** | ** | 20 | Freeway Ramp | Freeway Ramp | Existing Right-Shoulder Width of X Feet | HSM Eqn 19-35 |
| 2은$\vdots$40$\frac{4}{11}$2 | Install Intersection Lighting | Night <br> Time | ALL | 0.881 | 0.881 | 0.881 | 0.881 | 15 | - | Intersection | No Lighting Present | CMF ID: 4462 |
|  | Increase Stopping Sight Distance on Crest Vertical Curve-Intersection Approach | ALL | Rural | 0.62 | 0.62 | 0.62 | 0.70 | 20 | - | Intersection Approach with Crest Vertical Curve | Crest Vertical Curve with Inadequate Sight Distance | $\begin{aligned} & \text { CMF ID: 6870, } \\ & 6871 \end{aligned}$ |
|  | Add Flashing Lights to Railroad (RR) Crossings with Signs | VT | - | 0.23 | 0.23 | 0.23 | 0.23 | 10 | - | RR Grade Crossing | RR Grade Crossing with Static Warning Signs | CMF ID: 487 |
|  | Add Gates to RR Crossings with Signs | VT | - | 0.06 | 0.06 | 0.06 | 0.06 | 10 | Minor <br> Arterial | RR Grade Crossing | RR Grade Crossing with Static Warning Signs | CMF ID: 489 |
|  | Adaptive Signal Control | ALL | U+S | 0.92 | 0.92 | 0.92 | 0.83 | 20 | - | Signalized Intersection | Non-Adaptive Traffic Signal | CMF ID: 6856 6857 |
|  | Add 3-Inch Yellow Retroreflective Sheeting to Signal Backplates | ALL | Urban | 0.85 | 0.85 | 0.85 | 0.85 | 6 | - | Signalized Intersection | No Backplates Present | CMF ID: 1410 |
|  | Advanced Activated/ Dynamic Flasher | ALL | - | 0.82 | 0.82 | 0.82 | 0.814 | 6 | - | Signalized Intersection | Signalized Intersection with No Advance Warning System | $\begin{aligned} & \text { CMF ID: 4198, } \\ & 4201 \end{aligned}$ |
|  | Advanced Cross Street Name Sign | ALL | - | 0.99 | 0.99 | 0.99 | 0.984 | 6 | - | Signalized Intersection | Signalized Intersection with No Advanced Street Sign | $\begin{aligned} & \text { CMF ID: 2449, } \\ & 2450 \end{aligned}$ |
|  | Advanced Dilemma Zone Detection | ALL | Rural | 0.918 | 0.887 | 0.887 | 0.918 | 20 | - | High Speed Signalized Intersection | No Dilemma Zone Warning System | $\begin{aligned} & \text { CMF ID: 4855, } \\ & 4857 \end{aligned}$ |
|  | Change from Permissive Left-Turn to Flashing Yellow Arrow | Left Turn | Urban | 0.635 | 0.635 | 0.635 | 0.635 | 20 | - | Signalized Intersection | Permissive Left-Turn Phasing | CMF ID: 4175 |
|  | Change from Permitted Left-Turn to Permitted/ Protected | Left Turn | Urban | 0.862 | 0.862 | 0.862 | 0.862 | 20 | - | Signalized Intersection | Permissive Left-Turn Phasing | CMF ID: 4270 |
|  | Change from Permitted Left-Turn to Protected on Major Approach | Angle | Urban | 0.01 | 0.01 | 0.01 | 0.01 | 20 | - | Signalized Intersection | Permissive Left-Turn Phasing on a Major Approach | CMF ID: 335 |
|  | Change from Permitted/ <br> Protected Left-Turn to Protected on Major Approach | Angle | Urban | 0.01 | 0.01 | 0.01 | 0.01 | 20 | - | Signalized Intersection | Protected/Permissive or Vice-Versa Left-Turn Phasing on a Major Approach | CMF ID: 339 |

VIRGINIA STATE PREFERRED CMF LIST

Table 1 Virginia State Preferred CMF List (cont)

|  | COUNTERMEASURE | CRASH <br> TYPE | AREA <br> TYPE | K | A | BC | 0 | SERVICE <br> LIFE | FUNCTIONAL CLASS | SITE DESCRIPTION | PRIOR CONDITION | REFERENCE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Change from Permitted/ Protected Left-Turn to Protected on Minor Approach | Angle | Urban | 0.04 | 0.04 | 0.04 | 0.04 | 20 | - | Signalized Intersection | Protected/Permissive or Vice-Versa Left-Turn Phasing on a Minor Approach | CMF ID: 337 |
|  | Change from Pretimed Signal to Actuated Signal | ALL | - | 0.8 | 0.8 | 0.8 | 0.8 | 20 | - | Signalized Intersection | Pretimed Signal Control | NCDOT CRF List 1.6 |
|  | Change from Protected Left-Turn to Flashing Yellow Arrow | Left <br> Turn | Urban | 2.242 | 2.242 | 2.242 | 2.242 | 20 | - | Signalized Intersection | Protected Left-Turn Phasing | CMF ID: 4173 |
|  | Change from Protected/ Permissive Left-Turn to Flashing Yellow Arrow | Left Turn | Urban | 0.806 | 0.806 | 0.806 | 0.806 | 20 | - | Signalized Intersection | Protected/Permissive LeftTurn Phasing | CMF ID: 4177 |
|  | Change Number of Approaches with Left-Turn Lanes from X Approaches to Y Approaches | ALL | ALL | ** | ** | ** | ** | 20 | - | Signalized Intersection | Left-Turn Lanes on X Number of Approaches | HSM |
|  | Change Number of Approaches with Prohibited Right Turn on Red from X Approaches to $Y$ Approaches | ALL | - | ** | ** | ** | ** | 20 | - | Signalized Intersection | Right Turn on Red Permitted on X Number of Approaches | CMF ID: 5194 |
|  | Change Number of Approaches with Right-Turn Lanes from X Approaches to Y Approaches | ALL | - | ** | ** | ** | ** | 20 | - | Signalized Intersection | Right-Turn Lanes on $X$ Number of Approaches | HSM Table $10-14,12-26$ |
|  | Change Number of Cycles per Hour from X Cycles per Hour to Y Cycles per Hour | Rear <br> End | U+S | ** | ** | ** | ** | 20 | Arterial | Signalized Intersection | X Cycles per Hour | CMF ID: 3072 |
|  | Channelize Right Turn | ALL | - | 0.65 | 0.65 | 0.65 | 1 | 20 | - | Signalized Intersection | No Right-Turn Channelization | FHWA CMF <br> Desktop <br> Reference <br> Guide |
|  | Closed Loop Signal System | ALL | - | 0.85 | 0.85 | 0.85 | 0.85 | 20 | - | Signalized Intersection | Signal System that is Not Closed Loop | NCDOT CRF List 1.7 |
|  | Convert from PedestalMounted Traffic Signal to Mast Arm-Mounted Traffic Signal | ALL | Urban | 0.56 | 0.56 | 0.56 | 0.49 | 20 | - | Signalized Intersection | Pedestal-Mounted Signal | $\begin{aligned} & \text { CMF ID: 1424, } \\ & 1425 \end{aligned}$ |

VIRGINIA STATE PREFERRED CMF LIST

Table 1 Virginia State Preferred CMF List (cont)


VIRGINIA STATE PREFERRED CMF LIST

Table 1 Virginia State Preferred CMF List (cont)

|  | COUNTERMEASURE | CRASH <br> TYPE | AREA <br> TYPE | K | A | BC | 0 | SERVICE <br> LIFE | FUNCTIONAL CLASS | SITE DESCRIPTION | PRIOR CONDITION | REFERENCE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Change Number of Uncontrolled Approaches with Right-Turn Lanes from X to Y at Intersection of Rural, Multilane Highway | ALL | Rural | ** | ** | ** | ** | 20 | - | Stop-Controlled Intersection <br> - Rural Multilane Highway | Right-Turn Lanes on X Number of Approaches | HSM Table $11-23$ |
|  | Change Number of Uncontrolled Approaches with Right-Turn Lanes from X to Y at Intersection of Rural, Two-Lane Roads | ALL | Rural | ** | ** | ** | ** | 20 | - | Stop-Controlled Intersection <br> - Rural Two-Lane Road | Right-Turn Lanes on X Number of Approaches | HSM Table $10-14$ |
|  | Change Number of Uncontrolled Approaches with Right-Turn Lanes from X to Y at Urban or Suburban Arterial Intersection | ALL | U+S | ** | ** | ** | ** | 20 | - | Stop-Controlled Intersection <br> - Urban and Suburban <br> Arterial | Right-Turn Lanes on X Number of Approaches | HSM Table $12-26$ |
|  | High-Friction Surface Treatment on Approach | ALL | - | 0.799 | 0.799 | 0.799 | 0.799 | 10 | - | Stop-Controlled Intersection Approach | Standard Pavement on Intersection Approach | CMF ID: 2259 |
|  | Increase Intersection Sight Distance from X Feet of Available Sight Distance to Y Feet | Angle <br>  <br> Left <br> Turn | - | ** | ** | ** | ** | 10 | - | Stop-Controlled Intersection Approach | Intersection Sight Distance of X Feet | NCHRP <br> 17-59, Report <br> 875 |
|  | Intersection Collision Warning System | ALL | - | 0.742 | 0.742 | 0.742 | 0.704 | 6 | - | Stop-Controlled Intersection | No Collision Warning System Present | $\begin{aligned} & \text { CMF ID: 8474, } \\ & 8475 \end{aligned}$ |
|  | Reduce Intersection Skew from X to Y-3-Leg Intersection | ALL | Rural | ** | ** | ** | ** | 20 | - | 3-Leg Stop-Controlled Intersection | Intersection Skew Angle of X Degrees | HSM <br> Equation: $10-22$ |
|  | Reduce Intersection Skew from X to Y-4-Leg Intersection | ALL | Rural | ** | ** | ** | ** | 20 | - | 4-Leg Stop-Controlled Intersection | Intersection Skew Angle of X Degrees | HSM <br> Equation: $10-23$ |
|  | Systemic Signage and Pavement Marking Improvements | ALL | - | 0.899 | 0.899 | 0.899 | 0.917 | 6 | - | Stop-Controlled Intersection | Stop-Controlled Intersection with No Supplemental Signage | FHWA Proven <br> Safety Countermeasures |
|  | Transverse Rumble Strips | ALL | Rural | 0.987 | 0.987 | 0.987 | 1.191 | 10 | Minor <br> Arterial | Stop-Controlled Intersection Approach | No Transverse Rumble Strips Present | $\begin{aligned} & \text { CMF ID: 2707, } \\ & 2708 \end{aligned}$ |
|  | Add Quadrant Roadway to Intersection | N/A | - | - | - | - | - | 20 | - | Conventional Intersection | Conventional Intersection | N/A |
|  | Convert 3-Leg Signalized Intersection to Continuous Green T-Intersection | ALL | - | 0.846 | 0.846 | 0.846 | 0.958 | 20 | - | 3-Leg Signalized Intersection | Standard 3-Leg Signalized Intersection | $\begin{aligned} & \text { CMF ID: 8655, } \\ & 8656 \end{aligned}$ |

VIRGINIA STATE PREFERRED CMF LIST

Table 1 Virginia State Preferred CMF List (cont)

|  | COUNTERMEASURE | CRASH <br> TYPE | AREA <br> TYPE | K | A | BC | 0 | SERVICE <br> LIFE | FUNCTIONAL CLASS | SITE DESCRIPTION | PRIOR CONDITION | REFERENCE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Convert At-Grade Intersection to Interchange | ALL | - | 0.58 | 0.43 | 0.43 | 0.64 | 20 | - | 4-Leg Intersection | At-Grade Intersection | $\begin{aligned} & \text { CMF ID: 459, } \\ & 460,461 \end{aligned}$ |
|  | Convert 4-Leg Intersection to Two Offset T-Intersections | ALL | Urban | 0.75 | 0.75 | 0.75 | 1 | 20 | - | 4-Leg Stop-Controlled Intersection | 4-Leg Stop-Controlled Intersection | HSM CMF: <br> Table 14-2 |
|  | Convert Minor Stop-Control to All-Way Stop Control | ALL | ALL | 0.23 | 0.23 | 0.23 | 0.319 | 20 | - | Minor Stop-Controlled Intersection | Stop-Control on Minor Approaches | $\begin{aligned} & \text { CMF ID: 3127, } \\ & 3128 \end{aligned}$ |
|  | Convert Signalized Intersection to Roundabout | ALL | - | 0.52 | 0.22 | 0.22 | 0.52 | 20 | - | Signalized Intersection | Signalized Intersection | $\begin{aligned} & \text { CMF ID: 225, } \\ & 226 \end{aligned}$ |
|  | Convert Stop-Controlled Intersection to Roundabout | ALL | ALL | 0.56 | 0.18 | 0.18 | 0.56 | 20 | - | Stop-Controlled Intersection | Minor Stop-Controlled Intersection | $\begin{aligned} & \text { CMF ID: } 227 \text {, } \\ & 228 \end{aligned}$ |
|  | Convert Stop-Controlled Intersection to Signalized Intersection | ALL | ALL | 0.642 | 0.642 | 0.642 | 0.639 | 20 | - | Stop-Controlled Intersection | Minor Stop-Controlled Intersection | $\begin{aligned} & \text { CMF ID: 7983, } \\ & 7986 \end{aligned}$ |
| $z$은$\vdots$00$\frac{1}{u}$$\frac{5}{2}$ | Convert to Displaced LeftTurn Intersection | ALL | - | 0.81 | 0.81 | 0.81 | 0.76 | 20 | - | High-Speed Intersection | Traditional Intersection | FHWA TechBrief |
|  | Convert to J-Turn Intersection | ALL | Rural | 0.652 | 0.463 | 0.463 | 0.652 | 20 | Principal <br> ArterialOther | High-Speed Intersection | At-Grade Minor StopControlled Intersection | CMF ID: 5555, 5556 |
|  | Convert to Median U-Turn Intersection | ALL | - | 0.70 | 0.70 | 0.70 | 0.91 | 20 | Arterial | High-Speed Intersection | Conventional Signalized Intersection | FHWA TechBrief |
|  | Convert to Signalized Intersection to Signalized RCUT | ALL | - | 0.78 | 0.78 | 0.78 | 0.85 | 20 | - | High-Speed Signalized Intersection | Conventional Signalized Intersection | FHWA Report |
|  | Convert to Signalized Intersection to Unsignalized RCUT | N/A | - | - | - | - | - | 20 | - | High-Speed Signalized Intersection | Signalized Intersection | N/A |
|  | Convert to Unsignalized Intersection to Unsignalized RCUT | ALL | Rural | 0.37 | 0.37 | 0.37 | 0.54 | 20 | Principal <br> ArterialOther | High-Speed Stop-Controlled Intersection | Conventional Unsignalized Intersection | $\begin{aligned} & \text { CMF ID: 4883, } \\ & 4884 \end{aligned}$ |
|  | Convert Two Offset T-Intersection, Offset by X Miles, to T-Intersections with Major Road AADT | ALL | Rural | ** | ** | ** | ** | 20 | - | Offset T-Intersections | T-Intersections Offset by X Miles | HSM Eqn $10-17$ |
|  | Convert Unsignalized Intersection to Unsignalized Superstreet Intersection | ALL | Rural | 0.37 | 0.37 | 0.37 | 0.54 | 20 | Principal <br> Arterial- <br> Other | High-Speed Stop-Controlled Intersection | Stop-Control on Minor Approaches | $\begin{aligned} & \text { CMF ID: 4883, } \\ & 4884 \end{aligned}$ |

Table 1 Virginia State Preferred CMF List (cont)

|  | COUNTERMEASURE | CRASH <br> TYPE | AREA <br> TYPE | K | A | BC | 0 | SERVICE <br> LIFE | FUNCTIONAL CLASS | SITE DESCRIPTION | PRIOR CONDITION | REFERENCE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Install Interim Roundabout | ALL | ALL | 0.23 | 0.23 | 0.23 | 0.319 | 5 | - | Stop-Controlled Intersection | Stop-Control on Minor Approaches | $\begin{aligned} & \text { CMF ID: } 3127 \text {, } \\ & 3128 \end{aligned}$ |
|  | Remove Unwarranted Signal | ALL | U | 0.76 | 0.76 | 0.76 | 0.76 | 20 | Minor <br> Arterial, Collectors | Signalized Intersection of One-Way Streets | Unwarranted Traffic Signal | CMF ID: 332 |
|  | Install Temporary Traffic Circle | N/A | - | - | - | - | - | 2 | - | Unsignalized Intersection | No Control, Yield Control, or Stop Controlled | N/A |
|  | Active Traffic Management with Hard Shoulder Running | ALL | - | 0.69 | 0.69 | 0.69 | 0.75 | 20 | Principal <br> Arterial - <br> Interstate | Freeway Segment | No Active Traffic Management or Hard Shoulder Running | UVA Study |
|  | Active Traffic Management without Hard Shoulder Running | ALL | - | 1.18 | 1.18 | 1.18 | 1.16 | 20 | Principal Arterial Interstate | Freeway Segment | No Active Traffic Management | UVA Study |
|  | Add Cable Median Barrier | $\begin{aligned} & \text { CM,F, } \\ & \text { O, HO } \end{aligned}$ | Rural | 0.09 | 0.09 | 0.09 | 0.09 | 15 | Principal Arterial Interstate | Freeway Segment with Traversable Median | No Median Barrier Present | CMF ID:1966 |
|  | Add Rumble Strips to Inside Shoulder | SV | - | 0.811 | 0.811 | 0.811 | 1 | 10 | Principal Arterial Intersectate | Freeway Segment | No Rumble Strips Present on Inside Shoulder | HSM Eqn 18-36 |
|  | Add Median Concrete Barrier | $\begin{aligned} & \text { CM,F, } \\ & \text { O,HO } \end{aligned}$ | Rural | 0 | 0 | 0 | 0 | 15 | Principal <br> Arterial-Other <br> Freeways and Expressways | Freeway Segment | No Median Barrier Present | CMF ID: 2256 |
|  | Add Median Guardrail | CM | - | 0.22 | 0.22 | 0.22 | 0.22 | 15 | Principal <br> Arterial - Other <br> Freeways and <br> Expressways | Freeway Segment | No Median Barrier Present | CMF ID: 51 |
|  | Add Rumble Strips to Outside Shoulder | SV | - | 0.811 | 0.811 | 0.811 | 1 | 10 | Principal Arterial Intersectate | Freeway Segment | No Rumble Strips Present on Outside Shoulder | HSM Eqn $18-36$ |
|  | Add Raised Pavement Markers | ALL | Rural | 0.87 | 0.87 | 0.87 | 0.87 | 2 | Principal <br> Arterial - Other <br> Freeways and <br> Expressways | Freeway Segment | No Raised Pavement Markers Present | CMF ID: 5498 |
|  | Add Roadside Guardrail | ALL | - | 0.84 | 0.84 | 0.99 | 1.06 | 15 | Principal <br> Arterial - Other <br> Freeways and <br> Expressways | Freeway Segment | No Roadside Barrier Present | $\begin{aligned} & \text { CMF ID: } 8391 \text {, } \\ & 8392,8393 \end{aligned}$ |

Table 1 Virginia State Preferred CMF List (cont)

|  | COUNTERMEASURE | $\begin{aligned} & \text { CRASH } \\ & \text { TYPE } \end{aligned}$ | AREA <br> TYPE | K | A | BC | 0 | SERVICE <br> LIFE | FUNCTIONAL CLASS | SITE DESCRIPTION | PRIOR CONDITION | REFERENCE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Implement Incident Management to Reduce Incident Duration Time | SC | - | 0.85 | 0.85 | 0.85 | 0.85 | 6 | Principal <br> Arterial - <br> Interstate | Freeway Segment | No Incident Management Program | VA Planning Level CMFs |
|  | Implement Variable Speed Limits | ALL | Urban | 0.71 | 0.71 | 0.71 | 0.75 | 6 | Principal Arterial Interstate | Freeway Segment | Static Posted Speed Limit | $\begin{aligned} & \text { CMF ID: 8730, } \\ & 8731 \end{aligned}$ |
|  | Rural: Widen from 4 Lanes to 6 Lanes | ALL | Rural | 0.7 | 0.7 | 0.7 | 0.7 | 20 | - | Rural Freeway Segment | 4-Lane Cross-Section | VDOT SPFs, Crash Rate Ratios |
|  | Upgrade Horizontal Curve Signage | ALL | Rural | 0.75 | 0.75 | 0.75 | 0.82 | 6 | - | Freeway Horizontal Curve Segment | No Horizontal Curve Signs or Dirty Signs with No Retroreflectivity | $\begin{aligned} & \text { CMF ID: 2431, } \\ & 2433 \end{aligned}$ |
|  | Upgrade Pavement Markings to Wet-Reflective Pavement Markings | ALL | - | 0.881 | 0.881 | 0.881 | 1.032 | 2 | Principal <br> Arterial - Other <br> Freeways and <br> Expressways | Freeway Segment | Standard Pavement Markings | $\begin{aligned} & \text { CMF ID: 8093, } \\ & 8134 \end{aligned}$ |
|  | Upgrade Roadside Guardrail | ALL | - | 0.95 | 0.95 | 0.95 | 0.95 | 10 | - | Freeway Segment with Roadside Guardrail | Damaged or Below Standard Guardrail | Desktop <br> Reference <br> Guide |
|  | Urban: Widen from 4 Lanes to 6 Lanes | ALL | Urban | 0.9 | 0.9 | 0.9 | 0.9 | 20 | - | Urban Freeway Segment | 4-Lane Cross-Section | VDOT SPFs, Crash Rate Ratios |
|  | Urban: Widen from 4 Lanes to 8+ Lanes | ALL | Urban | 0.75 | 0.75 | 0.75 | 0.75 | 20 | - | Urban Freeway Segment | 4-Lane Cross-Section | VDOT SPFs, Crash Rate Ratios |
|  | Urban: Widen from 6 Lanes to 8+ Lanes | ALL | Urban | 0.8 | 0.8 | 0.8 | 0.8 | 20 | - | Urban Freeway Segment | 6-Lane Cross-Section | VDOT SPFs, Crash Rate Ratios |
|  | Widen Clear Zone from X Feet to Y Feet | SV | - | ** | ** | ** | 1 | 20 | - | Freeway Segment | Clear Zone Width of X Feet | $\begin{aligned} & \text { HSM Eqn } \\ & 18-38 \end{aligned}$ |
|  | Widen Median from X Feet to Y Feet | ALL | - | ** | ** | ** | ** | 20 | - | Freeway Segment | Median Width of X Feet | HSM Eqn 18-27 |
|  | Widen Paved Inside Shoulder from X Feet to Y Feet | ALL | - | ** | ** | ** | ** | 20 | - | Freeway Segment | Inside Shoulder Width of X Feet | HSM Eqn $18-26$ |
|  | Widen Paved Outside Shoulder on Horizontal Curve from X Feet to Y Feet | SV | - | ** | ** | ** | ** | 20 | - | Freeway Horizontal Curve Segment | Outside Shoulder Width of X Feet | HSM Eqn 18-35 and Table 18-21 |

VIRGINIA STATE PREFERRED CMF LIST

Table 1 Virginia State Preferred CMF List (cont)

|  | COUNTERMEASURE | $\begin{aligned} & \text { CRASH } \\ & \text { TYPE } \end{aligned}$ | AREA <br> TYPE | K | A | BC | 0 | SERVICE <br> LIFE | FUNCTIONAL CLASS | SITE DESCRIPTION | PRIOR CONDITION | REFERENCE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Widen Paved Outside Shoulder on Horizontal Tangent from X Feet to Y Feet | SV | - | ** | ** | ** | 1 | 20 | - | Freeway Horizontal Tangent Segment | Outside Shoulder Width of X Feet | HSM Eqn 18-35 and Table 18-21 |
|  | Add Automated Speed Enforcement Cameras | ALL | - | 0.83 | 0.83 | 0.83 | 0.84 | 6 | - | Non-Freeway Segment | No Automated Speed Enforcement Present | $\begin{aligned} & \text { CMF ID: } 2688 \text {, } \\ & 4583 \end{aligned}$ |
|  | Add Auxiliary Passing Lane | ALL | Rural | 0.67 | 0.67 | 0.67 | 0.58 | 20 | - | Rural Two-Lane Undivided Highway | No Passing Lanes Present | $\begin{aligned} & \text { CMF ID: 9111, } \\ & 9112 \end{aligned}$ |
|  | Add Centerline Rumble Strips (Including Sinusoidal/ Mumble) | HO, O | Rural | 0.55 | 0.55 | 0.55 | 0.63 | 10 | - | Non-Freeway Segment | No Centerline Rumble Strips Present | $\begin{aligned} & \text { CMF ID: } 3355 \text {, } \\ & 3360 \end{aligned}$ |
|  | Add Chevron Signs at Horizontal Curves | Night <br> Time | Rural | 0.75 | 0.75 | 0.75 | 0.75 | 6 | - | Small Radius Horizontal Curve on Rural Two-Lane Undivided Highway | No Chevrons Present | CMF ID: 2439 |
|  | Add Chevron Signs, Curve Warning Signs, and Sequential Flashing Beacons | Night <br> Time | - | 0.592 | 0.592 | 0.592 | 0.592 | 6 | - | Horizontal Curve on Multilane Highway | No Curve Delineation Treatment Present | CMF ID: 1852 |
|  | Add Raised Pavement Markers | ALL | Rural | 0.81 | 0.81 | 0.81 | 0.81 | 2 | Principal <br> Arterial - Other <br> Freeways and <br> Expressways | Non-Freeway Segment | No Raised Pavement Markers Present | CMF ID: 5496 |
|  | Add Safety Edge | Run Off <br> Road | Rural | 0.79 | 0.79 | 0.79 | 0.79 | 15 | Principal Arterial Other | Two-Lane Undivided Rural Highway | No Safety Edge Present | FHWA Proven Safety |
|  | Add Segment Lighting | Night <br> Time | Urban | 0.68 | 0.68 | 0.68 | 0.76 | 15 | Minor Arterial | Non-Freeway Segment | No Lighting Present | $\begin{aligned} & \text { CMF ID: 7781, } \\ & 7782 \end{aligned}$ |
|  | Add Shoulder Rumble Strips (Including Sinusoidal/ Mumble) | Run Off Roadright | Rural | 0.83 | 0.83 | 0.83 | 0.84 | 10 | - | Non-Freeway Segment | No Shoulder Rumble Strips Present | $\begin{aligned} & \text { CMF ID: 3442, } \\ & 3447 \end{aligned}$ |
|  | Add Two-Way Left-Turn Lane (2U to 3T) | ALL | - | 0.739 | 0.739 | 0.739 | 0.797 | 20 | - | Two-Lane Undivided Highway | No TWLTL Present | $\begin{aligned} & \text { CMF ID: 2341, } \\ & 2346 \end{aligned}$ |
|  | Add Two-Way Left-Turn Lane (4U to 5T) | ALL | Urban | 0.45 | 0.45 | 0.45 | 0.45 | 20 | - | Four-Lane Undivided Highway | No TWLTL Present | CMF ID: 4084 |
|  | Breakaway Supports for Utility Poles in Clear Zones | ALL | Rural | 0.94 | 0.94 | 0.94 | 1.00 | 10 | - | Non-Freeway Segment | Non-Breakaway Supports | $\begin{aligned} & \text { HSM Eqn } \\ & 10-20 \end{aligned}$ |
|  | Change 4" Wide Edgelines to 6" Wide Edgelines | ALL | Rural | 0.635 | 0.635 | 0.635 | 0.877 | 2 | - | Rural Two-Lane Highway | 4" Edgelines | $\begin{aligned} & \text { CMF ID: 4737, } \\ & 4738 \end{aligned}$ |

VIRGINIA STATE PREFERRED CMF LIST

Table 1 Virginia State Preferred CMF List (cont)

|  | COUNTERMEASURE | CRASH <br> TYPE | AREA <br> TYPE | K | A | BC | 0 | SERVICE <br> LIFE | FUNCTIONAL CLASS | SITE DESCRIPTION | PRIOR CONDITION | REFERENCE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Change Driveway Density (Driveways/Mile) from $X$ to $Y$ | ALL | Rural | ** | ** | ** | ** | 20 | Principal Arterial Other | Rural Non-Freeway Segment | Driveway Density of $X$ Driveways per Mile | $\begin{aligned} & \text { CMF ID: 1973, } \\ & 2248 \end{aligned}$ |
|  | Change Roadside Hazard Rating from $X$ to $Y$ by <br> Flattening Roadside Slope | ALL | Rural | ** | ** | ** | ** | 20 | - | Two-Lane Undivided Highway | Roadside Hazard Rating of X ■ | $\begin{aligned} & \text { HSM Eqn } \\ & 10-20 \end{aligned}$ |
|  | Change Superelevation Variance from $X$ to $Y$ (if Variance Between 0.01 and 0.02) | ALL | Rural | ** | ** | ** | ** | 20 | - | Horizontal Curve on Two-Lane Undivided Highway | Superelevation Deficiency of X Feet per Foot in Decimal | $\begin{aligned} & \text { HSM Eqn } \\ & 10-15 \end{aligned}$ |
|  | Change Superelevation Variance from $X$ to $Y$ (if Variance Greater than 0.02) | ALL | Rural | ** | ** | ** | ** | 20 | - | Horizontal Curve on Two-Lane Undivided Highway | Superelevation Deficiency of X Feet per Foot in Decimal | $\begin{aligned} & \text { HSM Eqn } \\ & 10-16 \end{aligned}$ |
|  | Dynamic Speed Feedback Signs | ALL | Rural | 0.95 | 0.95 | 0.95 | 0.95 | 6 | - | Two-Lane Undivided Highway | No Dynamic Speed Feedback Sign Present | CMF ID: 6885 |
|  | Flatten Horizontal Curve | ALL | Rural | - | - | - | - | 20 | - | Horizontal Curve on Two-Lane Undivided Highway | Please use the Existing Horizontal Curve Geometry Tab to Calculate the CMFs | $\begin{aligned} & \text { CMF ID: 9271, } \\ & 9272 \end{aligned}$ |
|  | Implement High-Friction Surface Treatment on Horizontal Curve | ALL | - | 0.759 | 0.759 | 0.759 | 0.759 | 10 | - | Horizontal Curve on Non-Freeway Segment | Horizontal Curve with Standard Pavement | CMF ID: 7900 |
|  | Increase Stopping Sight Distance on Crest Vertical Curve | ALL | Rural | 0.76 | 0.76 | 0.76 | 0.82 | 20 | - | Crest Vertical Curve on Two-Lane Highway | Crest Vertical Curve with Inadequate Sight Distance | $\begin{aligned} & \text { CMF ID: } 6868 \text {, } \\ & 6869 \end{aligned}$ |
|  | Pave Unpaved Shoulder | ALL | Rural | 0.97 | 0.97 | 0.97 | 0.97 | 20 | - | Two-Lane Undivided Rural Highway | Unpaved Shoulder | HSM Eqn <br> 10-12, Table <br> 10-9 and <br> 10-10 |
|  | Pavement Resurfacing Rural | ALL | Rural | 1.03 | 1.03 | 1.03 | 1.03 | 10 | - | Two-Lane Undivided Highway | Old Pavement | CMF ID: 5626 |
|  | Pavement Resurfacing Urban | ALL | Urban | 0.894 | 0.894 | 0.894 | 0.929 | 10 | Principal Arterial Other | Non-Freeway Segment | Old Pavement | $\begin{aligned} & \text { CMF ID: 9289, } \\ & 9290 \end{aligned}$ |
|  | Prohibit On-Street Parking | ALL | Urban | 0.78 | 0.78 | 0.78 | 0.72 | 20 | Principal Arterial Other | Urban Arterial with Street Parking | On-Street Parking Allowed | $\begin{aligned} & \text { CMF ID: 4574, } \\ & 4575 \end{aligned}$ |
|  | Remove or Relocate Fixed Object Outside of Clear Zone | CFO | - | 0.62 | 0.62 | 0.62 | 0.62 | 20 | - | Non-Freeway Segment | Fixed Object within Clear Zone | $\begin{aligned} & \text { CMF ID: 1024, } \\ & 1044 \end{aligned}$ |
|  | Road Diet (4U to 3T) | ALL | Urban | 0.71 | 0.71 | 0.71 | 0.71 | 20 | Minor Arterial | 4-Lane Undivided Highway | 4-Lane Cross-Section | CMF ID: 199 |

■ Please go to https://www.fhwa.dot.gov/publications/research/safety/99207/appd.cfm for a description of RHR ratings.

VIRGINIA STATE PREFERRED CMF LIST

Table 1 Virginia State Preferred CMF List (cont)

|  | COUNTERMEASURE | CRASH <br> TYPE | AREA TYPE | K | A | BC | 0 | SERVICE <br> LIFE | FUNCTIONAL CLASS | SITE DESCRIPTION | PRIOR CONDITION | REFERENCE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SEGMENTS (NON-FREEWAY) | Upgrade Chevrons with Flourescent Sheeting | Night time | Rural | 0.65 | 0.65 | 0.65 | 0.65 | 6 | - | Horizontal Curve on Rural Two-Lane Undivided Highway | No Signs Present, Signs with No Fluorescent Sheeting, or Dirty Signs Present | CMF ID: 2434 |
|  | Upgrade Pavement Markings by Increasing Retroreflectivity | Night time | - | 0.81 | 0.81 | 0.81 | 0.81 | 2 | - | Non-Freeway Segment | Edgeline, Centerline, and Skip Line Pavement Markings with Low Retroreflectivity | $\begin{aligned} & \text { CMF ID: 2116, } \\ & 2117,2120 \end{aligned}$ |
|  | Upgrade Pavement Markings to Wet-Reflective Pavement Markings | ALL | - | 0.881 | 0.881 | 0.881 | 1.032 | 2 | Principal <br> Arterial-Other <br> Freeways and <br> Expressways | Non-Freeway Segment | Traditional Pavement Markings | $\begin{aligned} & \text { CMF ID: 8093, } \\ & 8134 \end{aligned}$ |
|  | Widen Clear Zone | ALL | Rural | 0.78 | 0.78 | 0.78 | 0.78 | 20 | - | Rural Two-Lane Highway | Rural Two-Lane Highway with Narrow Clear Zone | CMF ID: 35 |
|  | Widen Lane | ALL | Rural | 0.87 | 0.87 | 0.87 | 0.87 | 20 | - | Two-Lane Undivided Highway | Narrow Lane Width | HSM Table <br> 10-8, Eqn <br> 10-11 |
|  | Widen Average Shoulder Width | HO, CFO, $0, \mathrm{~S}$ | Rural | - | - | - | A | 20 | - | Two-Lane Undivided Highway | Existing Shoulder Width | HSM 10-9 |

Table 2 CMFunction Equations

|  | COUNTERMEASURE | K | A | BC | 0 | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lengthen Acceleration Lane from X Miles to Y Miles | $\mathrm{e}^{-4.55^{*}[\mathrm{Y}-\mathrm{X}]}$ | $e^{-4.55^{*}[\gamma-X]}$ | $e^{-4.55^{*}[\gamma-X]}$ | $\mathrm{e}^{-2.59^{*}[\mathrm{Y}-\mathrm{X}]}$ | Miles |
|  | Widen Ramp Lane Width from X to Y in Feet | $e^{0.0458^{*}[\mathrm{X}-\mathrm{Y}]}$ | $e^{0.0458^{*}[X-Y]}$ | $e^{0.0458^{*}[\mathrm{X}-\mathrm{Y}]}$ | 1 | Feet |
|  | Widen Ramp Left Shoulder X Feet to Y Feet | $e^{0.0539^{*}[\mathrm{X}-\mathrm{Y}]}$ | $e^{0.0539^{*}[X-Y]}$ | $e^{0.0539^{*}[X-Y]}$ | $e^{0.0259^{*}[X-Y]}$ | Feet |
|  | Widen Ramp Right Shoulder X Feet to Y Feet | $e^{0.0539 *[X-Y]}$ | $e^{0.0539^{*}[\mathrm{X}-\mathrm{Y}]}$ | $e^{0.0539^{*}[X-Y]}$ | $e^{0.0259 *[X-Y]}$ | Feet |
| $z$은u0wwㄴz | Change Number of Approaches with Left-Turn Lanes from X Approaches to Y Approaches | $0.90{ }^{\text {Y-X }}$ | $0.90^{\mathrm{Y}-\mathrm{X}}$ | $0.90{ }^{\mathrm{Y}-\mathrm{X}}$ | $0.90^{\text {r-x }}$ | Approaches |
|  | Change Number of Approaches with Prohibited Right Turn on Red from X Approaches to Y Approaches | $0.98{ }^{\text {r-X }}$ | $0.98{ }^{\text {r-X }}$ | $0.98{ }^{\mathrm{Y}-\mathrm{X}}$ | $0.98{ }^{\text {r-x }}$ | Approaches |
|  | Change Number of Approaches with Right-Turn Lanes from X Approaches to Y Approaches | $0.96{ }^{\text {r-x }}$ | $0.96{ }^{\mathrm{r}-\mathrm{X}}$ | $0.96{ }^{\text {r-x }}$ | $0.96{ }^{\text {r-X }}$ | Approaches |
|  | Change Number of Cycles per Hour from X Cycles per Hour to Y Cycles per Hour | $e^{-0.0444^{*}[\gamma-X]}$ | $\mathrm{e}^{-0.0444^{*}[\gamma-X]}$ | $\mathrm{e}^{-0.0444^{*}[\mathrm{Y}-\mathrm{X}]}$ | $\mathrm{e}^{-0.0444^{*}[Y-X]}$ | Cycles per Hour |
|  | Change Number of Uncontrolled Approaches with Left-Turn Lanes from X Approaches to Y Approaches at 4-Leg Intersection | $0.72{ }^{\text {r-X }}$ | $0.72{ }^{\text {r-X }}$ | $0.72{ }^{\text {Y-X }}$ | $0.72{ }^{\text {r-X }}$ | Approaches |
|  | Change Number of Uncontrolled Approaches with Right-Turn Lanes from $X$ to $Y$ at Intersection of Rural, Multilane Highway | $0.77^{\mathrm{r}-\mathrm{x}}$ | $0.77^{\mathrm{Y}-\mathrm{X}}$ | $0.77^{\text {r-x }}$ | $0.77^{\mathrm{r}-\mathrm{x}}$ | Approaches |
|  | Change Number of Uncontrolled Approaches with Right-Turn Lanes from $X$ to $Y$ at Intersection of Rural, Two-Lane Roads | $0.86{ }^{\text {Y-X }}$ | $0.86{ }^{\mathrm{Y}-\mathrm{X}}$ | $0.86{ }^{\text {r-X }}$ | $0.86{ }^{\text {r-X }}$ | Approaches |
|  | Change Number of Uncontrolled Approaches with Right-Turn Lanes from $X$ to $Y$ at Urban or Suburban Arterial Intersection | $0.86{ }^{\text {r-X }}$ | $0.86{ }^{\mathrm{Y}-\mathrm{X}}$ | $0.86{ }^{\mathrm{Y}-\mathrm{X}}$ | $0.86{ }^{\text {r-X }}$ | Approaches |
|  | Increase Intersection Sight Distance from X Feet of Available Sight Distance to $Y$ Feet | $e^{195.791 \star[1 / \mathrm{V}-1 / \mathrm{X}]}$ | $\mathrm{e}^{195.791^{*}[1 / \mathrm{Y}-1 / \mathrm{X}]}$ | $\mathrm{e}^{195.791^{\star}[1 / \mathrm{l}-1 / \mathrm{X}]}$ | $\mathrm{e}^{203.368^{*}[1 / \mathrm{V}-1 / \mathrm{X}]}$ | Feet |

Table 2 CMFunction Equations (cont)

|  | COUNTERMEASURE | K | A | BC | 0 | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Reduce Intersection Skew from $X$ to Y-3 Leg Intersection | $e^{0.004^{*}[\mathrm{Y}-\mathrm{X}]}$ | $e^{0.004 *[Y-X]}$ | $e^{0.004 *[Y-X]}$ | $e^{0.004^{*}[\mathrm{Y}-\mathrm{X}]}$ | Degrees of Skew |
|  | Reduce Intersection Skew from $X$ to Y-4 Leg Intersection | $e^{0.0054 *[Y-X]}$ | $e^{0.0054 \star[Y-X]}$ | $e^{0.0054 *[Y-X]}$ | $e^{0.0054 \star[Y-X]}$ | Degrees of Skew |
|  | Convert Two Offset T-Intersection, Offset by X Miles, to 4-Leg Signalized Intersection with Major Road AADT | $\frac{\frac{0.05-0.005 * \ln (\mathrm{AADT})}{x}+0.322}{\frac{2 *(0.05-0.005 * \ln (\mathrm{AADT}))}{x}+0.322}$ | $\frac{\frac{0.05-0.005 * \ln (\text { AADT })}{x}+0.322}{\frac{2 \star(0.05-0.005 * \ln (\text { AADT }))}{x}+0.322}$ | $\frac{\frac{0.05-0.005 * \ln (\text { AADT })}{x}+0.322}{\frac{2 *(0.05-0.005 * \ln (\text { AADT }))}{x}+0.322}$ | $\frac{\frac{0.05-0.005 * \ln (A A D T)}{x}+0.322}{\frac{2 \star(0.05-0.005 * \ln (\text { AADT }))}{x}+0.322}$ | X-MIles AADT-Vehicles per Day |
|  | Widen Clear Zone from $X$ Feet to $Y$ Feet | $e^{0.00451 *[X-Y]}$ | $e^{0.00451 *[X-Y]}$ | $e^{0.00451 *[X-Y]}$ | 1 | Feet |
|  | Widen Median from X Feet to Y Feet | $e^{0.131^{*}[1 / \mathrm{Y}-1 / \mathrm{X}]}$ | $e^{0.131^{\star}[1 / \mathrm{Y}-1 / \mathrm{X}]}$ | $e^{0.131^{\star}[1 / \mathrm{Y}-1 / \mathrm{X}]}$ | $e^{0.169 *[1 / \mathrm{Y}-1 / \mathrm{X}]}$ | Feet |
|  | Widen Paved Inside Shoulder from X Feet to Y Feet | $e^{0.0172^{*}[\mathrm{X}-\mathrm{Y}]}$ | $e^{0.0172^{\star}[\mathrm{X}-\mathrm{Y}]}$ | $e^{0.0172^{*}[X-Y]}$ | $e^{0.0153 *[X-Y]}$ | Feet |
|  | Widen Paved Outside Shoulder on Horizontal Curve from X Feet to Y Feet | $e^{0.0897 *[X-Y]}$ | $e^{0.0897 *[X-Y]}$ | $e^{0.0897 *[X-Y]}$ | $e^{0.0840 *[X-Y]}$ | Feet |
|  | Widen Paved Outside Shoulder on Horizontal Tangent from X Feet to Y Feet | $e^{0.0647 *[X-Y]}$ | $e^{0.0647 *[X-Y]}$ | $e^{0.0647 *[X-Y]}$ | 1 | Feet |
|  | Change Driveway Density (Driveways/Mile) from $X$ to $Y$ | $e^{0.0152^{\star}[\mathrm{Y}-\mathrm{X}]}$ | $e^{0.0152^{\star}[\mathrm{Y}-\mathrm{X}]}$ | $e^{0.0152^{\star}[Y-X]}$ | $e^{0.0232^{\star}[\mathrm{Y}-\mathrm{X}]}$ | Driveways per Mile |
|  | Change Roadside Hazard Rating from X to Y by Flattening Roadside Slope | $e^{0.0668 *[Y-X]}$ | $e^{0.0668 *[Y-X]}$ | $e^{0.0668 *[Y-X]}$ | $e^{0.0668 *[Y-X]}$ | Roadside Hazard Rating ■ |
|  | Change Superelevation Variance from X to Y (if Variance Between 0.01 and 0.02) | $\frac{1+6 *[\mathrm{Y}-0.01]}{1+6 *[\mathrm{x}-0.01]}$ | $\frac{1+6 *[\mathrm{Y}-0.01]}{1+6 *[\mathrm{x}-0.01]}$ | $1+6 *[\mathrm{Y}-0.01]$ $1+6 *[\mathrm{x}-0.01]$ | $\frac{1+6 *[Y-0.01]}{1+6 *[x-0.01]}$ | Feet per Foot |
|  | Change Superelevation Variance from $X$ to $Y$ (if Variance Greater than 0.02) | $\frac{1.06+3 \star[\mathrm{Y}-0.02]}{1.06+3 *[\mathrm{x}-0.02]}$ | $\frac{1.06+3 *[Y-0.02]}{1.06+3 *[x-0.02]}$ | $\begin{gathered} 1.06+3 *[\mathrm{Y}-0.02] \\ \hline 1.06+3 *[\mathrm{x}-0.02] \end{gathered}$ | $\frac{1.06+3 *[\mathrm{Y}-0.02]}{1.06+3 *[\mathrm{x}-0.02]}$ | Feet per Foot |

■ Please go to https://www.fhwa.dot.gov/publications/research/safety/99207/appd.cfm for a description of RHR ratings.

VIRGINIA STATE PREFERRED CMF LIST

Table 3 References


VIRGINIA STATE PREFERRED CMF LIST

Table 3 References (cont)

|  | COUNTERMEASURE | Reference | REFERENCE/CITATION HYPERLINK \#1 | REFERENCE/CITATION HYPERLINK \#2 |
| :---: | :---: | :---: | :---: | :---: |
|  | Install Raised Pedestrian Crossing | PED CMF Toolbox | https://safety.fhwa.dot.gov/ped_bike/tools_solve/ fhwasa18041/fhwasa18041.pdf | - |
|  | Prohibit Left Turns | Ped CMF Toolbox | https://safety.fhwa.dot.gov/ped_bike/tools_solve/ fhwasa18041/fhwasa18041.pdf | - |
|  | Remove Parking Near Intersection | PED CMF Toolbox | https://safety.fhwa.dot.gov/ped_bike/tools_solve/ fhwasa18041/fhwasa18041.pdf | - |
|  | Upgrade Crosswalk to High-Visibility | CMF ID: 4658 | http://www.cmfclearinghouse.org/detail. cfm?facid=4658 | - |
|  | Widen Sidewalk at Intersection | CMF ID: 413 | http://www.cmfclearinghouse.org/detail. cfm?facid=413 | - |
|  | Add Auxiliary Lane Between Entrance and Exit Ramps | CMF ID: 7440, 7441 | http://www.cmfclearinghouse.org/detail. <br> cfm?facid=7440 | http://www.cmfclearinghouse.org/detail. cfm?facid=7441 |
|  | Add Collector-Distributor Road | ISATe, HSM Chapters 18 and 19 | http://onlinepubs.trb.org/onlinepubs/nchrp/docs/ nchrp17-45_fr.pdf | - |
|  | Add Entrance Ramp to One Side of Freeway | ISATe, HSM Chapters 18 and 19 | http://onlinepubs.trb.org/onlinepubs/nchrp/docs/ nchrp17-45_fr.pdf | - |
|  | Add Exit Ramp to One Side of Freeway | ISATe, HSM Chapters 18 and 19 | http://onlinepubs.trb.org/onlinepubs/nchrp/docs/ nchrp17-45_fr.pdf | - |
|  | Convert Diamond Interchange to Diverging Diamond Interchange | CMF ID: 8258, 8278 | http://www.cmfclearinghouse.org/detail. cfm?facid=8258 | http://www.cmfclearinghouse.org/detail. cfm?facid=8278 |
|  | Convert Diamond Interchange to SPUI | VDOT Planning Level CMFs | http://onlinepubs.trb.org/onlinepubs/nchrp/docs/ nchrp17-45_fr.pdf | - |
|  | Extend Deceleration Lane Length by 100 Feet | CMD ID: 475 | http://www.cmfclearinghouse.org/detail. cfm? facid $=475$ | - |
|  | Interchange Lighting | CMF ID: 1283 | http://www.cmfclearinghouse.org/detail. cfm?facid=1283 | - |
|  | Lengthen Acceleration Lane from X Miles to Y Miles | CMF ID: 5215, 5216 | http://www.cmfclearinghouse.org/detail. cfm?facid=5215 | http://www.cmfclearinghouse.org/detail. cfm?facid=5216 |
|  | Replace Loop Ramp with Short Direct Ramp | CMF ID: 480 | http://www.cmfclearinghouse.org/detail. cfm? facid=480 | - |
|  | Widen Ramp Lane Width from X to Y in Feet | HSM Eqn 19-34 | http://onlinepubs.trb.org/onlinepubs/nchrp/docs/ nchrp17-45_fr.pdf | - |
|  | Widen Ramp Left Shoulder | HSM Eqn 19-36 | http://onlinepubs.trb.org/onlinepubs/nchrp/docs/ nchrp17-45_fr.pdf | - |
|  | Widen Ramp Right Shoulder | HSM Eqn 19-35 | http://onlinepubs.trb.org/onlinepubs/nchrp/docs/ nchrp17-45_fr.pdf | - |

VIRGINIA STATE PREFERRED CMF LIST

Table 3 References (cont)


VIRGINIA STATE PREFERRED CMF LIST

Table 3 References (cont)


VIRGINIA STATE PREFERRED CMF LIST

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Table 3 References (cont)


VIRGINIA STATE PREFERRED CMF LIST

Table 3 References (cont)


VIRGINIA STATE PREFERRED CMF LIST

Table 3 References (cont)

|  | COUNTERMEASURE | Reference | REFERENCE/CITATION HYPERLINK \#1 | REFERENCE/CITATION HYPERLINK \#2 |
| :---: | :---: | :---: | :---: | :---: |
|  | Upgrade Pavement Markings to Wet-Reflective Pavement Markings | CMF ID: 8093, 8134 | http://www.cmfclearinghouse.org/detail. cfm?facid=8093 | http://www.cmfclearinghouse.org/detail. cfm?facid=8134 |
|  | Upgrade Roadside Guardrail | Desktop Reference Guide | http://www.cmfclearinghouse.org/collateral/FHWA_ Desktop_Reference_Guide.pdf | - |
|  | Urban: Widen from 4 Lanes to 6 Lanes | VDOT SPFs, Crash Rate Ratios | http://vasmartscale.org/documents/ss_planning_ level_cmfs_092116.pdf | - |
|  | Urban: Widen from 4 Lanes to 8+ Lanes | VDOT SPFs, Crash Rate Ratios | http://vasmartscale.org/documents/ss_planning_ level_cmfs_092116.pdf | - |
|  | Urban: Widen from 6 Lanes to 8+ Lanes | VDOT SPFs, Crash Rate Ratios | http://vasmartscale.org/documents/ss_planning_ level_cmfs_092116.pdf | - |
|  | Widen Clear Zone from X Feet to Y Feet | HSM Eqn 18-38 | http://onlinepubs.trb.org/onlinepubs/nchrp/docs/ nchrp17-45_fr.pdf | - |
|  | Widen Median from X Feet to Y Feet | HSM Equation 18-27 | http://onlinepubs.trb.org/onlinepubs/nchrp/docs/ nchrp17-45_fr.pdf | - |
|  | Widen Paved Inside Shoulder from X Feet to Y Feet | HSM Eqn 18-26 | http://onlinepubs.trb.org/onlinepubs/nchrp/docs/ nchrp17-45_fr.pdf | - |
|  | Widen Paved Outside Shoulder on Horizontal Curve from X Feet to Y Feet | HSM Eqn 18-35 and Table 18-21 | http://onlinepubs.trb.org/onlinepubs/nchrp/docs/ nchrp17-45_fr.pdf | - |
|  | Widen Paved Outside Shoulder on Horizontal Tangent from $X$ Feet to $Y$ Feet | HSM Eqn 18-35 and Table 18-21 | http://onlinepubs.trb.org/onlinepubs/nchrp/docs/ nchrp17-45_fr.pdf | - |
| SEGMENTS (NON-FREEWAY) | Add Automated Speed Enforcement Cameras | CMF ID: 2688, 4583 | http://www.cmfclearinghouse.org/detail. cfm?facid=2688 | http://www.cmfclearinghouse.org/detail. cfm?facid=4583 |
|  | Add Auxiliary Passing Lane | CMF ID: 9111, 9112 | http://www.cmfclearinghouse.org/detail. cfm?facid=9111 | http://www.cmfclearinghouse.org/detail. cfm?facid=9112 |
|  | Add Centerline Rumble Strips (Including Sinusoidal/ Mumble) | CMF ID: 3355, 3360 | http://www.cmfclearinghouse.org/detail. cfm?facid=3355 | http://www.cmfclearinghouse.org/detail. cfm?facid=3360 |

VIRGINIA STATE PREFERRED CMF LIST

Table 3 References (cont)

|  | COUNTERMEASURE | Reference | REFERENCE/CITATION HYPERLINK \#1 | REFERENCE/CITATION HYPERLINK \#2 |
| :---: | :---: | :---: | :---: | :---: |
|  | Add Chevron Signs at Horizontal Curves | CMF ID: 2439 | http://www.cmfclearinghouse.org/detail. cfm?facid=2439 | - |
|  | Add Chevron Signs, Curve Warning Signs, and Sequential Flashing Beacons | CMF ID: 1852 | http://www.cmfclearinghouse.org/detail. cfm?facid=1852 | - |
|  | Add Raised Pavement Markers | CMF ID: 5496 | http://www.cmfclearinghouse.org/detail. cfm?facid=5496 | - |
|  | Add Safety Edge | FHWA Proven Safety Countermeasures | https://safety.fhwa.dot.gov/provencountermeasures/ safety_edge/ | - |
|  | Add Segment Lighting | CMF ID: 7781, 7782 | http://www.cmfclearinghouse.org/detail. cfm?facid=7781 | http://www.cmfclearinghouse.org/detail. cfm?facid=7782 |
|  | Add Shoulder Rumble Strips (Including Sinusoidal/ Mumble) | CMF ID: 3442, 3447 | http://www.cmfclearinghouse.org/detail. cfm?facid=3442 | http://www.cmfclearinghouse.org/detail. cfm?facid=3447 |
|  | Add Two-Way Left-Turn Lane (2U to 3T) | CMF ID: 2341, 2346 | http://www.cmfclearinghouse.org/detail. cfm?facid=2341 | http://www.cmfclearinghouse.org/detail. cfm?facid=2346 |
|  | Add Two-Way Left-Turn Lane (4U to 5T) | CMF ID: 4084 | http://www.cmfclearinghouse.org/detail. cfm?facid=4084 | - |
|  | Breakaway Supports for Utility Poles in Clear Zones | HSM Eqn 10-20 | https://www.fhwa.dot.gov/publications/research/ safety/99207/99207.pdf | - |
|  | Change 4" Wide Edgelines to 6" Wide Edgelines | CMF ID: 4737, 4738 | http://www.cmfclearinghouse.org/detail. cfm?facid=4737 | http://www.cmfclearinghouse.org/detail. cfm?facid=4738 |
|  | Change Driveway Density (Driveways/Mile) from X to Y | CMF ID: 1973, 2248 | http://www.cmfclearinghouse.org/detail. cfm?facid=1973 | http://www.cmfclearinghouse.org/detail. cfm?facid=2248 |
|  | Change Roadside Hazard Rating from $X$ to $Y$ by Flattening Roadside Slope | HSM Eqn 10-20 | https://www.fhwa.dot.gov/publications/research/ safety/99207/99207.pdf | - |
|  | Change Superelevation Variance from X to Y (if Variance Between 0.01 and 0.02) | HSM Eqn 10-15 | https://www.fhwa.dot.gov/publications/research/ safety/99207/99207.pdf | - |
|  | Change Superelevation Variance from X to Y (if Variance Greater than 0.02) | HSM Eqn 10-16 | https://www.fhwa.dot.gov/publications/research/ safety/99207/99207.pdf | - |
|  | Dynamic Speed Feedback Signs | CMF ID: 6885 | http://www.cmfclearinghouse.org/detail. cfm?facid=6885 | - |

VIRGINIA STATE PREFERRED CMF LIST

Table 3 References (cont)

|  | COUNTERMEASURE | reference | REFERENCE/CITATION HYPERLINK \#1 | REFERENCE/CITATION HYPERLINK \#2 |
| :---: | :---: | :---: | :---: | :---: |
|  | Flatten Horizontal Curve | CMF ID: 9271, 9272 | http://www.cmfclearinghouse.org/detail. cfm?facid=9271 | http://www.cmfclearinghouse.org/detail. cfm?facid=9272 |
|  | Implement High-Friction Surface Treatment on Horizontal Curve | CMF ID: 7900 | http://www.cmfclearinghouse.org/detail. cfm?facid=7900 | - |
|  | Increase Stopping Sight Distance on Crest Vertical Curve | CMF ID: 6868, 6869 | http://www.cmfclearinghouse.org/detail. cfm?facid=6868 | http://www.cmfclearinghouse.org/detail. cfm?facid=6869 |
|  | Pave Unpaved Shoulder | HSM Eqn 10-12, Table 10-9 and 10-10 | https://www.fhwa.dot.gov/publications/research/ safety/99207/99207.pdf | - |
|  | Pavement Resurfacing - Rural | CMF ID: 5626 | http://www.cmfclearinghouse.org/detail. cfm?facid=5626 | - |
|  | Pavement Resurfacing - Urban | CMF ID: 9289, 9290 | http://www.cmfclearinghouse.org/detail. cfm?facid=9289 | http://www.cmfclearinghouse.org/detail. cfm?facid=9290 |
|  | Prohibit On-Street Parking | CMF ID: 4574, 4575 | http://www.cmfclearinghouse.org/detail. cfm?facid=4574 | http://www.cmfclearinghouse.org/detail. cfm?facid=4575 |
|  | Remove or Relocate Fixed Object Outside of Clear Zone | CMF ID: 1024, 1044 | http://www.cmfclearinghouse.org/detail. cfm?facid=1024 | http://www.cmfclearinghouse.org/detail. cfm?facid=1044 |
|  | Road Diet (4U to 3T) | CMF ID: 199 | http://www.cmfclearinghouse.org/detail. cfm? facid=199 | - |
|  | Upgrade Chevrons with Flourescent Sheeting | CMF ID: 2434 | http://www.cmfclearinghouse.org/detail. cfm?facid=2434 | - |
|  | Upgrade Pavement Markings by Increasing Retroreflectivity | CMF ID: 2116, 2117, 2120 | http://www.cmfclearinghouse.org/detail. cfm?facid=2116 | http://www.cmfclearinghouse.org/detail. cfm?facid=2117 |
|  | Upgrade Pavement Markings to Wet-Reflective Pavement Markings | CMF ID: 8093, 8134 | http://www.cmfclearinghouse.org/detail. cfm?facid=8093 | http://www.cmfclearinghouse.org/detail. cfm?facid=8134 |
|  | Widen Clear Zone | CMF ID: 35 | http://www.cmfclearinghouse.org/detail.cfm?facid=35 | - |
|  | Widen Lane | HSM Table 10-8, Eqn 10-11 | https://www.fhwa.dot.gov/publications/research/ safety/99207/99207.pdf | - |
|  | Widen Average Shoulder Width | HSM Table 10-9 | https://www.fhwa.dot.gov/publications/research/ safety/99207/99207.pdf | - |

## Appendix I

## Previous Studies

## Appendix I-1

## VDOT Study

# COMMONWEALTH of VIRGINIA 

 DEPARTMENT OF TRANSPORTATIONCulpeper District
Traffic Engineering

## Route $\mathbf{7 4 3}$ \& Route 660 in Albemarle County

 Intersection Safety Evaluation

Route: Route 743 (Earlysville Rd) at Route 660 (Reas Ford Rd \& Earlysville Forest Dr) Location: Albemarle County, Virginia
Project Description: Intersection Safety Evaluation
Date: January 5, 2018
Prepared By: Jet R Dienner

## Intersection Safety Evaluation Route 743 and Route 660, Albemarle County

## Background

Culpeper District Traffic Engineering was requested by Delegate Rob Bell on behalf of citizens and residents in the area to evaluate safety at the intersection of Route 743 (Earlysville Road) and Route 660 (Reas Ford Road \& Earlysville Forest Dr). This intersection has been the subject of several study requests in the past, and this document is intended to provide information and guidance for future improvements as traffic volumes and development increases in this area in the future. Crash data, intersection sight distance, signal warrants, turn lane warrants, and sign and pavement markings were reviewed to identify possible operational and safety improvements. The subject intersection is shown in the study area maps below.


## Existing Conditions

Route 743 (Earlysville Road) is a two lane roadway with an additional right turn lane in the northbound direction. It has a functional classification of Urban Collector, with a 2016 AADT of 9,500 vehicles per day, and is posted at 35 MPH within the limits of the study area. Route 660 west of the intersection (Reas Ford Rd) is a two lane roadway with a Rural Major Collector functional classification, a 2016 AADT of 2,000 vehicles per day, and is posted at 35 MPH within the limits of the study area. Route 660 east of the intersection (Earlysville Forest Dr) is a two lane roadway with a Urban Local functional classification, a 2016 AADT of 1,000 vehicles per day, and is posted at 35 MPH within the limits of the study area. Both approaches of Route 743 have appropriate MUTCD compliant advance intersection warning signs. Both approaches of Route 660 are currently stop-controlled at the intersection with appropriate MUTCD compliant "Stop Ahead" signs installed in advance of the intersection. The eastbound approach of Route 660 includes "Stop Ahead" pavement markings.

## Crash Analysis

Five years of the most current crash data (June 1, 2012 through June 30, 2017) was examined. During that time frame there were 12 crashes within $300^{\prime}$ of the intersection. These crashes included four angle crashes, three left turn crashes, two road departure crashes, and three rear end crashes. Of the twelve crashes, there were three injury crashes resulting in four total injuries. One of the injury crashes was an angle crash resulting in two injuries, one road departure crash resulting in one injury, and the remaining injury came from a rear end crash. See exhibit 1 (of this report) for a detailed crash diagram.

## Sight Distance Analysis

Sight Distance is a critical factor that plays into the cause of many angle crashes at an intersection. The AASHTO Green-book states that the Intersection sight distance for a 35 MPH roadway is a distance of 390 feet. The minimum measured sight distance was $420^{\prime}$ on the SB approach of Route 660. Left and Right sight distance requirements were exceeded for all approaches of the intersection as shown on the sight distance diagram (exhibit 2 of this report). It was observed that the stop bar on the SB approach can be shifted 8 ' closer to the edge of travel way, which will increase the sight distance on this approach by 40'+/-.

## Signal Warrant Analysis-Methodology

The 2009 Edition of the MUTCD lists various Traffic Signal warrants to analyze in consideration for the installation of a Traffic Signal at intersecting roadways. For this safety study Warrant 1 -- Eight-Hour Vehicular Volume, Warrant 2 -- Four-Hour Vehicular Volume, and Warrant 7 -- Crash Experience, were analyzed to determine if this intersection would meet any of these warrants. Warrant 3 -- Peak Hour was not analyzed as the Peak Hour warrant is applicable only in "unusual cases, such as office complexes, manufacturing plants, industrial complexes, or high-occupancy vehicle facilities that attract or discharge large numbers of vehicles over a short time" (2009 MUTCD, Section 4C.04). Based on the classification of the major route and field observation, the peak hour warrant did not currently apply. Refer to Chapter 4C, "Traffic Control Signal Needs Studies" in the 2009 edition of the MUTCD for detailed descriptions of each traffic signal Warrant criteria. A 12 hour turning movement count was collected on November 14, 2016 from 6:30 AM to 6:30 PM. The data gathered was used to analyze the 8 and 4 hour warrants. Based on the Urban Collector functional classification of Route 743, the close proximity to neighborhoods, and the posted 35 MPH speed limit, urban values were used. PC Warrants software was used to analyze the data (exhibit 3 of this report). It was noted during the 12 hour field observation that minimal delay and queue lengths were observed. The longest observed queue was six vehicles on EB 660. The following summarizes the findings regarding the signal warrant analysis for the study intersection. The current traffic volumes do not meet eight or four hour signal warrants. The minor route (Route 660) traffic volumes are $30 \%$ below the threshold for meeting eight hour signal Warrant 1A. Results of the signal warrant analysis for the eight and four hour warrants and the crash warrant are below:

## Results

Warrant 1, Eight-Hour Vehicular Volume:

Condition A: The minimum vehicular volume is intended for application at locations where a large volume of intersecting traffic is the principal reason to consider installing a traffic control signal. For Route 743, Condition A requires 500 vehicles per hour for any eight hours of the average day; Route 660 is required to carry 150 vehicles per hour for the same eight hours (Table 4C-1) on the highest volume approach. Route 660 carries 124 vehicles in its peak hour with no right turn discount.

Due to the minor street approach volumes, Warrant 1 A is not met.

Condition B: The interruption of continuous traffic is intended for application at locations where Condition $A$ is not satisfied and where the traffic volume on a major street is so heavy that traffic on a minor intersecting street suffers excessive delay or conflict in entering or crossing the major street. The volumes required for the same eight hours for Route 743 and Route 660 are 750 vehicles per hour and 75 vehicles per hour respectively. Route 743 only carries sufficient volume to meet Condition B for 2 of the counted hours.
Due to lack of sufficient volumes Warrant 1B is not met.

Condition $C$ : The combination of conditions $A$ and $B$ is intended for application at location where Condition A is not satisfied and Condition B is not satisfied only after an adequate trial of other alternatives that could cause less delay and inconvenience to traffic has failed to solve the traffic problems. For Condition C, $80 \%$ of the volumes in both Condition A and B must be met. Based on current volumes this intersection does not meet this criterion.

## Due to lack of sufficient volumes, Warrant 1C is not met.

Table 4C-1. Warrant 1, Eight-Hour Vehicular Volume
Condition A-Minimum Vehicular Volume

| Number of la traffic on | es for moving approach | Vehicles per hour on major street (total of both approaches) |  |  |  | Vehicles per hour on higher-volume minor-street approach (one direction only) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street | Minor Street | $100 \%{ }^{\text {a }}$ | 80\% ${ }^{\text {b }}$ | 70\% ${ }^{\text { }}$ | 56\% ${ }^{\text {d }}$ | 100\% ${ }^{\text {a }}$ | 80\% ${ }^{\text {b }}$ | 70\% ${ }^{\circ}$ | 56\% ${ }^{\text {d }}$ |
| 1 | 1 | 500 | 400 | 350 | 280 | 150 | 120 | 105 | 84 |
| 2 or more | 1 | 600 | 480 | 420 | 336 | 150 | 120 | 105 | 84 |
| 2 or more | 2 or more | 600 | 480 | 420 | 336 | 200 | 160 | 140 | 112 |
| 1 | 2 or more | 500 | 400 | 350 | 280 | 200 | 160 | 140 | 112 |

Condition B-Interruption of Continuous Traffic

| Number of lanes for moving traffic on each approach |  | Vehicles per hour on major street (total of both approaches) |  |  |  | Vehicles per hour on higher-volume minor-street approach (one direction only) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street | Minor Street | 100\% ${ }^{\text {a }}$ | 80\% ${ }^{\text {b }}$ | 70\% ${ }^{\circ}$ | 56\% ${ }^{\text {d }}$ | 100\% ${ }^{\text {a }}$ | $80 \%{ }^{\text {b }}$ | 70\% ${ }^{\circ}$ | 56\% ${ }^{\text {d }}$ |
| 1 | 1 | 750 | 600 | 525 | 420 | 75 | 60 | 53 | 42 |
| 2 or more | 1 | 900 | 720 | 630 | 504 | 75 | 60 | 53 | 42 |
| 2 or more | 2 or more | 900 | 720 | 630 | 504 | 100 | 80 | 70 | 56 |
| 1 | 2 or more | 750 | 600 | 525 | 420 | 100 | 60 | 70 | 56 |

a Basic minimum hourly volume
${ }^{\text {b }}$ Used for combination of Conditions A and B after adequate trial of other remedial measures

- May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000
${ }^{d}$ May be used for combination of Conditions A and B afier adequate trial of other remedial measures when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000


## Warrant 2, Four-Hour Vehicular Volume

The four hour vehicular volume signal warrant conditions are intended to be applied where the volume of intersecting traffic is the principal reason to consider installing a traffic control signal. Warrant 2 requires that for any four hours of the day the vehicles per hour from the minor street plotted with the total vehicles per hour for the same four hours must fall above the curve shown below. The required minimum volume on Route 660 only met for the required volumes for 1 out of the required 4 hours.

The minor approaches do not have sufficient volume for four hours a day and Warrant 2 is not met.


## Warrant 7, Crash Experience

Two correctable crashes (by type) occurred in the most recent year of crash data. In order for the crash warrant to be met, five crashes of a correctable type must occur at the intersection within the 12 month study period, after an adequate trial of alternatives with satisfactory observance and enforcement has failed to reduce the crash frequency. Current district average is one per year. See exhibit 1 (of this report) for a detailed crash diagram.

The two crashes of a correctable type in the intersection within the past 12 months does not meet the five required by the warrant. Warrant 7 is not met.

## Turn Lane Warrant Analysis-Methodology

Turn Lane Warrants were examined for all approaches per the guidance provided in Appendix F, Section 3 "Turning Lanes" of the VDOT Road Design Manual. These warrants were provided as a part of this report to provide an analysis of how the intersection is functioning operationally, and provide guidance for recommended improvements as traffic volumes and development in the area increases. These analyses are attached as Exhibit 4 of this report. The table below summarizes the results:

| TURN LANE WARRANT SUMMARY <br> (L= Storage Lane Length, T=Taper Length) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right Turn <br> Lane/Taper | Right Turn Storage <br> Lane \& Taper Length | Left Turn <br> Lane/Taper | Left Turn Storage <br> Lane \& Taper Length |  |
| Route <br> 743 NB | N/A | Existing |  <br> Taper Warrants | L= 200', T=200' <br> Route <br> 743 SB <br> Route <br> 660 EB <br> Only <br> Taper Warrants |  |
| Route <br> 660 WB | Does not meet <br> warrants | $\mathrm{T}=200^{\prime}, \mathrm{T}=200^{\prime}$ | Does not meet <br> warrants | N/A |  |

## Study Summary and Proposed Recommendations

Upon review of the intersection crash history, existing traffic control devices, daily traffic volumes, and available sight distance, it has been determined that the existing roadway geometrics and traffic control devices are functionally adequate in safely controlling the current volume of traffic at this intersection. While the current crash volumes are relatively low, the study revealed things that can be improved in the short, intermediate, and long-term to improve the safety and functionality of the intersection as traffic volumes and development increases. These results and recommendations are listed below.

Results of the crash data and signal warrants show that a signal is NOT warranted at Route 743 (Earlysville Rd) and Route 660 (Reas Ford Rd \& Earlysville Forest Dr). None of the signal warrants, including the crash warrant, were currently met. The current stop signs and advance warning signs are appropriate as installed with no upgrades recommended at the time of this study.

Recommendations have been categorized into short, intermediate and long-term. These are typically defined as follows:
Short Term Recommendations can be generalized as improvements that are low cost, quickly implementable (within a few weeks to a few months), require little or no engineering design, typically require no right-of way, and can be done with state or contractor work forces.
Intermediate Term Recommendations can be generalized as improvements that are low to mid-range in cost, implementable within six months to a couple years, require minimal engineering design, typically require little or no right-of way, and can be implemented partially or in full with state or contractor work forces.
Long Term Recommendations can be generalized as those improvements that are mid to high cost, require planning and design, may take one to six years to implement, typically require right-of way, and are typically implemented through a contract with contractor work forces.

## Short Term Recommendations:

- Refresh "Stop Ahead" pavement markings
- Shift WB approach stop bar to improve sight distance
- Refresh EB approach stop bar

The review of the pavement markings and intersection sight distance revealed some things that can be upgraded and improved to improve the overall safety of intersection. The current "Stop Ahead" pavement marking on the eastbound approach of Route 660 are faded and should be refreshed. The transverse white lines prior and after these pavement markings should be removed. The existing stop bar on the WB approach of 660 is currently $16^{\prime}$ from the edge of the travel lane on Route 743 . Shifting this stop bar forward $8^{\prime}$ would improve the sight distance left by 40+/-, improving driver reaction/response time and improving safety. See exhibit 5 for the proposed pavement marking plan which includes both of these short term recommendations.

## Intermediate Term Recommendations:

- Upgrade existing commercial entrances to meet VDOT standards
- Install a right turn lane on the EB approach

Results of the 5-year crash analysis show that there have been three crashes related to left turn movements into the commercial parcel on the northwest corner. This parcel does not currently have an entrance that meets VDOT Access Management standards. This entrance should be improved to meet standards in the future as it is developed.

Results of the turn lane warrants analysis revealed that a right turn lane is warranted on the EB approach of Route 660. Based on field observation, and the collected turning movement counts, this right turn is the highest volume turn movement of all (left or right) approaches. It is recommended that a right turn lane be constructed as funding and right of way become available (potentially with the development of the adjacent parcel). It appears that this turn lane could be constructed with minimal right of way acquisition, and grading/utility impacts, and it would currently provide the most Intermediate Term benefit to the operations of the intersection.

## Long Term Recommendations

- Evaluate and install a roundabout as the preferred intersection alternative The results from the turn lane analysis show that right and left turn lanes are warranted under current traffic volumes on the EB and NB approaches. As traffic volumes and development increases in the area queues and delays are likely to increase to a point where operations and safety will warrant significant intersection upgrades. While a right tune lane on the EB approach is an intermediate term recommendation at this location, a left turn lane would cost significantly more due to the right of way acquisition and utility relocation cost. Additionally the potential points of conflict would not be reduced by the addition of turn lanes, and the NB approach grades limit sight distance to potential queued traffic increasing the risk of rear end crashes. Based operations, safety, and NB sight distance it is recommended that a roundabout be evaluated in the future as the preferred alternative.


## EXHIBIT 1

Crash Diagram

## COLLISION DIAGRAM

Rte. 743 (Earlysville $\mathbb{R} d_{0}$ ) at Rt. 660 (Reas Ford Rd.)
Allbemarlle County


## EXHIBIT 2

Sight Distance Diagram


## EXHIBIT 3 <br> PC Warrants Report

## VDOT Culpeper District Traffic Division <br> Route 743 (Earlysville Rd) and Route 660 (Reas Ford Rd)

## Signal Warrants - Summary

Major Street Approaches Minor Street Approaches
Northbound: 4750 Eastbound: 1000
Number of Lanes: 1
Total Approach Volume: 866
Westbound: 500
Number of Lanes: 1
Total Approach Volume: 563
Warrant Summary (Urban values apply.)
Warrant 1 - Eight Hour Vehicular Volumes ........................................................................................................................................ Not Satisfied
Warrant 1A - Minimum Vehicular Volume Not Satisfied
Required volumes reached for 0 hours, 8 are needed
Warrant 1B - Interruption of Continuous Traffic Not Satisfied
Required volumes reached for 3 hours, 8 are needed
Warrant 1 A\&B - Combination of Warrants Not Satisfied
Required volumes reached for 1 hours, 8 are needed
Number of hours (0) volumes exceed minimum < minimum required (4).
Warrant 3A - Peak Hour Delay ...
Warrant 3B - Peak Hour Volumes Not Evaluated
Warrant 4 - Pedestrian Volumes
Warrant 5 - School Crossing ..... Not Evaluated
Warrant 6-Coordinated Signal System ..... Not Evaluated
Warrant 7-Crash Experience
Number of accidents (2) is less than minimum (5). Volume minimums are not met.
Warrant 8 - Roadway Network ..... Not Evaluated

## VDOT Culpeper District Traffic Division <br> Route 743 (Earlysville Rd) and Route 660 (Reas Ford Rd)

Signal Warrants - Summary


Analysis of 8-Hour Volume Warrants:


## EXHIBIT 4

## Turn Lane Warrants Analysis

WARRANTS FOR RIGHT TURN TREATMENT (2-LANE HIGHWAY)
Major Route \& Direction: Route 660 WB


Note: This spreadsheet is intended to supplement the guidance provided in Appendix F, Section 3 Turning Lanes, of the VDOT Road Design Manual. This policy should be fully reviewed and understood prior to using this application.

WARRANTS FOR RIGHT TURN TREATMENT (2-LANE HIGHWAY)
Major Route \& Direction: Route 743 SB


Note: This spreadsheet is intended to supplement the guidance provided in Appendix F, Section 3 Turning Lanes, of the VDOT Road Design Manual. This policy should be fully reviewed and understood prior to using this application.

WARRANTS FOR LEFT TURN LANES ON TWO-LANE HIGHWAYS
Major Route \& Direction: Route 743 SB


Left Turn Lane NOT WARRANTED

| VPH OPPOSING VOLUME | ADVANCING VOLUME |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 5\% | 10\% | 20\% | 30\% |
|  | LEFT TURNS | LEFT TURNS | LEFT TURNS | LEFT TURNS |
|  | 40-MPH DESIGN SPEED* |  |  |  |
| 800 | 330 | 240 | 180 | 160 |
| 600 | 410 | 305 | 225 | 200 |
| 400 | 510 | 380 | 275 | 245 |
| 200 | 640 | 470 | 350 | 305 |
| 100 | 720 | 515 | 390 | 340 |
|  | 50-MPH DESIGN SPEED* |  |  |  |
| 800 | 280 | 210 | 165 | 135 |
| 600 | 350 | 280 | 195 | 170 |
| 400 | 430 | 320 | 240 | 210 |
| 200 | 550 | 400 | 300 | 270 |
| 100 | 615 | 445 | 335 | 295 |
|  | 60-MPH DESIGN SPEED* |  |  |  |
| 800 | 230 | 170 | 125 | 115 |
| 600 | 290 | 210 | 160 | 140 |
| 400 | 365 | 270 | 200 | 175 |
| 200 | 450 | 330 | 250 | 215 |
| 100 | 505 | 370 | 275 | 240 |

TABLE 3-2
Source: Adapted from 2011 AASHTO Green Book, Chapter 9, Section 9.7.3, Page 9-132, Table 9-23

* USE DESIGN SPEED IF AVAILABLE, IF NOT USE LEGAL SPEED LIMIT.

Note: This spreadsheet is intended to supplement the guidance provided in Appendix F, Section 3
Turning Lanes, of the VDOT Road Design Manual. This policy should be fully reviewed and understood prior to using this application.

WARRANTS FOR LEFT TURN LANES ON TWO-LANE HIGHWAYS
Major Route \& Direction: Route 743 NB


| $\begin{gathered} \text { VPH } \\ \text { OPPOSING } \\ \text { VOLUME } \end{gathered}$ | ADVANCING VOLUME |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $5 \%$ <br> LEFT TURNS | $10 \%$ <br> LEFT TURNS | $\begin{gathered} 20 \% \\ \text { LEFT TURNS } \end{gathered}$ | $30 \%$ LEFT TURNS |
|  | 40-MPH DESIGN SPEED* |  |  |  |
| 800 | 330 | 240 | 180 | 160 |
| 600 | 410 | 305 | 225 | 200 |
| 400 | 510 | 380 | 275 | 245 |
| 200 | 640 | 470 | 350 | 305 |
| 100 | 720 | 515 | 390 | 340 |
|  | 50-MPH DESIGN SPEED* |  |  |  |
| 800 | 280 | 210 | 165 | 135 |
| 600 | 350 | 280 | 195 | 170 |
| 400 | 430 | 320 | 240 | 210 |
| 200 | 550 | 400 | 300 | 270 |
| 100 | 615 | 445 | 335 | 295 |
|  | 60-MPH DESIGN SPEED* |  |  |  |
| 800 | 230 | 170 | 125 | 115 |
| 600 | 290 | 210 | 160 | 140 |
| 400 | 365 | 270 | 200 | 175 |
| 200 | 450 | 330 | 250 | 215 |
| 100 | 505 | 370 | 275 | 240 |

TABLE 3-2
Source: Adapted from 2011 AASHTO Green Book, Chapter 9, Section 9.7.3, Page 9-132, Table 9-23

* USE DESIGN SPEED IF AVAILABLE, IF NOT USE LEGAL SPEED LIMIT.

Note: This spreadsheet is intended to supplement the guidance provided in Appendix F, Section 3
Turning Lanes, of the VDOT Road Design Manual. This policy should be fully reviewed and understood prior to using this application.

WARRANTS FOR RIGHT TURN TREATMENT (2-LANE HIGHWAY)
Major Route \& Direction: Route 660 EB


Note: This spreadsheet is intended to supplement the guidance provided in Appendix F, Section 3 Turning Lanes, of the VDOT Road Design Manual. This policy should be fully reviewed and understood prior to using this application.

## EXHIBIT 5 <br> Proposed Pavement Marking Plan



## EXHIBIT 6

Conceptual Right Turn Lane Improvements


## Appendix I-2

## Kimley Horn Study

# Earlysville Road (Route 743) and Reas Ford Road (Route 660) 

## Intersection Safety Review

## Albemarle County, VA

November 2019

Prepared for:
Virginia Department of Transportation

Prepared by:<br>Kimley-Horn and Associates, Inc. 1700 Willow Lawn Drive, Suite 200<br>Richmond, Virginia 23230<br>P: 804.673.3882

Kimley-Horn Project \#. 117473204
Kimley»"Horn
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### 1.0 Introduction

The Virginia Department of Transportation (VDOT) has received complaints and various inquiries from members of the Albemarle County Board of Supervisors, local emergency services personnel, and local residents regarding the perception of safety issues at the Earlysville Road (Route 743) and Reas Ford Road (Route 660) intersection in Albemarle, Virginia. Further discussions between VDOT and Albemarle County led to the need to evaluate the existing conditions at the study intersection. This evaluation will be used to identify potential transportation improvement solutions at the study intersection and to assist VDOT and Albemarle County staff in their discussions with property owners and developers as they convey future plans and projects in the vicinity of the study intersection. Specifically, the intended outcomes of this study were to:
*. Determine the safety and integrity of existing transportation infrastructure

* Provide recommended improvements that improve safety and mobility at the intersection

The purpose of this study was to evaluate potential improvements to the intersection of Earlysville Road and Reas Ford Road to enhance intersection safety and operations. This study focused primarily on safety during typical weekday operations. Traffic operations and access management were also analyzed in order to develop a cohesive recommendation. The limits of this study area are defined by the functional area of the Earlysville Road and Reas Ford Road intersection, which is approximately 500 feet on each approach.

This study will serve as a technical document that describes and illustrates the feasibility of the proposed alternatives as well as the associated potential operational and safety impacts of each.

### 2.0 Existing Conditions

### 2.1 Field Review

A field review was conducted on September 3, 2019 to observed existing conditions at the study intersection. Available traffic, crash and asset data was obtained from VDOT and used to document existing conditions. During the field review, the following information was observed and collected.

* Observations of existing roadway geometrics, such as lane designations, signing, striping, posted speed limits, sight distance restrictions, potential design impacts or constraints
* Observations of existing roadway conditions to determine opportunities for improvements to increase safety
* Observations of traffic operations including passenger cars and trucks
* Digital photographs to capture the study area characteristics observed

The existing conditions analyses were developed using the data collected during the field review supplemented by visual observations of the operational characteristics.

### 2.2 Roadway Characteristics

Earlysville Road is classified as an urban major collector according to VDOT's 2014 Functional Classification map. The section of roadway within the study area is oriented in an east-west direction and is a two-lane, undivided roadway with a paved shoulder ranging from 0 to 10 feet wide and an open ditch cross section. Photographs 1 and 2 show the westbound and eastbound approaches, respectively. The Earlysville Road posted speed limit is 35 M PH near Reas Ford Road. The posted speed limit increases to 45 M PH approximately 300 feet east of the intersection. A Cross Road (W2-1) warning sign is located approximately 525 feet in advance of Reas Ford Road on the eastbound and westbound approaches.

Reas Ford Road is classified as a rural major collector south of Earlysville Road according to VDOT's 2014 Functional Classification map. The roadway is referred to as Reas Ford Road south of Earlysville Road and is referred to as Earlysville Forest Drive north of Earlysville Road. The section of roadway within the study area is oriented in a north-south direction and is a two-lane, undivided roadway with no shoulder and an open ditch cross section. Photographs $\mathbf{3}$ and $\mathbf{4}$ show the northbound and southbound approaches, respectively. The Reas Ford Road/Earlysville Forest Drive posted speed limit is 35 M PH near Earlysville Road. A Stop Ahead (W3-1) warning sign is located approximately 300 feet in advance of Earlysville Road on the northbound approach.


Photograph 1: Westbound Approach - Earlysville Road


Photograph 3: Northbound Approach - Reas Ford Road


Photograph 2: Eastbound Approach - Earlysville Road


Photograph 4: Southbound Approach - Earlysville Forest Drive

The study intersection currently operates as a two-way stop intersection. A variety of land uses are located within the vicinity of the subject intersection, including residential, commercial, and civic (e.g. post office) uses. The northbound and southbound approaches are stop-controlled and the eastbound and westbound approaches are free-flow. Turn lanes are not provided at the study intersection except for a right-turn lane on the westbound approach on Earlysville Road. Intersection lighting and bicycle and pedestrian accommodations are not provided at the study intersection. A Vehicular Traffic (W11-1) warning sign with a Share the Road (W16-1P) plaque is located approximately 250 feet east of the intersection along Earlysville Road.

The required sight distance on a 35 M PH roadway (per the VDOT Road Design Manual) is 390 feet. The sight distance on the northbound approach, looking to the left, is approximately 200 feet, which is below the minimum required. An intersection with a sight distance of 200 feet would only accommodate a design speed of approximately 17 MPH.

### 2.3 Traffic Volumes

A weekday 12-hour (6:30 AM - 6:30 PM ) turning movement count was conducted at the study intersection on Tuesday, November 14, 2017 and included in Appendix A. Weekday AM and PM peak hours were computed to be 7:30-8:30 AM and 5:00-6:00 PM , respectively. Based on the 2018 VDOT published traffic data, the approximate annual average daily traffic (AADT) volume on Earlysville Road is 9,700 vehicles per day (VPD) near Reas Ford Road. The approximate AADT volume on Reas Ford Road is 2,000 VPD to the south of Earlysville Road. The approximate AADT on Earlysville Forest Drive is 1,000 VPD to the north of Earlysville Road.

### 2.4 Crash Analysis

Crash analysis for the study intersection was conducted using the latest five years of available crash data. Crash reports dating from January 1, 2014 to M ay 31, 2019 were obtained from VDOT. Over the five-year period, twenty crashes were reported within a 500-foot radius of the study intersection.

```
* 2014: }0\mathrm{ crashes
* 2015: }3\mathrm{ crashes
* 2016: }4\mathrm{ crashes
* 2017: }8\mathrm{ crashes
* 2018: }4\mathrm{ crashes
* 2019: }1\mathrm{ crash
```

Overall, there were no noteworthy crash patterns identified at the study intersection. The following subsections provide additional information associated with the twenty total crashes that occurred at the study intersection.

## Crash by Type



> A majority of crashes (40\%) were angle collisions. However, these crashes were divided between the various approaches and turning movements.
> The remaining 12 crashes were equally divided between rear-end, fixed object, and other.

Crashes by Time of Day


* The majority of crashes (13 crashes or $65 \%$ ) occurred during off peak periods.
* The majority of the peak period crashes ( 5 of the 7 total peak period crashes) occurred during the PM peak period.


## Crash Severity

No fatal crashes occurred at the study intersection. Ten (50\%) of the crashes resulted in an injury. Three of these were Type A crashes, six were Type B, and one was Type C.

## Weather Conditions

Eighteen of the twenty crashes occurred during clear weather conditions at the study intersection.

## Light Conditions

Sixteen ( $80 \%$ ) of the twenty crashes occurred during daylight conditions at the study intersection.

### 2.5 Intersection Capacity Analyses

Capacity analyses allow traffic engineers to assess the operational conditions and identify the impacts of traffic on the surrounding roadway network. The Transportation Research Board's (TRB) Highway Capacity M anual (HCM) methodologies govern the methodology for evaluating capacity and the quality of service provided to road users traveling through a roadway network. There are six letter grades for Levels of Service (LOS) ranging from A to F, with LOS A representing the best operating conditions and LOS F representing the worst operating conditions.

Intersection level of service is defined in terms of delay (seconds per vehicle), a measure of driver discomfort, frustration, fuel consumption, and lost travel time. Error! Reference source not found summarizes the delay associated with each unsignalized and roundabout intersection LOS category.

Table 1: Intersection Level of Service Criteria

| LOS | Intersection Delay (sec/veh) |  |
| :---: | :---: | :---: |
|  | Unsignalized | Roundabout/ Signalized |
| A | $0-10$ | $0-10$ |
| B | $>10-15$ | $>10-20$ |
| C | $>15-25$ | $>20-35$ |
| D | $>25-35$ | $>35-55$ |
| E | $>35-50$ | $>55-80$ |
| F | $>50$ | $>80$ |
| Source: Transportation | Research Board, Highway Capacity Manual 2000 |  |

* Source: Transportation Research Board, Highway Capacity M anual 2000

The unsignalized study intersection was analyzed using Synchro based on methodologies in the HCM 6. Existing conditions Synchro delay and LOS results are shown in Error! Reference source not found. Synchro output sheets are included in Appendix D.

The stop-controlled approaches (northbound and southbound) currently experience moderate to long delays in the peak hours as shown in Table 5. It is typical for stop sign controlled side streets intersecting major streets to experience long delays during peak hours, while the majority of the traffic moving through the intersection on the major street experiences little or no delay.

Table 2: 2017 Existing Conditions Synchro Results

| Time of Day | Delay <br> (sec/ veh) | LOS | Delay <br> (sec/veh) | LOS |
| :--- | :---: | :---: | :---: | :---: |
| Lane Group | AM Peak Hour | PM PeakHour |  |  |
| Earlysville Rd (EB) LTR | 0.1 | A | 0.7 | A |
| Earlysville Rd (WB) LTR | 2.8 | A | 1.0 | A |
| Reas Ford Rd (NB) LTR | 37.5 | E | 35.5 | E |
| Earlysville Forest Dr (SB) LTR | 130.4 | F | 34.8 | D |

### 3.0 Alternative Development and Analysis

All traffic operations analysis for alternatives analysis was conducted using 2017 volumes. The VDOT Junction Screening Tool (VJUST) version 1.02 was used to develop potential alternatives to consider for analysis. Results from the VJUST analysis are included in Appendix C. After consideration of the VJUST results, a roundabout was selected as an alternative to further evaluate. Traditional intersection configuration analyses were conducted using Synchro while roundabout analyses were conducted using SIDRA.

The following alternatives were evaluated:

* Alternative 1: Low-Cost Countermeasures
* Alternative 2: M ini-Roundabout
* Alternative 2: Signalized Intersection


### 3.1.1 Alternative 1 (Low-Cost Countermeasures)

Alternative 1 consists of the implementation of multiple low-cost countermeasures for stop-controlled intersections. Alternative 1 does not improve any access management issues, operations issues, nor heavily improve any safety issues, but would reduce potential risks within the intersection. According to FHWA, this alternative "involves deploying a group of multiple low-cost countermeasures, such as enhanced signing and pavement markings...to increase driver awareness and recognition of the intersection and potential conflicts." The following treatments are recommended.

* Earlysville Road
- Doubled up (left and right), oversized advance intersection (W2-1) warning signs, with street name sign (W16-8aP) plaques
- Enhanced pavement markings that delineate through lane edge lines
* Reas Ford Road/ Earlysville Forest Drive
- Doubled up (left and right), oversized advance "Stop Ahead" (W3-1) intersection warning signs
- Doubled up (left and right), oversized Stop (R1-1) signs
- Retroreflective sheeting on sign posts
- Properly placed stop bar
- Removal of any vegetation or obstruction that limits sight distance

The implementation of these low-cost countermeasures at stop-controlled intersections can result in a 10\% reduction in injury and fatal crashes, based on Crash Reduction Factors (CRF).

Traffic conditions are not expected to change with the implementation of Alternative 1, therefore a separate traffic operations analysis was not conducted.

## -Figure 1 <br> 3.1.2 Alternative 2 (Mini-Roundabout)

As shown in Error! Reference source not found., Alternative 2 consists of the reconfiguration of the subject intersection to a mini-roundabout. In addition to an improvement to intersection capacity, the proposed roundabout would potentially improve safety as well by reducing the number of conflict points in the intersection. The installation of a roundabout can expect a $72 \%$ reduction in all intersection related crashes. The proposed roundabout would also mitigate sight distance deficiency on the northbound approach and act as a traffic calming measure on all approaches of the intersection. The analysis herein was based on minimum design requirements found in the VDOT Road Design M anual - Appendix F and the National Cooperative Highway Research Program (NCHRP) Report 672: Roundabouts: An Informational Guide, Second Edition, 2010.

Figure 1: Alternative \#2-Mini-Roundabout


The roundabout alternative was analyzed using SIDRA, which uses the HCM 6 traffic signal delay thresholds to determine LOS. To evaluate the study intersection, existing traffic volume data was used in conjunction with existing and proposed geometric data to determine the LOS.

The construction of a roundabout at the study intersection is expected to improve traffic operations for the northbound and southbound approaches while still maintaining short to moderate levels of delay along the eastbound and westbound approaches. The increase in control delay for the eastbound and westbound approaches is to be expected when converting free-flow movements to yield-controlled. Table 6 summarizes the delay for Alternative 2. Additional information is provided in Appendix D.

Table 3: 2017 Altemative 2 (Proposed Mini-Roundabout) SIDRA Results

| Time of Day | Delay <br> (sec/ veh) | LOS | Delay <br> (sec/veh) | LOS |
| :--- | :---: | :---: | :---: | :---: |
| Lane Group | AM Peak Hour | PM Peak Hour |  |  |
| Earlysville Rd (EB) LTR | 20.5 | C | 5.8 | A |
| Earlysville Rd (WB) LTR | 5.3 | A | 9.7 | A |
| Reas Ford Rd (NB) LTR | 5.1 | A | 17.9 | C |
| Earlysville Forest Dr (SB) LTR | 27.2 | D | 6.5 | A |

### 3.2 Alternative 3: Signalized Intersection

A signal warrant analysis was conducted to determine if a signal is justified at this location. The results of that analysis, described further below, did not support the installation of a traffic signal, therefore no additional traffic operations or safety analysis was performed and this alternative was not carried forward for further design or cost considerations.

### 3.2.1 Traffic Signal Warrant

A traffic signal warrant analysis was performed using the 2017 turning movement count data collected at the study intersection. Traffic signal warrants were performed based on methodologies defined in the M anual of Uniform Traffic Control Devices (MUTCD, 2009 edition). This approach is consistent with methods used by VDOT to determine whether a traffic signal should be considered at an intersection. Nine warrants are documented in the MUTCD, which provides guidance on justification of traffic signal installation. The results of the nine warrants are provided below.

## Warrants 1 through 3

Warrant 1 (Eight-Hour Vehicular Volume), Warrant 2 (Four-Hour Vehicular Volume), and Warrant 3 (Peak Hour) were evaluated at the study intersection. Warrant 1 contains three conditions, which are shown in Error! Reference source not found.. The results of Warrants 1 through 3 are shown in Error! Reference source not found..

Table 4: MUTCD Warrant 1 Conditions

| Warrant 1 | Eight-Hour Vehicular Volume |
| :---: | :---: |
| Condition A | Minimum Vehicular Volume |
| Condition B | Interruption of Continuous Traffic |
| Combination | Combination of Condition A and Condition B |

## Table 5: Traffic Signal Warrant Analysis Results

|  | Warrant 1A | Warrant 1B | Warrant 1 <br> Combination | Warrant 2 | Warrant 3 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2017 Existing | Not Met (1 of 8 hours satisfied) | Not Met ( 5 of 8 hours satisfied) | Not Met (4 of 8 hours satisfied) | Not Met (3 of 4 hours satisfied) | Met |

Under existing traffic conditions, the study intersection is not projected to meet traffic signal Warrant 1 or Warrant 2. At this time, only Warrant 3 is met. Although Warrant 3 is met, a traffic signal would not be warranted at this intersection without satisfying the eight-hour volumes. Traffic signal warrant worksheets are included in Appendix B. Should existing traffic volumes, patterns or land uses change in the vicinity of the intersection, a traffic signal warrant analysis may need to be conducted to consider the future conditions.

## Warrant 4

Warrant 4 (Pedestrian Volume) is intended for applications where traffic volume on a major street is so heavy that pedestrians experience excessive delay in crossing the major street. To meet the requirements for Warrant 4, the pedestrian volume crossing the major street along with the major street traffic volume at an intersection (or midblock location) during an average day are plotted against two charts provided in the MUTCD. On the first chart, each of any four hours must exceed the warrant, while on the second chart any one hour must exceed the warrant. No pedestrians were counted at the subject intersection during the 12 -hour traffic count conducted; therefore, the pedestrian volume requirements of Warrant 4 were not met.

## Warrant 5

Warrant 5 (School Crossing) is intended for application where school children crossing the major street are the principal reason to install a traffic signal. To meet the requirements for Warrant 5 , there must be a minimum of 20 students during the highest crossing hour across the major street. There are no schools near the study intersection, and the counted volume of pedestrians does not meet the 20 -student minimum. Therefore, Warrant 5 was not met.

## Warrant 6

Warrant 6 (Coordinated Signal System) is applicable in situations where a coordinated signal system necessitates the installation of a traffic control signal to maintain proper platooning of vehicles. The subject intersection is not located within a coordinated network; therefore, Warrant 6 was not met.

## Warrant 7

Warrant 7 (Crash Experience) is intended for application where the severity and frequency of crashes are the principle reasons to consider installing a traffic control signal. To meet the requirements for Warrant 7, there must be a history of crashes amounting to at least five crashes within the past year resulting in personal injury or property damage above the reporting thresholds. These crashes must also be of such a type that is correctable by the installation of a traffic signal. An adequate trial of alternatives must also have been attempted. In addition to meeting these criteria, certain vehicular and pedestrian volumes must be present for eight hours of the day. Based on a review of the crash data from 2015 through 2019, only one year had five preventable crashes occur at the subject intersection and the remaining years all had less than five. Additionally, these five crashes were not all susceptible to correction by a traffic signal; therefore, Warrant 7 was not met.

## Warrant 8

Warrant 8 (Roadway Network) is intended for application where some intersections might be justified to encourage concentration and organization of traffic flow on a roadway network. To meet the requirements for

Warrant 8, the M UTCD states that the intersection must have an existing or immediately projected entering volume of at least 1,000 vehicles per hour during the peak hour of a typical weekday and five-year projected traffic volumes that meet one or more of Warrants 1, 2, and 3 during an average weekday or 1,000 vehicles per hour for each of any five hours of a typical weekend (Saturday or Sunday). The current traffic volumes exceed 1,000 vehicles per hour, but future traffic volumes were not projected. If the projected traffic volumes meet one or more of Warrants 1, 2, and 3 during an average weekday, then Warrant 8 may be met in the future.

## Warrant 9

W arrant 9 (Intersection Near a Grade Crossing) is intended for use at intersections where the conditions described in the other eight traffic signal warrants are not met. To meet the requirements of Warrant 9, proximity to a railroad grade crossing on an intersection approach controlled by a Stop or Yield sign is the principal reason to consider installing a traffic control signal. As no grade crossings exist within 140 feet of the subject intersection, W arrant 9 was not evaluated.

### 3.2.2 Traffic Signal Warrant Results

Based on an analysis of the M UTCD Traffic Signal Warrants 1 through 9, a traffic signal is not warranted at the Earlysville Road and Reas Ford Road intersection. VDOT does not support the installation of traffic signals for just meeting peak hour warrants. Error! Reference source not found. provides a summary of the results of Warrants 1 through 9.

Table 6: Traffic Signal Warrant Analysis Results

| Warrants |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| Not M et | Not M et | M et | Not M et | Not M et | Not M et | Not M et | Not Met | Not Met |

### 3.3 Conceptual Design and Planning Level Cost Estimates

The approximate planning level cost estimate is based a combination of PCES, the 2015 version of Transportation and M obility Planning Division Statewide Planning Level Cost Estimate Spreadsheet, quantity take-offs, and recent bid costs. Table 7 includes a cost breakdown of the roadway; construction contingency; construction, engineering, and inspection (CEI); preliminary engineering (PE); and right-of-way acquisition and utility relocation costs. The planning level cost estimate is preliminary and is not based on design.

### 3.3.1 Alternative 1 (Low-Cost Countermeasures)

Based on a review of available right-of-way near the intersection, it is anticipated Alternative 1 will not require the acquisition of additional right-of-way. It is assumed the proposed improvements could be delivered with maintenance staff resources, so it is assumed to be a no-plan project.

The Right-of-Way Acquisition and Utility Relocation Costs for Alternative 1 (Low-Cost Countermeasure) are shown as $\$ 0$ since these improvements should not impact right-of-way or utilities.

It is assumed that these improvements may be considered maintenance activities.

### 3.3.2 Alternative 2

For Alternative 2, depicted in Figure 1, it was determined that the construction of a mini-roundabout, with an inscribed diameter between 80 feet, would lessen the impacts to existing right-of-way when compared to a singlelane roundabout, with an inscribed diameter between 90-120 feet. Although the study intersection lies within prescriptive right-of-way, these additional right-of-way impacts can alter the timeframe for implementation and estimated planning level cost.

Prescriptive right-of-way is right-of-way in perpetuity for the use of a state-maintained roadway and its continual maintenance. The right-of-way measures 15 feet from either side of the centerline of the roadway. Typically, the purchase of the 15 feet of right-of-way has zero value but would still require a signed acquisition from the adjacent parcel owner.

A modified mini-roundabout with shoulder, as opposed to curb and gutter, was analyzed, but it was determined that the shoulder and ditch design would require additional right-of-way and utility impacts. These impacts were determined to be larger than the cost of the proposed curb and gutter and drainage features associated with the selected mini-roundabout. A single-lane roundabout with shoulders was not analyzed as the VDOT Road Design $M$ anual states that single-lane roundabouts shall be provided with curb and gutter on the outside of the circulatory roadway.

The following considerations should be considered during the design phase of the proposed mini-roundabout (Alternative 2).

* Truck turning movements must be accommodated during mini-roundabout design. A traversable center island and additional pavement for acute right turns will be required with a mini-roundabout to prevent truck over tracking.
* A school bus was used as a design vehicle for developing this alternative. This leads to a larger inscribed diameter and circulatory lane width than if a passenger car was used.
* All existing right-of-way in the area is prescriptive.
* Existing access to adjacent parcels and driveway locations should be able to be maintained in a proposed roundabout configuration. The concrete splitter island on the eastbound approach on Earlysville Road may need to be shortened and supplemented with pavement marking to allow turning movements into Rivanna Community Church and Earlysville Exchange.
* The proposed mini-roundabout is likely to increase the impervious (paved) area at one or more drainage outfalls of the study intersection. Current drainage and stormwater management regulations will need to be considered.

For Alternative 2 (M ini-Roundabout) the Right-of-Way Acquisition and Utility Relocation cost is made up of nearly $60 \%$ utility relocations. The utilities that have been estimated to be relocated include 3 distribution towers and 2 service poles. These have been estimated to be relocated due to the grading and drainage needed for the miniroundabout.

Table 7: Planning Level Cost Estimates

|  | Alternative 1 <br> Low-Cost Countermeasures <br> (2019 dollars) | Alternative 2 <br> Mini-Roundabout <br> (2019 dollars) |
| :--- | ---: | :---: |
| Construction Cost (with 25\% Contingency) | $\$ 60,000$ | $\$ 1,066,000$ |
| Construction, Engineering, \& Inspection (CEI) | $\$ 10,000$ | $\$ 178,000$ |
| Preliminary Engineering | $\$ 0$ | $\$ 235,000$ |
| Right-of-Way Acquisition and Utility Relocation | $\$ 0$ | $\$ 474,000$ |
| Project Total | $\$ 70,000$ | $\$ 1,998,000$ |

### 3.3.3 Additional Design Recommendations

Access-managements recommendations may be designed within the influence area of the study intersection to improve the safety and flow of traffic along Route 743 and Route 660. These following recommendations should
be considered in the further to supplement Alternative 1 and Alternative 2 in order to provide adequate intersection/access spacing in accordance with VDOT's M inimum Spacing Standards for Commercial Entrances, Intersections, and M edian Crossovers from the VDOT Road Design M anual.

## * Commercial access to Earlysville Exchange and VIP Customs

- A better defined commercial access with new curb and gutter in the west quadrant of the study intersection.
- Potential impacts to parking access for Earlysville Exchange and VIP Customs may trigger additional right-of-way and zoning impacts
- Potential impacts to the flow of travel through each site may be mitigated by a one-way drive aisle with parallel parking and right-in only and right-out only entrances to the site.
- It is assumed that these improvements are minor and could be covered by a Minimal-Plan Project. However, due to the impacts to the site parking, the right-of-way impacts would be considered moderate.


### 3.4 Altemative Comparison

Based on an evaluation of the proposed alternatives analysis provided herein, the study team developed the following comparative conclusions. Alternative 2 (mini-roundabout), operationally performs with less vehicle delay than Alternative 1 (low-cost countermeasures). Both Alternative 1 and Alternative 2 provide positive crash reduction; however, Alternative 2 provides a greater benefit. Alternative 2 provides overall greater safety and operational benefits to the traveler.

A summary of the pros and cons of Alternative 1 and Alternative 2 is provided in Table 8 and Table 9, respectively.
Table 8: Altemative 1 Benefits and Limitations Summary

| Improvement Benefits | Improvement Limitations |
| :--- | :--- |
| No right-of-way required | Does not improve traffic operations |
| * Improves safety | Does not help reduce vehicle speeds on Earlysville |
| $-\quad$ 10\% reduction in injury and fatal crashes | Road (traffic calming) |
| - Increases driver awareness and recognition of the |  |
| intersection and potential conflicts |  |

## Table 9: Altemative 2 Benefits and Limitations Summary

| Improvement Benefits | Improvement Limitations |
| :--- | :--- | :--- |
| * | Right-of-way required |
| Improves safety | Constilies impacted |
| Requires vehicles to slow down before entering the |  |
| roundabout (traffic calming) |  |
| Improves northbound sight distance for Reas Ford |  |
| Road approach |  |
| Accommodates school buses, fire trucks, and other |  |
| large vehicles |  |

### 4.0 Recommendations

Alternative 2 (mini-roundabout) is recommended for construction at the Earlysville Road and Reas Ford Road/Earlysville Forest Drive intersection to improve both the safety and operations of the intersection. However, should funding constraints exist,. Alternative 1 (low cost countermeasures) should be implemented as a near-term improvement to reduce crash risk within the intersection.

Public outreach should be performed within the local area to educate the public on the benefits of a roundabout and to educate drivers the rules of a roundabout (http://www.virginiadot.org/innovativeintersections/).

## Appendix A: Turning Movement Count Data

Intersection: Rt 743 and Rt 660
Start Date: 11/14/2017
Start Time: 6:30:00 AM

County: Albemarle


## Appendix B: Traffic Signal Warrant

Route 743 and Route 660
TRAFFIC SIGNAL VOLUME WARRANT ANALYSIS
Based on 2009 MUTCD


## Appendix C: VJUST Results



| Intersection Results |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Notes |
| Type | Dir | $\begin{gathered} \text { Maximum } \\ \text { V/C } \end{gathered}$ | Accommodation Compared to Conventional | Weighted Total Conflict Points |  |
| 50 Mini Roundabout | - | 0.77 |  | 8 |  |
| 75 Mini Roundabout | - | 0.76 |  | 8 |  |
| Roundabout | - | 0.56 |  | 8 |  |
| Two-Way Stop Control | - | 0.35 |  | 48 |  |

## Information

| Congestion | The maximum v/c ratio represents the worst v/c of all zones that make up an intersection. |
| :---: | :--- |
| Pedestrian | Compares the potential of each design to accommodate pedestrians based on safety, wayfinding, and delay. Potential is <br> qualitatively defined as better ( + ), similar (blank cell), or worse $(-)$ than a conventional intersection or traditional diamond <br> interchange. |
| Safety | Weighted Total $=(2 \times$ Crossing Conflicts $)+$ Merging Conflicts + Diverging Conflicts |

## VDOT Junction Screening Tool

 Input Worksheet| Project Title: | Earlysville Intersection Safety Review |
| ---: | :---: |
| E-W Facility: | Route 660 (Reas Ford Road) |
| N-S Facility: | Route 743 (Earlysville Road) |
| Date: | September 11, 2019 |


| Traffic Volume Demand |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Volume (veh/hr) |  |  |  |  |
|  | U-Tur | / Left | Through | Right | Truck |
|  |  |  | V | $\square$ | Percent (\%) |
| Eastbound |  |  | 3 | 12 | 2.00\% |
| Westbound |  |  | 2 | 99 | 2.00\% |
| Northbound |  |  | 625 | 50 | 2.00\% |
| Southbound |  |  | 126 | 12 | 2.00\% |
| Adjustment Factor | 0.80 | 0.95 |  | 0.85 | - |
| Suggested | U-0.8 | L-0.95 |  | 0.85 | - |
| Truck to PCE Factor |  |  | Suggested = 2.00 |  | 2.00 |
| Critical Lane Volume |  |  | 1600 |  |  |


| Equivalent Passenger Car Volume |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Volume (pc/hr) |  |  |  |
|  | U-Turn / Left | Through | Right | Approach |
|  |  |  |  |  |
|  | 67 | 3 | 12 | 82 |
| Westbound | 23 | 2 | 101 | 126 |
| Northbound | 8 | 638 | 51 | 697 |
| Southbound | 37 | 129 | 12 | 178 |


| Notes: |  |
| ---: | :--- |
| Left-turn Adjustment Factor | Conversion of left-turning vehicles to equivalent through vehicles |
| Right-turn Adjustment Factor | Conversion of right-turning vehicles to equivalent through vehicles |
| U-turn Adjustment Factor | Conversion of U-turning vehicles to equivalent through vehicles |
| Truck to PCE Factor | 1 truck = X Passenger Car Equivalents |
| Critical Lane Volume Sum Limit | Saturation value for critical lane volume sum at an intersection |

## VDOT Junction Screening Tool

Possible Configurations
Indicate with a " Y " or " N " if each intersection or interchange configuration should or should not be considered. Use the information links for guidance. Then, click the "Show/Hide Configurations button" to hide the worksheets for the configurations that will not be considered.


## VDOT Junction Screening Tool

Directional Questions and Base Lane Configurations
Before entering a base number of through lanes for each direction, answer all applicable directional question for each intersection or interchange configuration selected for consideration. Navigate to the lane configuration worksheet for example diagrams, if provided.

| Intersections | Question | Direction |
| :--- | :--- | :--- |
| Bowtie | N/A | N/A |
| Continuous Green-T | N/A | N/A |
| Echelon | N/A | N/A |
| Median U-Turn | N/A | N/A |
| Partial Displaced Left Turn | N/A | N/A |
| Partial Median U-Turn | N/A | N/A |
| Restricted Crossing U-Turn | N/A | N/A |
| Single Loop | N/A | N/A |
| Split Intersection | N/A | N/A |
| Interchanges |  | Question |
| All | N/A | Direction |

## Base Number of Through Lanes

Enter a base number of through lanes for each direction. The number of through lanes entered will populate on each non-roundabout lane configuration worksheet. This tool also allows the user to enter the number of through lanes on the lane configuration worksheets directly. This base number may be overwritten on individual lane configuration worksheets. Turn lanes, shared lanes, and channelized lanes must still be entered in each lane configuration worksheet.

| Eastbound | 1 |
| :---: | :---: |
| Westbound | 1 |
| Northbound | 1 |
| Southbound | 1 |






## Appendix D: Level of Service Worksheets

## AM Peak Period

## MOVEMENT SUMMARY

## \$ Site: 101 [Route 743 and Route 660 ]

Earlysville Safety Analysis
Site Category: (None)
Roundabout


Site Level of Service (LOS) Method: Delay \& v/C (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F vill resull if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection)
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6)
Roundabout Capacily Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies
Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D)
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## PM Peak Period

## MOVEMENT SUMMARY

## Site: 101 [Route 743 and Route 660]

Earlysville Safety Analysis
Site Category: (None)
Roundabout


Site Level of Service (LOS) Method: Delay \& vic (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab)
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F vill result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
intersection and Approach LOS values are based on average delay for all movements (vic not used as specified in HCM 6).
Roundabout Capacity Model SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies
Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D)
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation

HCM 2010 TWSC
3: Reas Ford Rd (Route 660)/Earlysville Forest Dr (Route 660) \& Earlysville Rd (Route 743)

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 16.3 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | $\uparrow$ | 「 |  | \$ |  |  | \$ |  |
| Traffic Vol, veh/h | 8 | 625 | 50 | 36 | 126 | 12 | 23 | 2 | 99 | 66 | 3 | 12 |
| Future Vol, veh/h | 8 | 625 | 50 | 36 | 126 | 12 | 23 | 2 | 99 | 66 | 3 | 12 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | 100 | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 66 | 81 | 56 | 60 | 90 | 75 | 52 | 50 | 79 | 71 | 75 | 60 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 12 | 772 | 89 | 60 | 140 | 16 | 44 | 4 | 125 | 93 | 4 | 20 |



| Approach | EB | WB | NB | SB |
| :--- | :--- | :---: | ---: | ---: |
| HCM Control Delay, s | 0.1 | 2.8 | 37.5 | 130.4 |
| HCM LOS |  | E | F |  |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 277 | 1424 | - | -781 | - | -125 |  |
| HCM Lane V/C Ratio | 0.627 | 0.009 | - | -0.077 | - | -0.936 |  |
| HCM Control Delay (s) | 37.5 | 7.5 | 0 | - | 10 | 0 | -130.4 |
| HCM Lane LOS | E | A | A | - | A | A | - |
| HCM 95th \%tile Q(veh) | 3.9 | 0 | - | - | 0.2 | - | - |
| H.1 |  |  |  |  |  |  |  |

HCM 2010 TWSC
3: Reas Ford Rd (Route 660)/Earlysville Forest Dr (Route 660) \& Earlysville Rd (Route 743)



| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, s | 0.7 | 1 | 35.5 | 34.8 |
| HCM LOS |  | E | D |  |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 246 | 885 | - | -1324 | - | -172 |  |
| HCM Lane V/C Ratio | 0.538 | 0.023 | - | -0.079 | - | -0.304 |  |
| HCM Control Delay (s) | 35.5 | 9.2 | 0 | - | 8 | 0 | -34.8 |
| HCM Lane LOS | E | A | A | - | A | A | - |
| HCM 95th \%tile Q(veh) | 2.9 | 0.1 | - | - | 0.3 | - | - |
| D | 1.2 |  |  |  |  |  |  |


[^0]:    *Rev. 1/15

[^1]:    *Rev. 1/15

[^2]:    *Rev. 1/15

[^3]:    *Rev. 1/15

[^4]:    *Rev. 1/15

[^5]:    *Rev. 1/15

[^6]:    *Rev. 1/15

[^7]:    *Rev. 1/15

